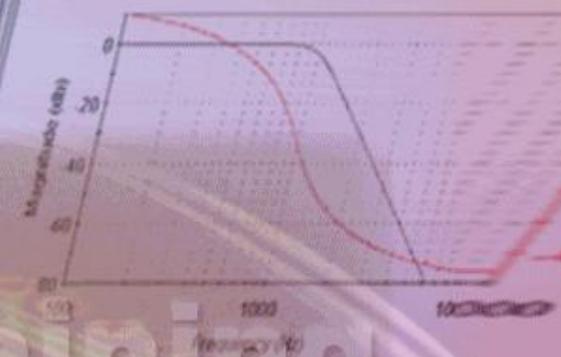


HANDS-ON

Training



107_OAF

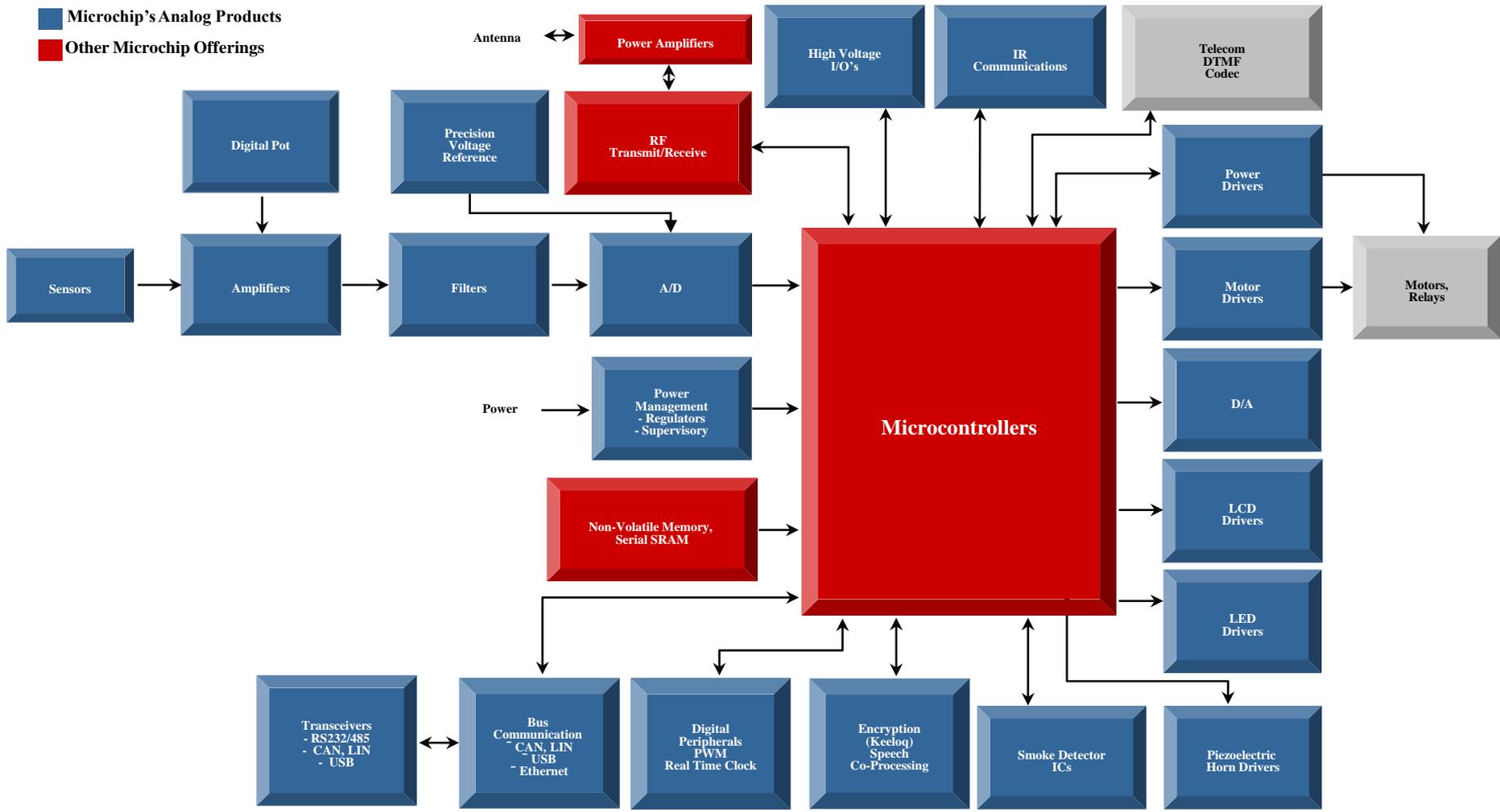
Operational Amplifier Fundamentals



Microchip Analog FAE
Michael Chu
Michael.chu@microchip.com



Universe of Embedded Control Systems





Overview

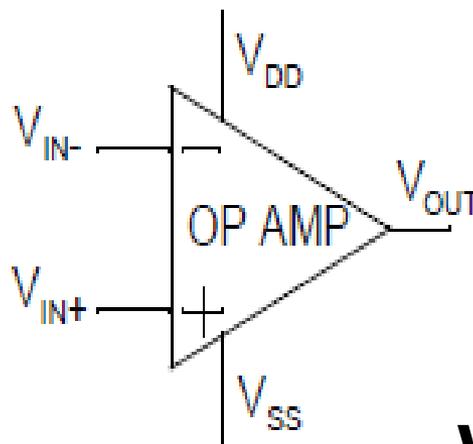
- The class will begin with basic **Operational Amplifier Concepts and Terminology**.
- Primary DC and AC characteristics found in an op amp data sheet will be defined and discussed, with **Examples** to enhance understanding.
- **Microchip Analog and Interface Product Introduction – TreeLink Application/ Product Selection Guide**
- Examples and analysis of Op Amp application circuits will be provided—**Demo Boards**

POWER SUPPLY

- No min or max Voltage (V_{DD} , V_{SS})
- $I_{SUPPLY} = 0$ Amps
- Power Supply Rejection Ratio (PSRR) = ∞

INPUT

- Input Current (I_g) = 0
- Input Impedance (Z_{IN}) = ∞
- Input Voltage Range (V_{IN}) \rightarrow no limits
- Zero Input Voltage and Current Noise
- Zero DC offset error (V_{OS})
- Common-Mode Rejection = ∞



OUTPUT

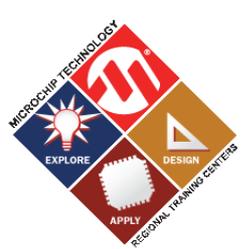
- $V_{OUT} = V_{SS}$ to V_{DD}
- $I_{OUT} =$
- Slew Rate (SR) = ∞
- $Z_{OUT} = 0\Omega$

$$V_{OUT} = A(V_{IN+} - V_{IN-})$$

SIGNAL TRANSFER

- Open Loop Gain (A_{OL}) = ∞
- Bandwidth = 0 \rightarrow ∞
- Zero Harmonic Distortion (THD)

FIGURE 1: The ideal op amp description can be separated into four basic categories: input, power supply, output, and signal transfer.

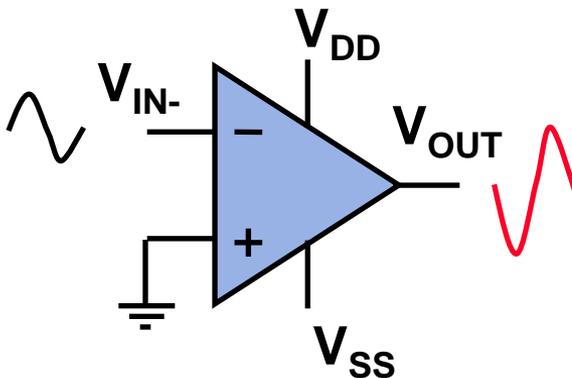


Op Amp Basics

Signal Input Modes

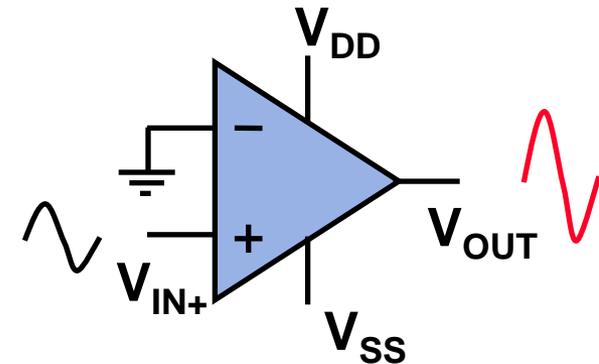
- Single-input mode

Inverting input

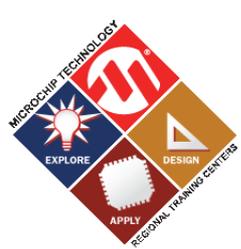


- Input signal is applied to the inverting input terminal
- V_{OUT} is 180° out of phase with V_{IN-}

Non-inverting input



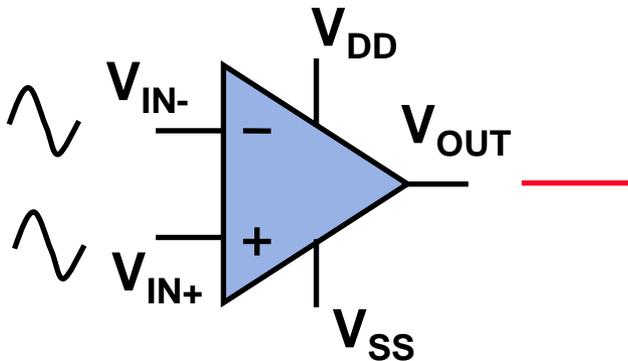
- Input signal is applied to the non-inverting input terminal
- V_{OUT} is in phase with V_{IN+}



Op Amp Basics

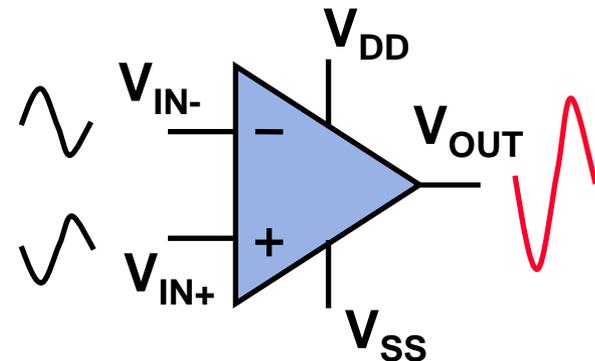
- Dual-input mode

Common mode inputs



- The input signals are in phase and their amplitudes are equal
- V_{OUT} is zero

Differential mode inputs



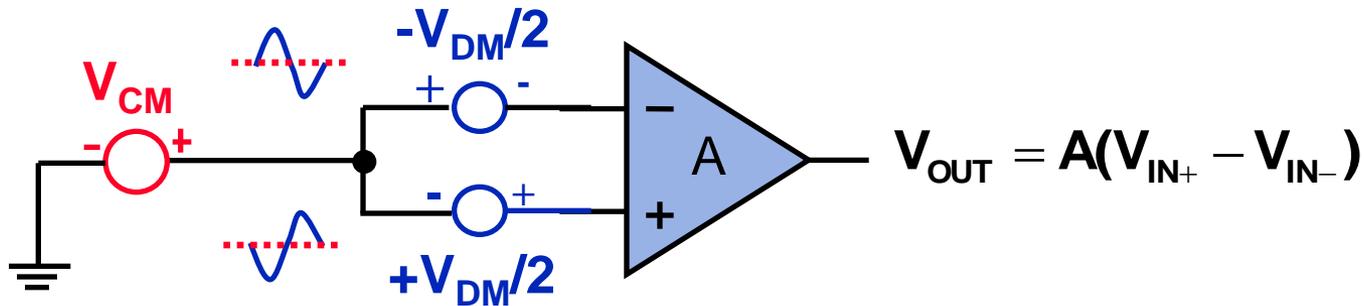
- The input signals are 180° out of phase and their amplitudes are equal
- V_{OUT} is in phase with V_{IN+}



Op Amp Basics

- **Emphasis: Representation of the input signals**

$V_{CM} = (V_{IN-} + V_{IN+})/2$ $V_{DM} = V_{IN+} - V_{IN-}$		$V_{IN+} = V_{CM} + V_{DM}/2$ $V_{IN-} = V_{CM} - V_{DM}/2$
---	--	---



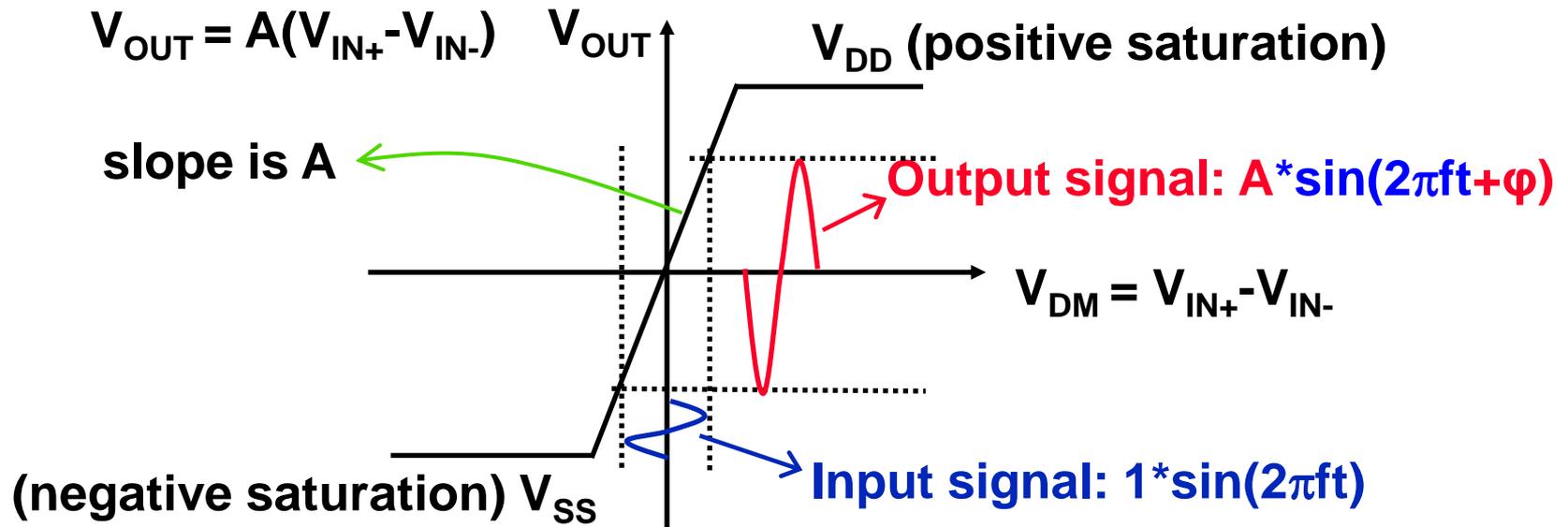
- Op amps **reject** common mode input (V_{CM}) and **only amplify** differential mode input (V_{DM})



Basic Op-Amp Concepts and Terminology

Op Amp Linearity

- When amplifying a signal, linearity means the information contained in the signal is not changed.
 - The **frequency** of signal is same.
 - The **amplitude** and **phase** of signal can be different.

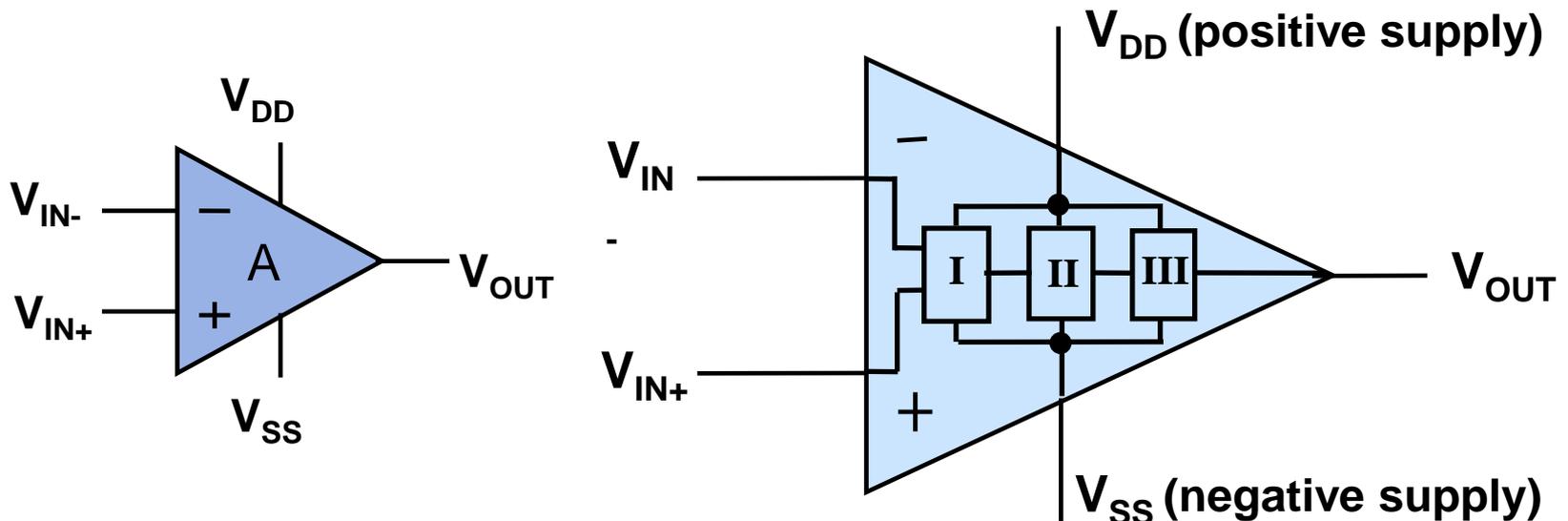




Basic Op-Amp Concepts and Terminology

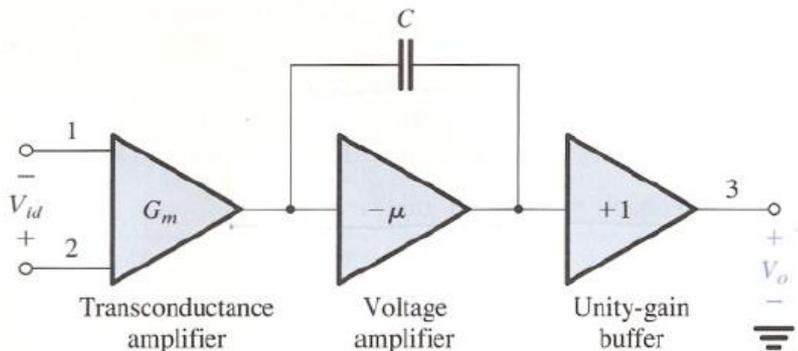
Op Amp Block Diagram

- The classical three stages inside an op amp.
 - I: Differential input stage
 - II: High voltage gain stage
 - III: Output stage



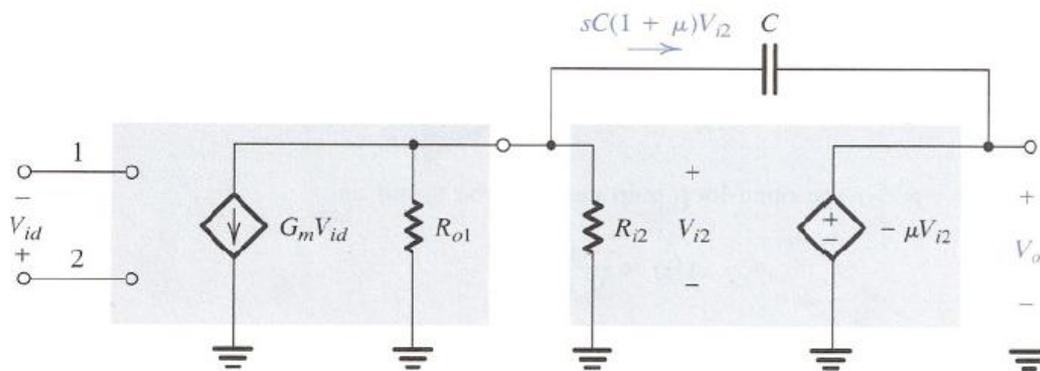


OP Amp Equivalent Circuit



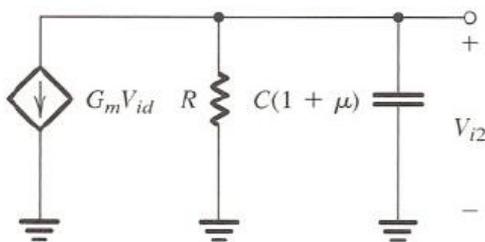
$$V_{i2} = -V_{id} \frac{G_m R}{1 + sC(1 + \mu)R}$$

$$A(s) \equiv \frac{V_o(s)}{V_{id}(s)} = \frac{\mu G_m R}{1 + sC(1 + \mu)R}$$



$$A_0 = \mu G_m R$$

$$\omega_b = \frac{1}{C(1 + \mu)R}$$



$$R = R_{o1} \parallel R_{i2}$$

$$A(s) = \frac{A_0}{1 + s/\omega_b}$$

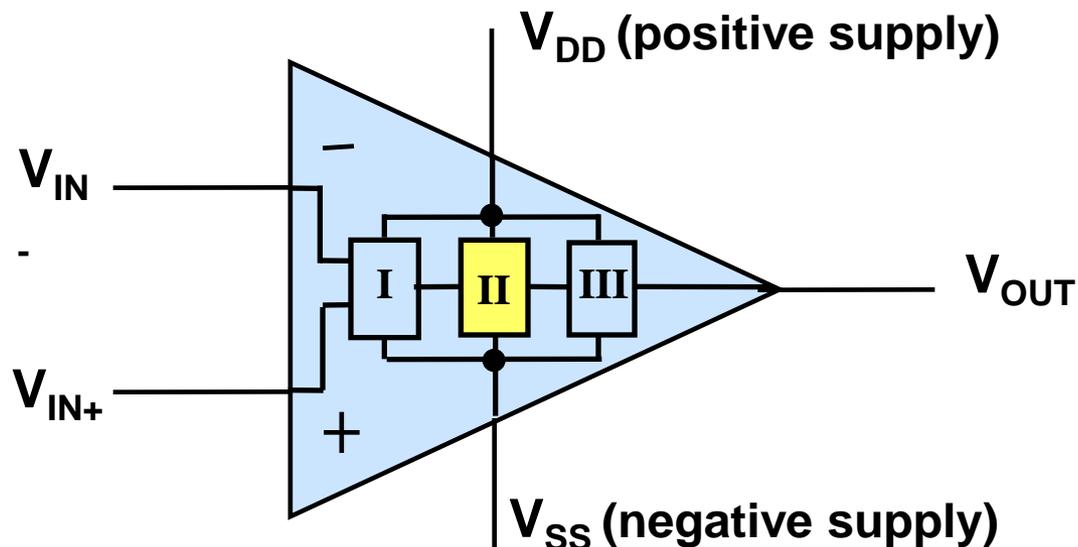
$$A(j\omega) = \frac{A_0}{1 + j\omega/\omega_b}$$



Basic Op-Amp Concepts and Terminology

High Voltage Gain Stage

- Provides very high open loop gain → **Infinity**
- Gains up the differential input signal and conveys it to the output stage.

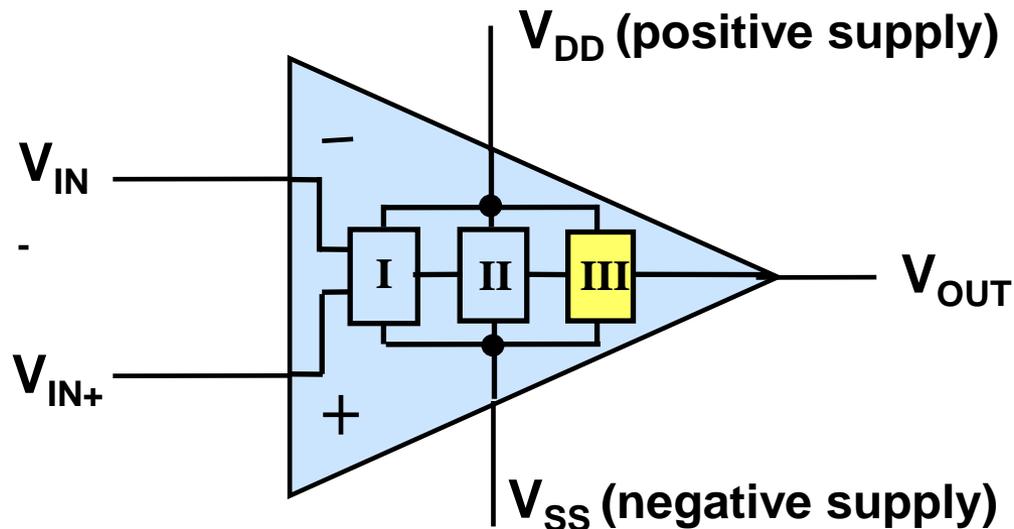




Basic Op-Amp Concepts and Terminology

Output Stage

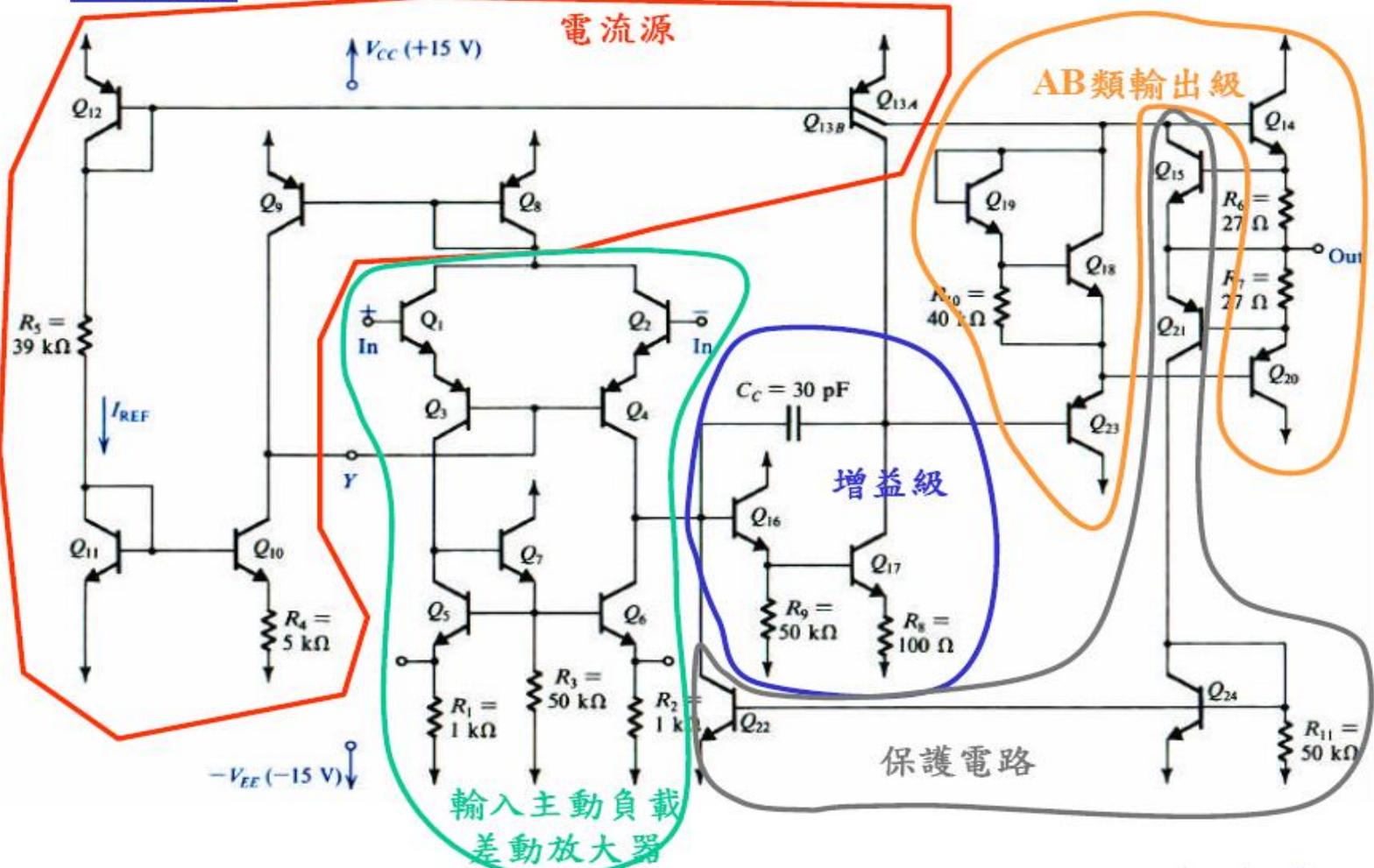
- Has very low output impedance → **Zero**
 - This minimizes the loading effect of the op amp output stage.
- Delivers current to the load of op amp.





運算放大器內部結構

741結構





Basic Op-Amp Concepts and Terminology

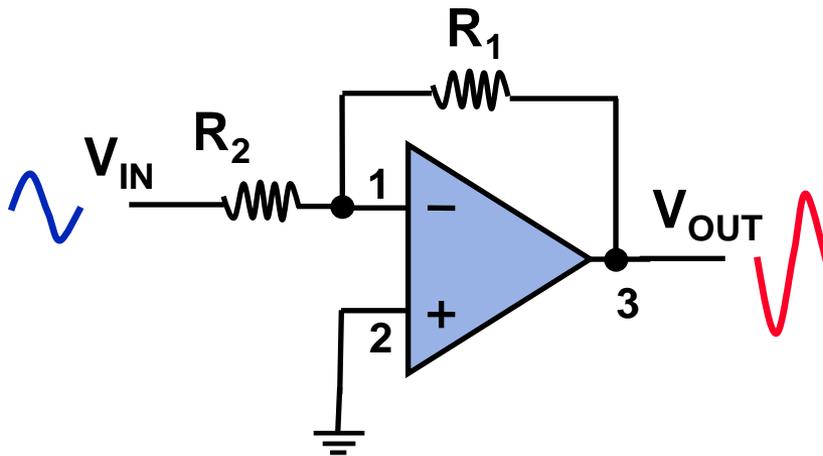
Analysis of Circuits Containing Ideal Op Amps

- Open Loop Configuration
 - Open loop gain is very large. Ideally, it is infinite. Op amp is normally not used in the open loop mode.
 - A typical application: Comparator (will be discussed later at the section of Applications Circuit) .
- Closed Loop Configuration
 - Inverting Amplifier
 - Non-inverting Amplifier
 - Voltage Follower
 - Differential Amplifier



Fundamental Op Amp Circuits

- **Emphasis: The Concept of the Virtual Short Circuit**
 - In a closed loop configuration, the virtual short circuit means that
 - **Whatever voltage is at 2 will automatically appear at 1** (due to the infinite open loop gain A_{OL})



For ideal op amp: $V_1 = V_2$

For real op amp: $V_1 \approx V_2$

$$V_2 - V_1 = \frac{V_o}{A} \approx 0 \text{ (workable)}$$

$$\Rightarrow V_2 \approx V_1$$

Assume $A \rightarrow \infty$ and this circuit works at all

→ Tracking each other in potential

→ Virtual short.

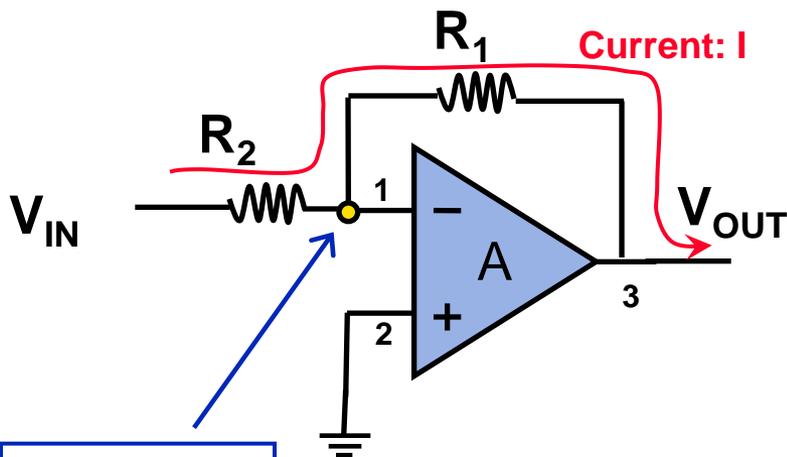
※ Virtual Ground.



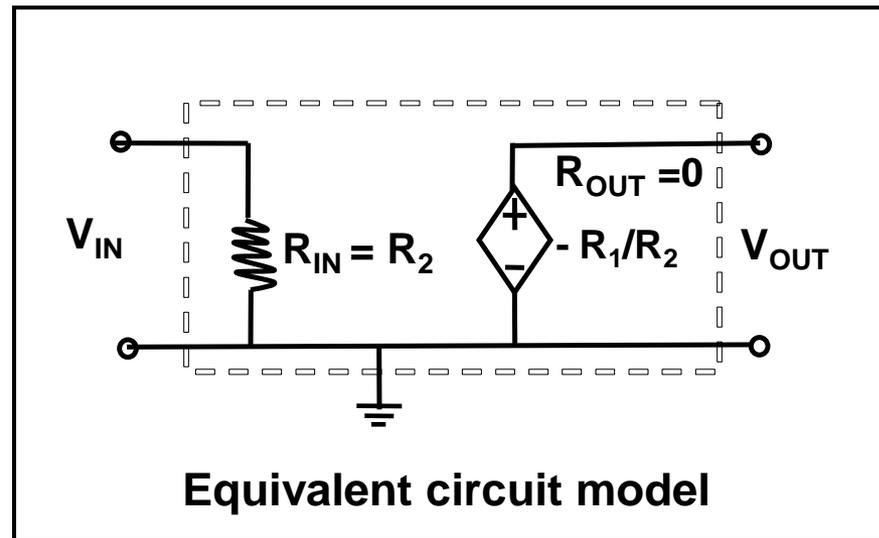
Basic Op-Amp Concepts and Terminology

Inverting Amplifier

- Closed loop gain $G = V_{OUT}/V_{IN} = - R_1/R_2$
- Input resistance $R_{IN} = R_2$, Output resistance $R_{OUT} = 0$



$V_1 \approx V_2 = 0$ because of $A \rightarrow \infty$



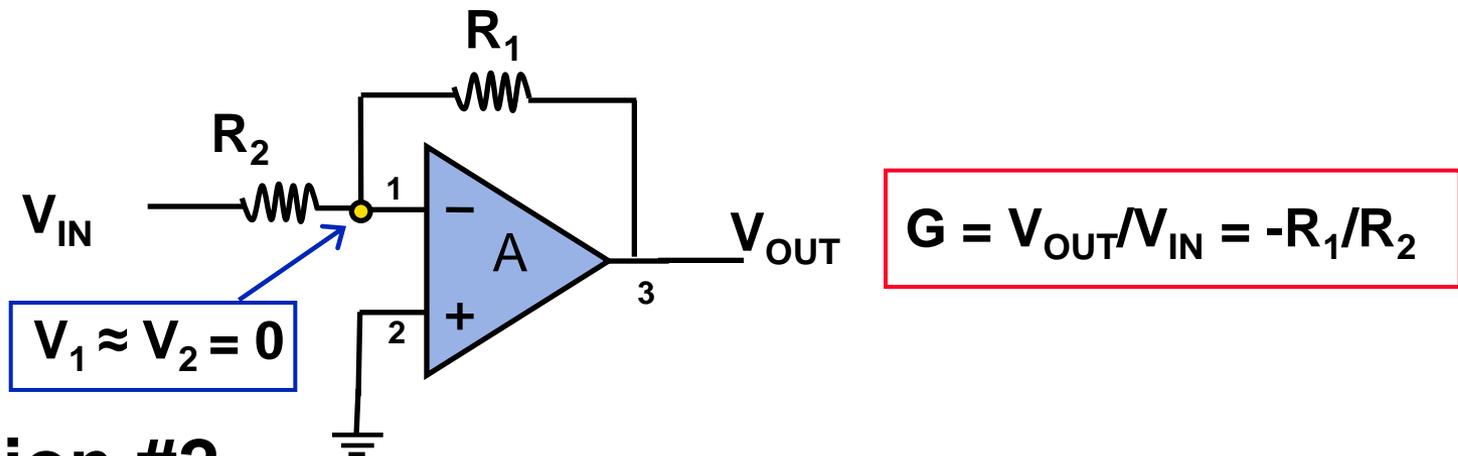
$$I = (V_{IN} - V_1)/R_2 = (V_1 - V_{OUT})/R_1 \rightarrow V_{IN}/R_2 = -V_{OUT}/R_1 \rightarrow V_{OUT}/V_{IN} = - R_1/R_2$$



Basic Op-Amp Concepts and Terminology

Exercise #2

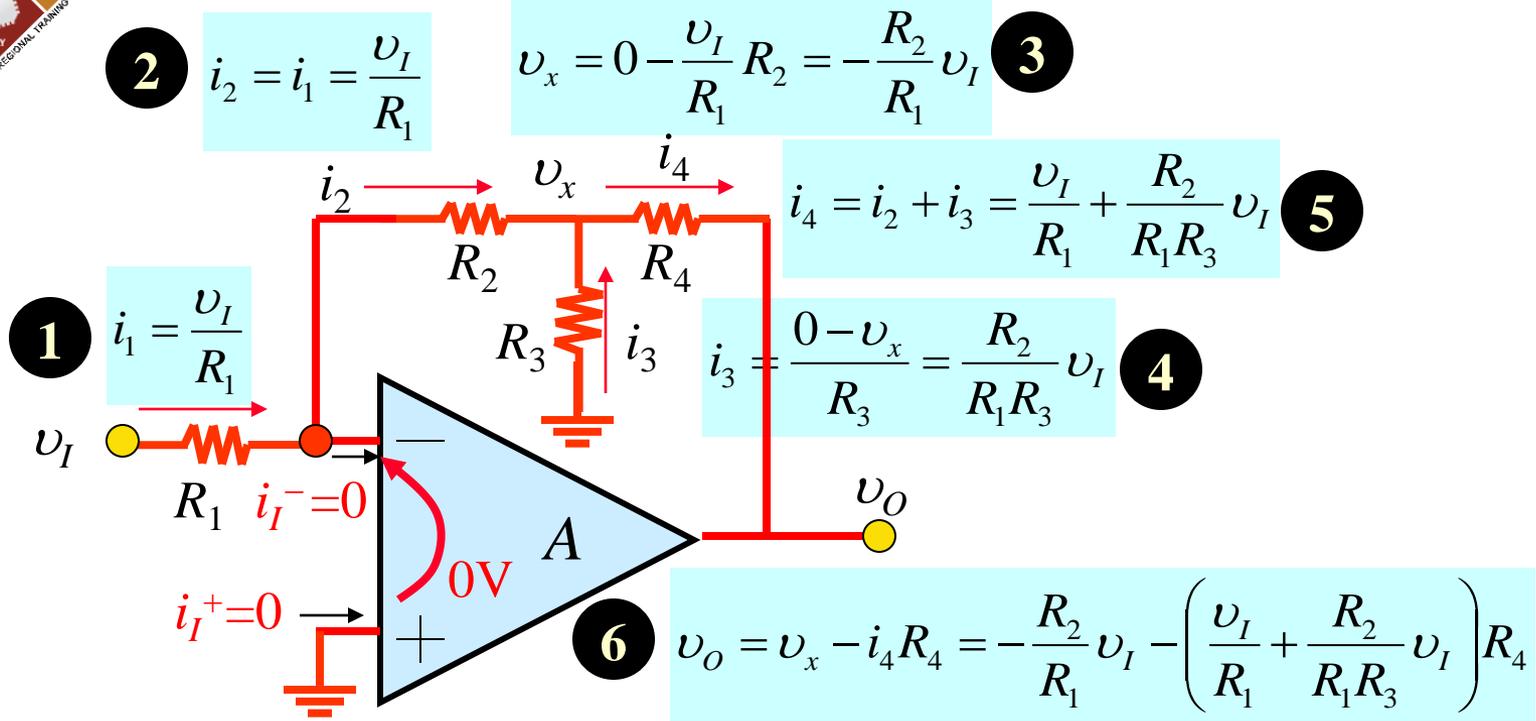
- Design an inverting amplifier having a gain of -10 and input resistance is $1\text{k}\Omega$. Give the values of R_1 and R_2 .
- If $V_{IN} = 0.2\text{V}$, what is the current that goes through R_2 ? And what is V_{OUT} ?



Solution #2

- $R_2 = 1\text{k}\Omega$, $R_1 = 10\text{k}\Omega$; $I_{R_2} = (V_{IN} - V_1) / R_2 = V_{IN} / R_2 = 0.2\text{mA}$,
 $V_{OUT} = -(R_1 / R_2) * V_{IN} = -2.0\text{V}$

用T型回授網路的反相放大器 (inverting amplifier with a T-network)

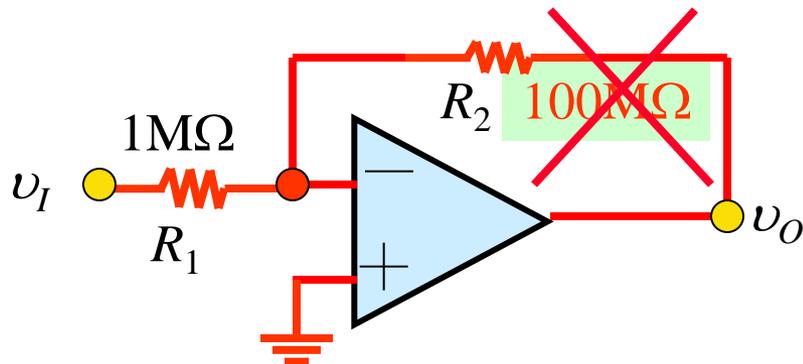


$$G = \frac{v_O}{v_I} = -\frac{R_2}{R_1} - \frac{R_4}{R_1} \left(1 + \frac{R_2}{R_3} \right) = -\frac{R_2}{R_1} \left(1 + \frac{R_4}{R_2} + \frac{R_4}{R_3} \right)$$

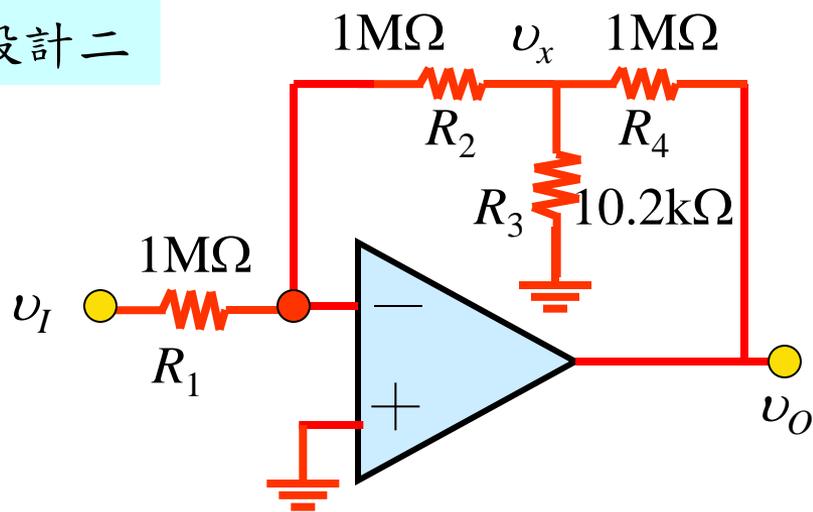


利用運算放大器設計一個反相放大器，輸入阻抗 $1\text{M}\Omega$ ，增益100，但電路中不得使用大於 $1\text{M}\Omega$ 的電阻。

設計一



設計二

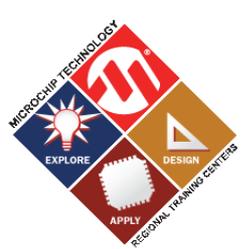


$$G = \frac{v_o}{v_i} = - \frac{R_2}{R_1} \left(1 + \frac{R_4}{R_2} + \frac{R_4}{R_3} \right)$$

1
1
98

100

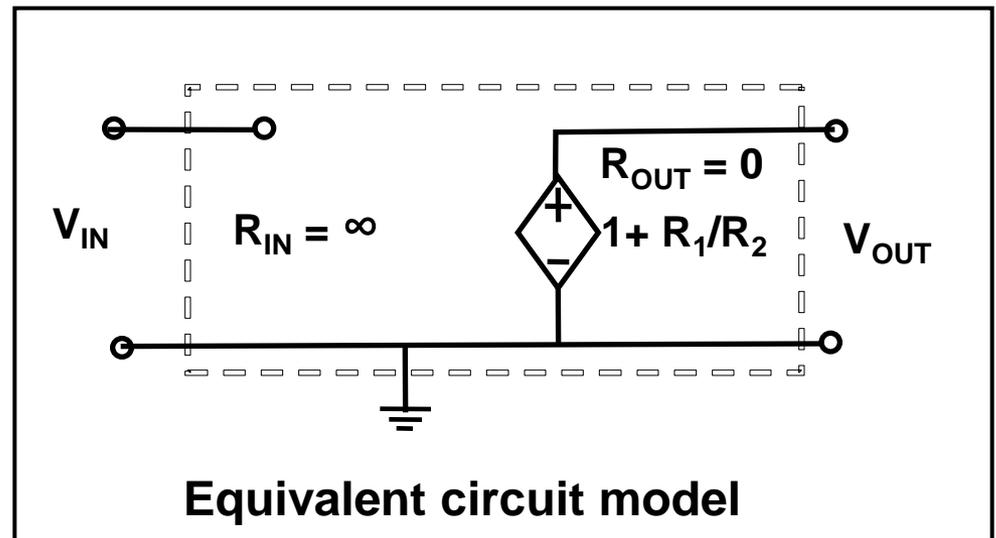
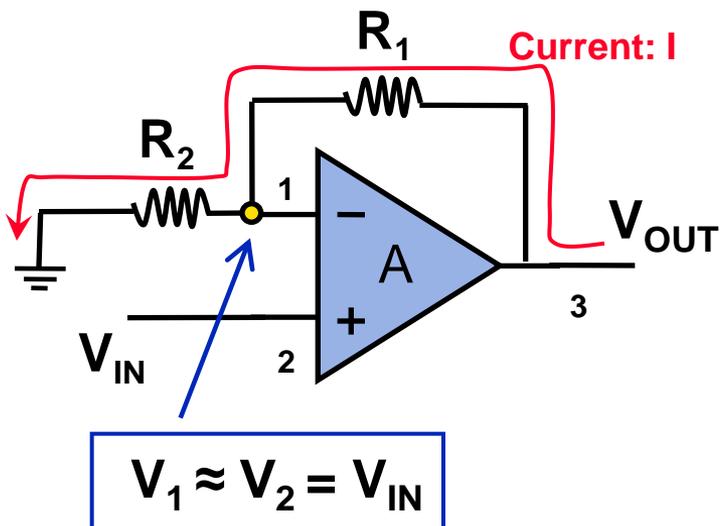
$$R_3 = 1\text{M}\Omega / 98 = 10.2\text{k}\Omega$$



Basic Op-Amp Concepts and Terminology

Non-inverting Amplifier

- Closed loop gain $G = V_{OUT}/V_{IN} = 1 + R_1/R_2$
- Input resistance $R_{IN} = \infty$, Output resistance $R_{OUT} = 0$



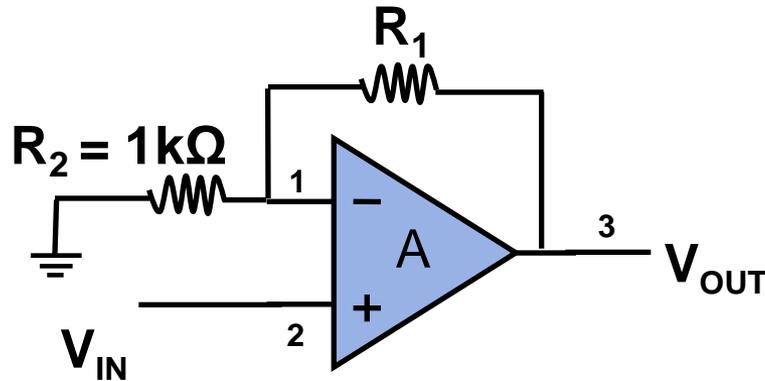
$$I = V_1/R_2 = (V_{OUT} - V_1)/R_1 \rightarrow V_{IN}/R_2 = (V_{OUT} - V_{IN})/R_1 \rightarrow V_{OUT}/V_{IN} = 1 + R_1/R_2$$



Basic Op-Amp Concepts and Terminology

Exercise #3

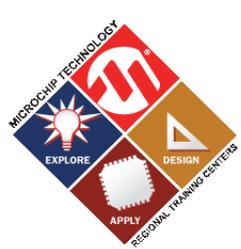
- Design a non-inverting amplifier having a gain of 10. Give the value of R_1 .
- If $V_{IN} = 0.1V$, what is the current that goes through R_2 ? And what is V_{OUT} ?



$$G = V_{OUT}/V_{IN} = 1 + R_1/R_2$$

Solution #3

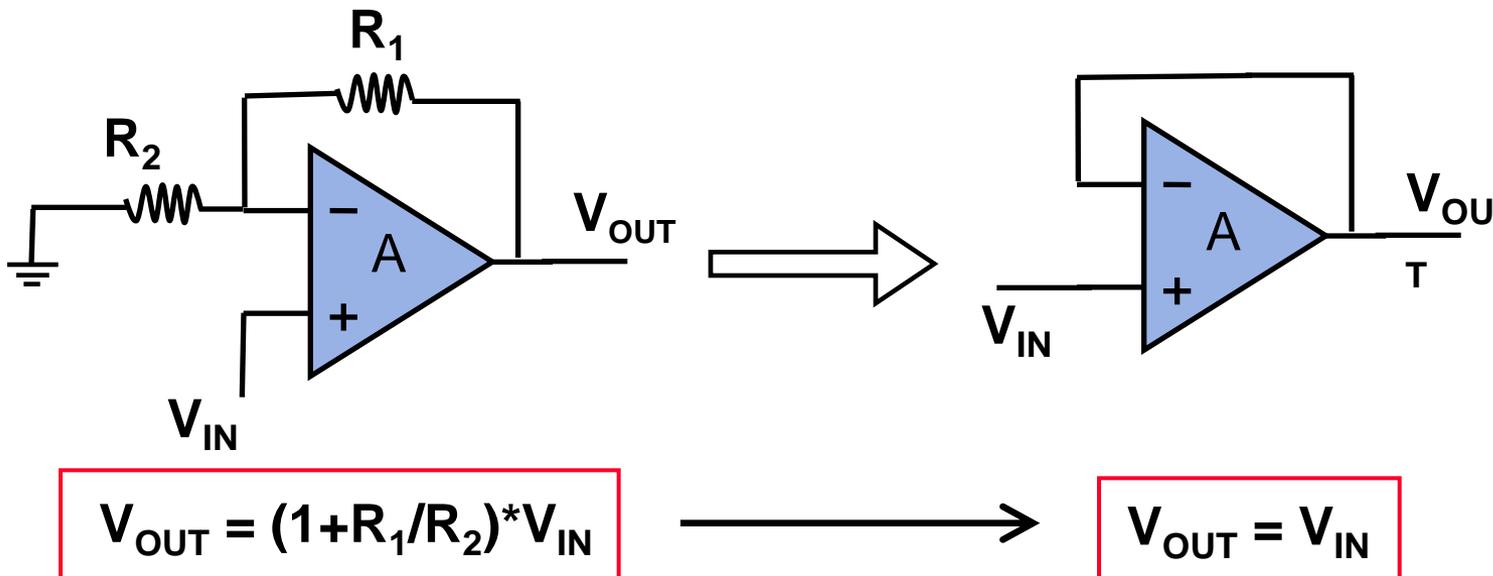
- $R_2 = 1k\Omega$, $R_1 = 9k\Omega$; $I_{R_2} = V_1/R_2 = V_{IN}/R_2 = 0.1mA$,
 $V_{OUT} = (1 + R_1/R_2) * V_{IN} = 10 * V_{IN} = 1.0V$



Basic Op-Amp Concepts and Terminology

Voltage Follower (Buffer Amplifier)

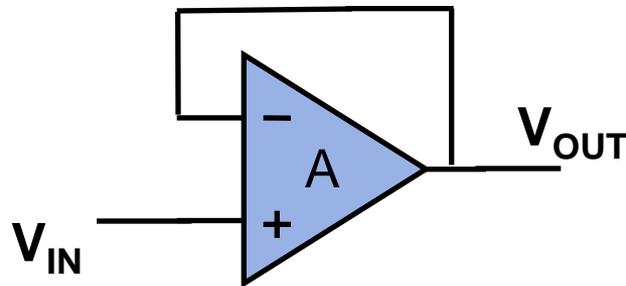
- Refer to the non-inverting amplifier configuration
 - Make $R_2 = \infty$ and $R_1 = 0$ to obtain the unity gain amplifier.



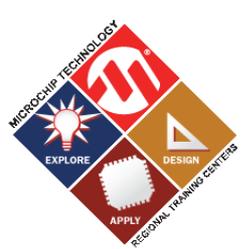


Basic Op-Amp Concepts and Terminology

- In the ideal case, $V_{OUT} = V_{IN}$, $R_{IN} = \infty$, $R_{OUT} = 0$
 - $V_{OUT} = V_{IN}$; Used as a voltage follower.
 - $R_{IN} = \infty$, $R_{OUT} = 0$; Used as a buffer amplifier for impedance matching and signal isolation.



Example: Buffer amplifiers are often used between the analog inputs/outputs of microcontroller and the outside circuits.



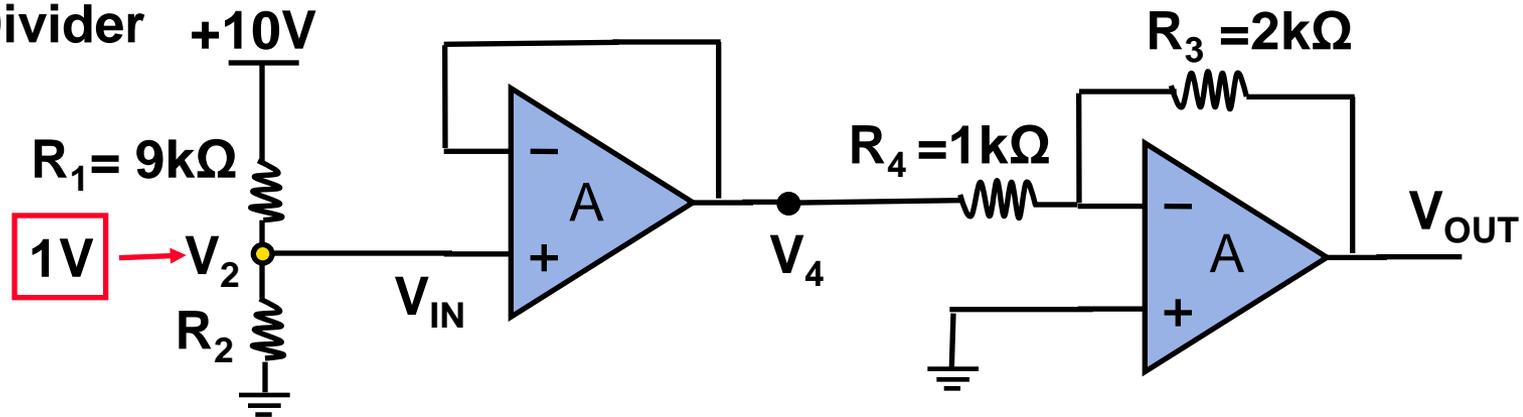
Basic Op-Amp Concepts and Terminology

Exercise #4

- Refer to the circuit, a buffer amplifier is connected with an inverting amplifier and a voltage divider. If $V_2 = 1V$, $R_2 = ?$ And $V_{OUT} = ?$
- If don't use buffer amplifier and connect them directly, can V_2 still keep 1V? Give the value of V_2 and V_{OUT} .

Voltage

Divider



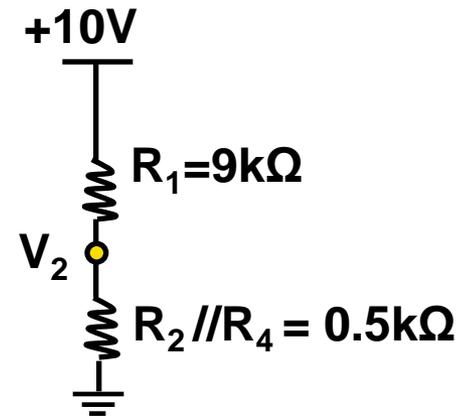
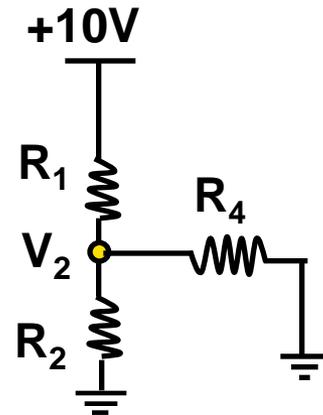
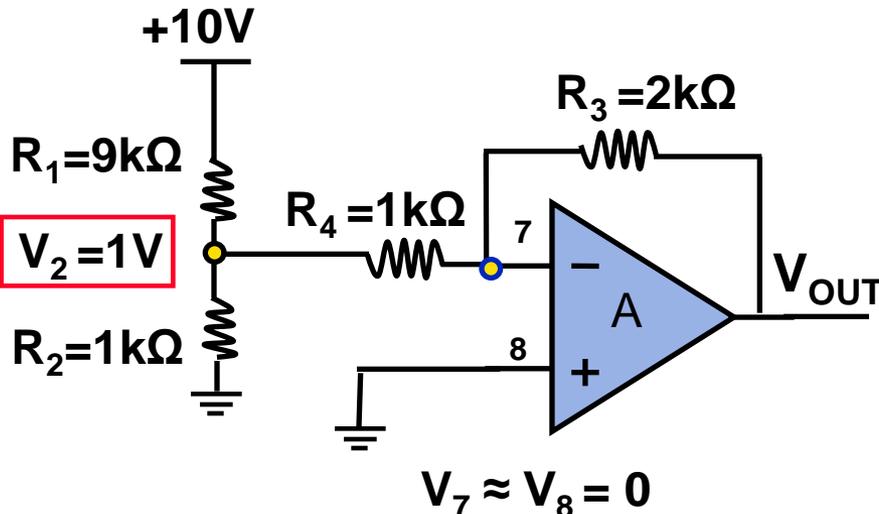


Basic Op-Amp Concepts and Terminology

Solution #4

- For $V_2 = 1V$, $R_2 = 1k\Omega$, $V_2 = V_4$
 $V_{OUT} = - (R_3/R_4)*V_4 = - (R_3/R_4)*V_2 = - 2*1V = -2V$
- If don't use buffer amplifier, V_2 can not keep 1.0V.
 $V_2 = [10V/(9k\Omega+0.5k\Omega)]*0.5k\Omega \approx 0.53V$ and $V_{OUT} = -1.06V$

Voltage Divider

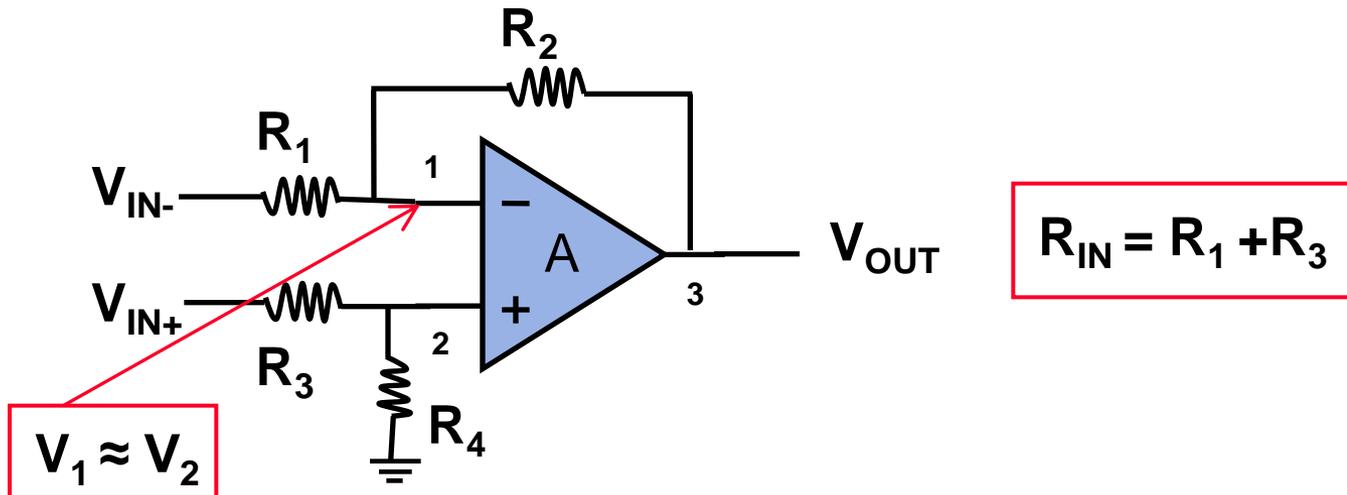




Basic Op-Amp Concepts and Terminology

Difference Amplifier

- The circuit shown is used for finding the difference of two voltages each multiplied by some constant (determined by the resistors).



- When $R_1 = R_3$ and $R_2 = R_4$, $V_{OUT} = (R_2/R_1) * (V_{IN+} - V_{IN-})$, it becomes a **Difference Amplifier**.

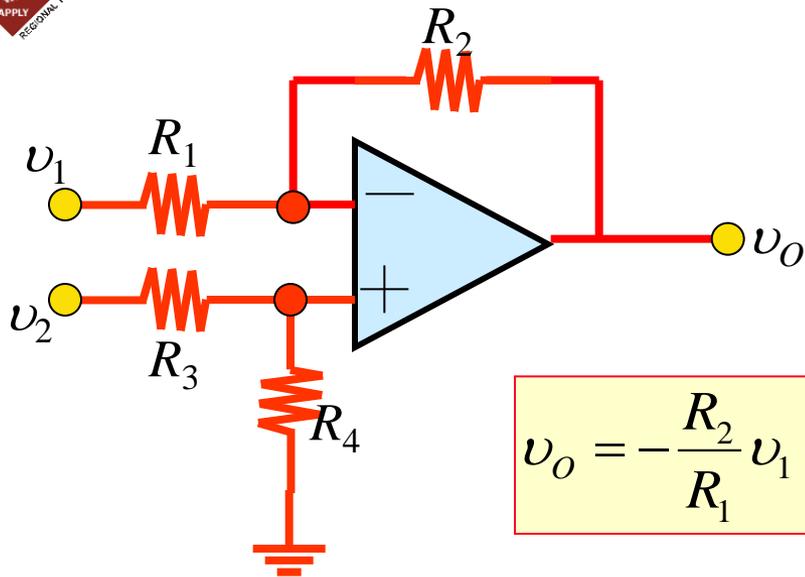
差動放大器 (difference amplifier)

差動放大器有兩個輸入訊號，利用線性疊加法：

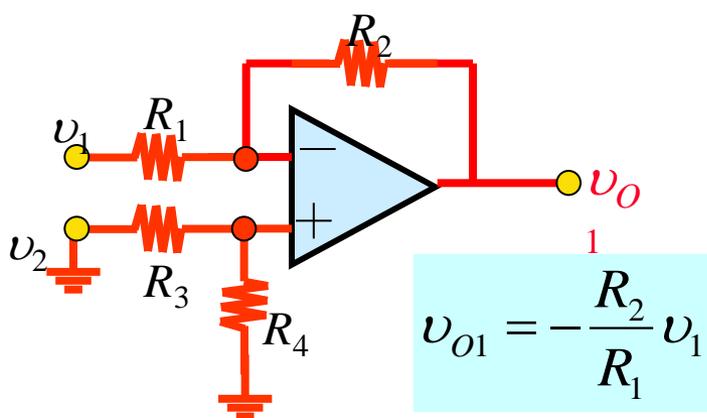
先令 $v_2 = 0$ ，得輸出 v_{O1}

再令 $v_1 = 0$ ，得輸出 v_{O2}

然後 $v_O = v_{O1} + v_{O2}$

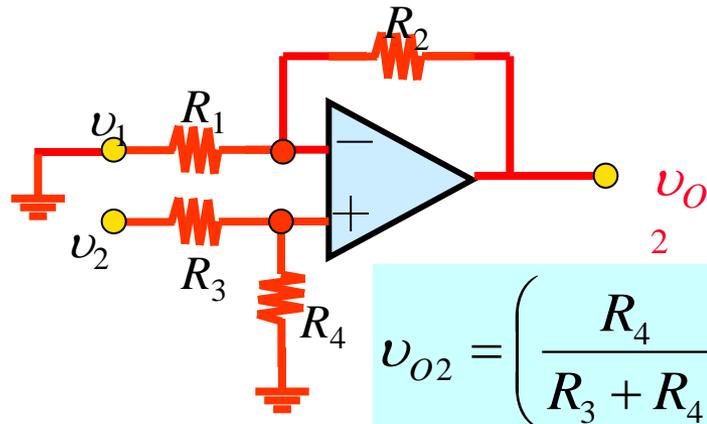


$$v_O = -\frac{R_2}{R_1} v_1 + \frac{1 + R_2 / R_1}{1 + R_3 / R_4} v_2$$



$$v_{O1} = -\frac{R_2}{R_1} v_1$$

$$R_{in1} = R_1$$



$$v_{O2} = \left(\frac{R_4}{R_3 + R_4} \right) \left(1 + \frac{R_2}{R_1} \right) v_2$$

$$R_{in2} = R_3 + R_4$$



$$v_o = -\frac{R_2}{R_1} v_1 + \frac{1 + R_2/R_1}{1 + R_3/R_4} v_2$$

我們希望輸入只有共模訊號 v_{CM} ，無差模訊號 v_d 時，輸出愈小愈好。

令 $v_1 = v_2 = v_{CM}$

共模增益為0

CMRR $\rightarrow \infty$

$$v_o = \left(-\frac{R_2}{R_1} + \frac{1 + R_2/R_1}{1 + R_3/R_4} \right) v_{CM} \rightarrow 0$$

$$\Rightarrow \frac{R_2}{R_1} = \frac{R_4}{R_3}$$

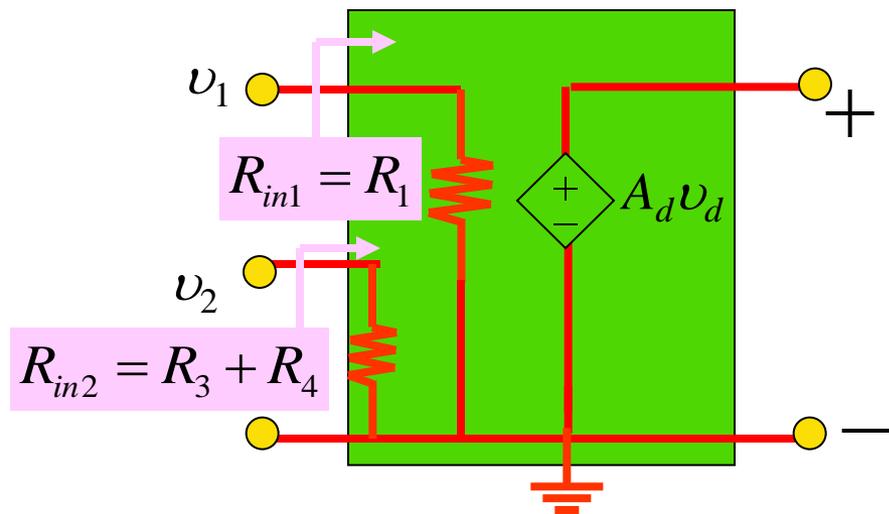
一般選擇 $R_1 = R_3$ ，
 $R_2 = R_4$

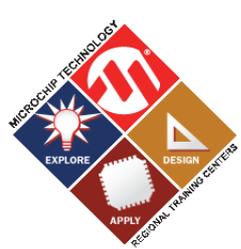
- 此差動放大器的缺點：
1. 增益不容易調整
 2. 輸入阻抗小
 3. 正負輸入端不對稱

$$\Rightarrow v_o = -\frac{R_2}{R_1} v_1 + \frac{1 + R_2/R_1}{1 + R_3/R_4} v_2$$

$$v_o = \frac{R_2}{R_1} (v_2 - v_1)$$

適當的選擇電阻後，
 $A_c = 0$ ， $A_d = R_2/R_1$

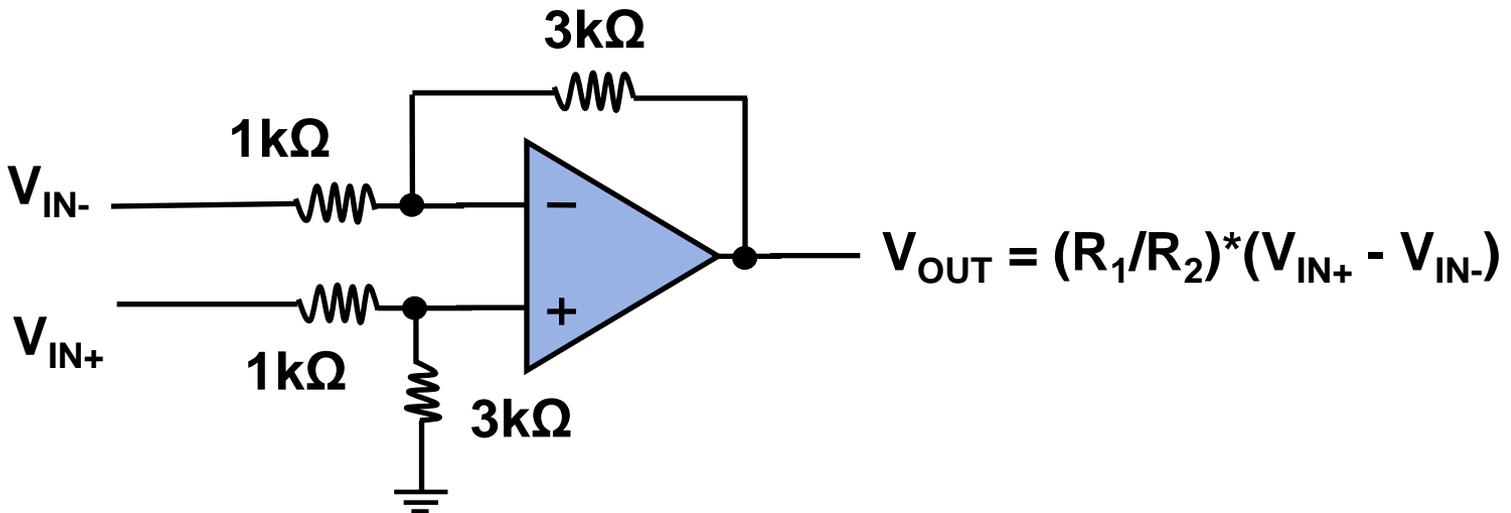




Fundamental Op Amp Circuits

Exercise #5

- Refer to the differential amplifier.
- $V_{IN+} = 1V + 0.5V \cdot \sin 2\pi ft$; $V_{IN-} = 1V - 0.5V \cdot \sin 2\pi ft$
- What is the closed loop gain G ?
- What is V_{CM} , V_{DM} and V_{OUT} ?

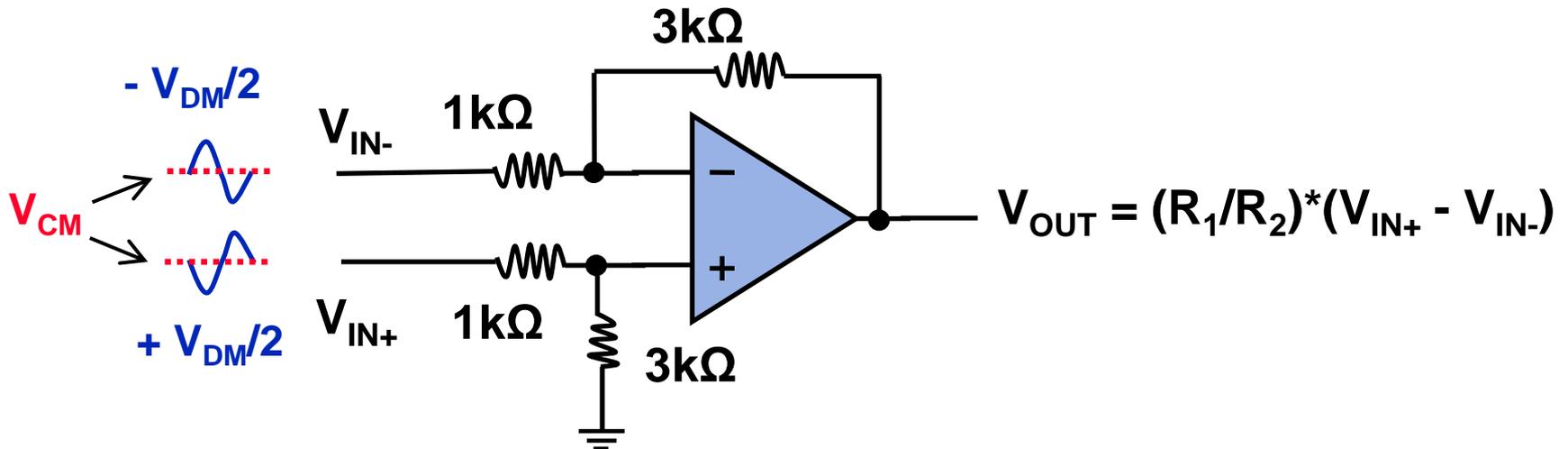




Fundamental Op Amp Circuits

Solution

- Closed loop gain: $G = 3 \text{ V/V}$
- We have $V_{IN+} = 1\text{V} + 0.5\text{V} \cdot \sin 2\pi ft$; $V_{IN-} = 1\text{V} - 0.5\text{V} \cdot \sin 2\pi ft$
 - $V_{CM} = (V_{IN-} + V_{IN+})/2 = 1\text{V}$
 - $V_{DM} = V_{IN+} - V_{IN-} = 1\text{V} \cdot \sin 2\pi ft$
 - $V_{OUT} = 3 \cdot (V_{IN+} - V_{IN-}) = 3 \cdot V_{DM} = 3\text{V} \cdot \sin 2\pi ft$





The Real World

In reality, there is no ideal op amp.

- **How to choose an op amp for your application?**

- *Various performance specifications need to be taken into consideration*

1. **Absolute Maximum Ratings**
2. **Operating Condition Ratings**
3. **Op Amp DC Specifications**
4. **Op Amp AC Specifications**

(Note: MCP601 data sheet is selected as an example in the class)



Absolute Maximum Ratings

First electrical table in our op amp data sheets

- **Absolute maximum ratings** are those limits beyond which the life of individual devices may be impaired.
- **Example: MCP601 data sheet**

Absolute Maximum Ratings †

$V_{DD} - V_{SS}$	7.0V
All inputs and outputs	$V_{SS} - 0.3V$ to $V_{DD} + 0.3V$
Difference Input voltage	$ V_{DD} - V_{SS} $
Output Short Circuit Current.....	continuous
Current at Input Pin	± 2 mA
Current at Output and Supply Pins	± 30 mA
Storage temperature	-65°C to $+150^{\circ}\text{C}$
Junction temperature	$+150^{\circ}\text{C}$
ESD protection on all pins (HBM; MM)	≥ 3 kV; 200V



Operating Condition Ratings

Operating Condition Ratings

- The op amp DC/AC specs are measured under the operating conditions
- **Beyond the operating conditions, op amp could have unsatisfactory performance.**

DC ELECTRICAL SPECIFICATIONS

Electrical Characteristics: Unless otherwise indicated, $V_{DD} = +1.8V$ to $+5.5V$, $V_{SS} = GND$, $T_A = +25^\circ C$, $V_{CM} = V_{DD}/2$, $V_{OUT} \approx V_{DD}/2$, $V_L = V_{DD}/2$, $R_L = 1\ M\Omega$ to V_L and CS is tied low. (Refer to [Figure 1-2](#) and [Figure 1-3](#)).

Parameters	Sym	Min	Typ	Max	Units	Conditions
Input Offset						
Input Offset Voltage	V_{OS}	-150	—	+150	μV	$V_{DD} = 3.0V$, $V_{CM} = V_{DD}/3$
Input Offset Drift with Temperature	$\Delta V_{OS}/\Delta T_A$	—	± 3.0	—	$\mu V/^\circ C$	$T_A = -40^\circ C$ to $+125^\circ C$, $V_{DD} = 3.0V$, $V_{CM} = V_{DD}/3$
Power Supply Rejection Ratio	PSRR	70	88	—	dB	$V_{CM} = V_{SS}$
Input Bias Current and Impedance						
Input Bias Current	I_B	—	± 1.0	100	pA	



Op Amp DC Specifications

Primary DC specifications

– Voltage Ranges

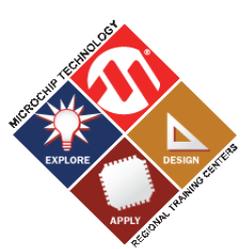
- Input Voltage Range (V_{IN} or V_{CM} or V_{DM})
- Output Voltage Swing (V_{OH} or V_{OL})

– Input Errors

- Open Loop Gain (A) /Closed Loop Gain (G)
- Input Offset Voltage (V_{OS})/Drift($\Delta V_{OS}/ \Delta T_A$)
- Common-Mode Rejection Ratio (CMRR)
- Power Supply Rejection Ratio (PSRR or PSR)
- Input Bias Current (I_B)

– Others

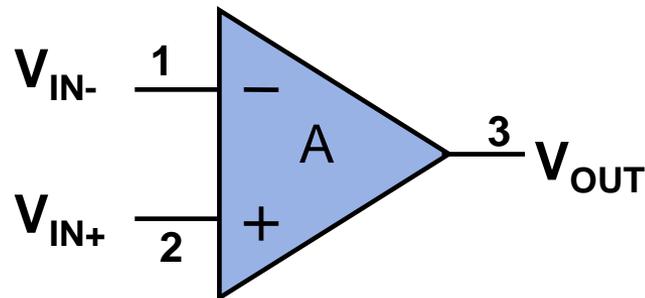
- Power Supply Requirements (V_{SS} , V_{DD} , I_Q)
- Input/Output Impedance (Z_{IN} and Z_{OUT})



Op Amp DC Specifications

Input Voltage Range (V_{IN} , V_{DM} or V_{CM})

- The inputs of op amp must stay within a certain voltage range for proper operation.
- Op amps are subject to drastic gain changes and bizarre behavior if these ranges are exceeded.
- Limited by the input stage transistors.





Op Amp DC Specifications

- **Input Voltage Range**

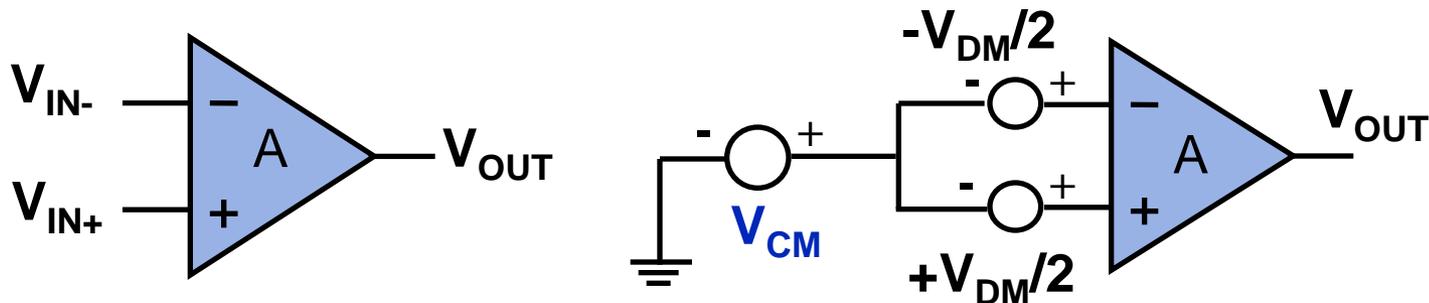
The range of acceptable voltages applied to EITHER of the input pins.

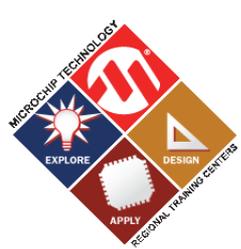
- **Difference Voltage Range $V_{DM} = V_{IN+} - V_{IN-}$**

The range of maximum voltage difference between the two inputs.

- **Common Mode Voltage Range $V_{CM} = (V_{IN+} + V_{IN-})/2$**

The range of acceptable common voltages applied to BOTH inputs simultaneously.





Op Amp DC Specifications

- **Example: MCP601 data sheet**

Electrical Specifications: Unless otherwise specified, $T_A = +25^\circ\text{C}$, $V_{DD} = +2.7\text{V}$ to $+5.5\text{V}$, $V_{SS} = \text{GND}$, $V_{CM} = V_{DD}/2$, $V_{OUT} = V_{DD}/2$ and $R_L = 100\text{ k}\Omega$ to $V_{DD}/2$.						
Parameters	Sym	Min	Typ	Max	Units	Conditions
Common Mode Input Range	V_{CMR}	$V_{SS} - 0.3$	—	$V_{DD} - 1.2$	V	

Absolute Maximum Ratings

All Inputs and Outputs $V_{SS} - 0.3\text{V}$ to $V_{DD} + 0.3\text{V}$
 Difference Input Voltage $|V_{DD} - V_{SS}|$

– Emphasis

- Stresses above those listed under “Maximum Ratings” may cause permanent damage to the device.
- Op amp is supposed to **reject** V_{CM} (common mode voltages) and **amplify** V_{DM} (difference voltage).



Op Amp DC Specs: Input

- **What Does “Rail-to-Rail Input” Mean?**
 - It means the common mode input range (V_{CMR}) can exceed the rails by several hundred millivolts
 - **Rail means supply voltage (V_{DD} and V_{SS})**

MCP6031 Datasheet

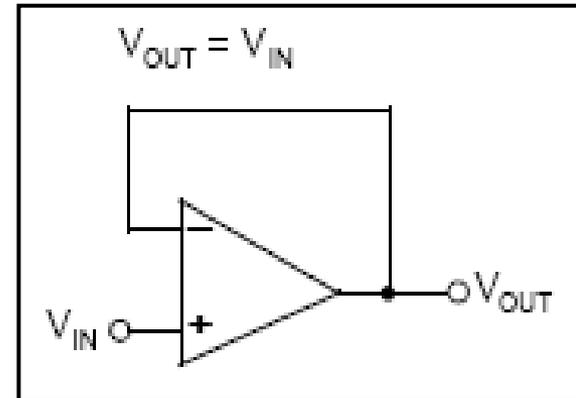
Parameters	Sym	Min	Typ	Max	Units	Conditions
Common Mode Input Voltage Range	V_{CMR}	$V_{SS} - 0.3$	—	$V_{DD} + 0.3$	V	



Op Amp DC Specs: Input

- **Application Examples**

- Voltage follower usually requires rail to rail operations at its inputs as well as its output

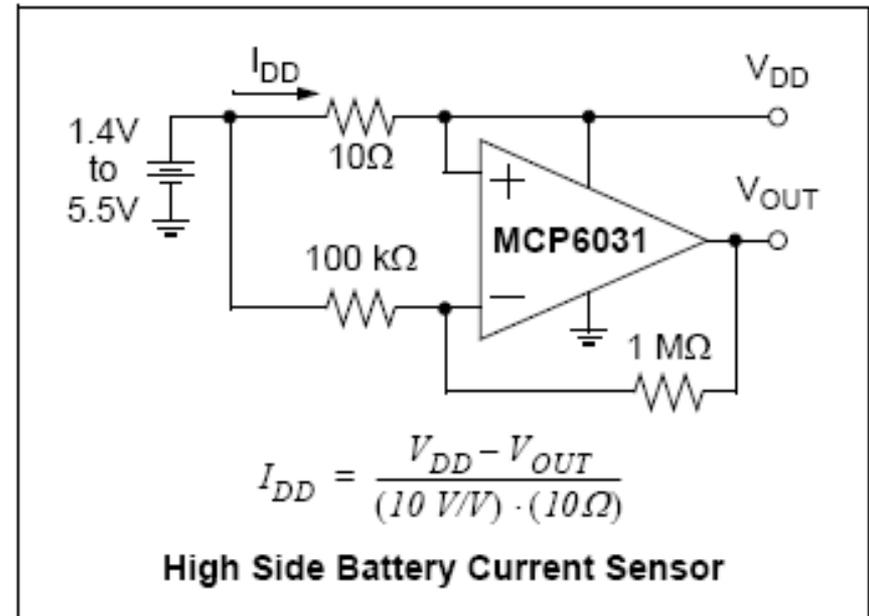


- For high-side battery

$$\frac{V_B - V_{DD}}{100k\Omega} = \frac{V_{DD} - V_{out}}{100k\Omega}$$

$$I_{DD} = \frac{V_B - V_{DD}}{10} = \frac{V_{DD} - V_{out}}{10(V/V) \cdot 10\Omega}$$

to

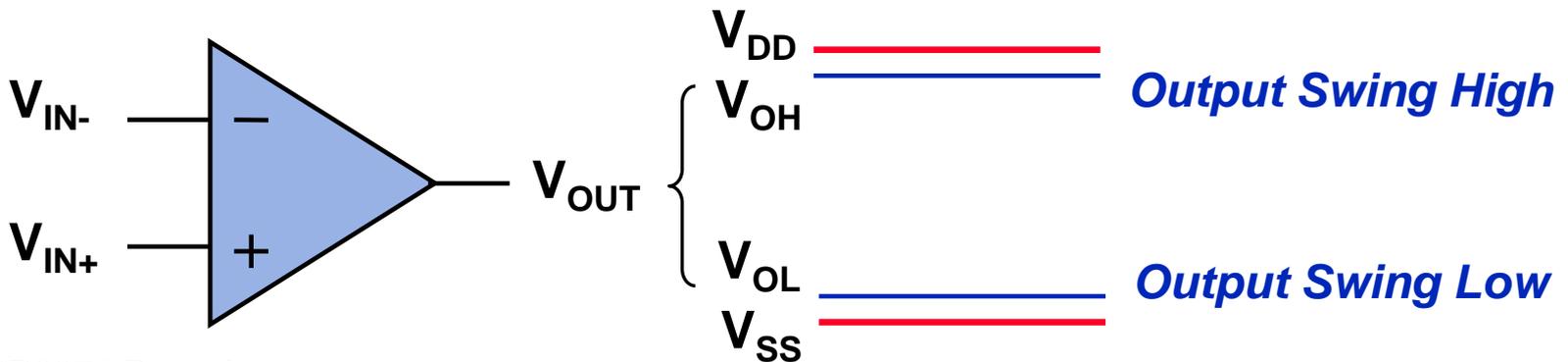




Output Related Specs

Voltage Output Swing (V_{OH} , V_{OL})

- Defines how close the op amp output can be driven to either power rail
- Rail-to-rail output means the V_{OUT} can almost, not exactly, reach the power supply rails.



MCP6071 Datasheet

Parameters	Sym	Min	Typ	Max	Units	Conditions
Maximum Output Voltage Swing	V_{OL}, V_{OH}	$V_{SS}+15$	—	$V_{DD}-15$	mV	$G = +2 V/V$, 0.5V input overdrive

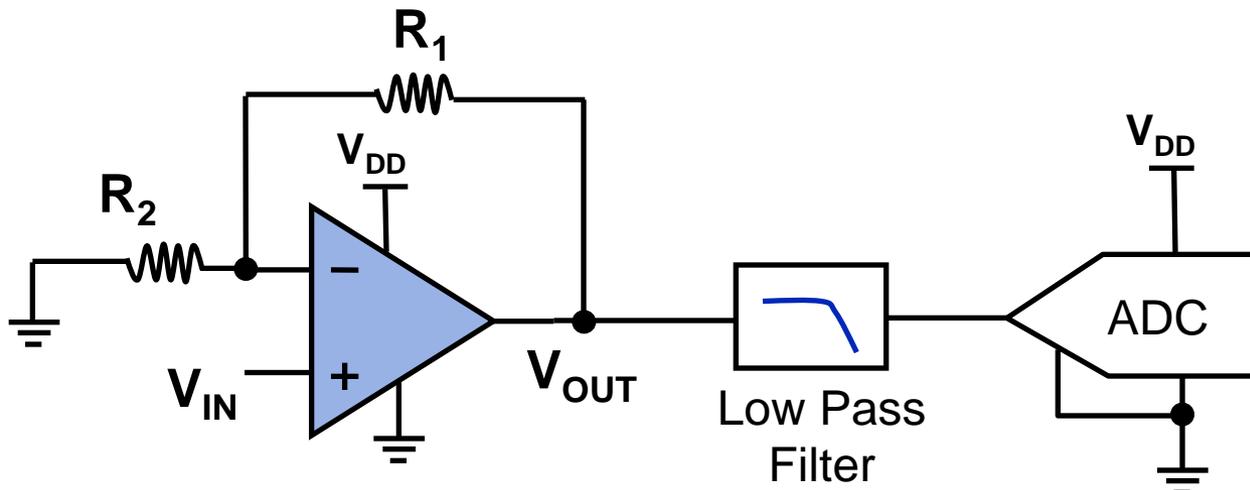


Output Related Specs

- **Application Challenge**

- Rail-to-rail output is preferred in order to maximize the output dynamic performance

- **Example:** op amp is used to drive the input of ADC, which is configured for full scale input voltage between V_{SS} and V_{DD}

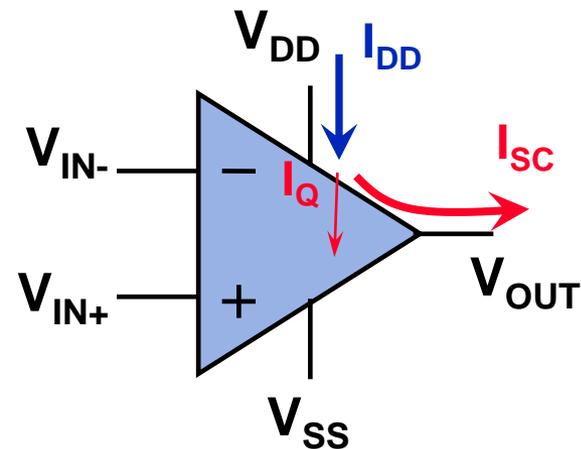




Output Related Specs

Output Short Circuit Current (I_{sc})

- It is the maximum output current that the op amp can deliver to a load



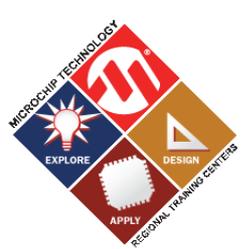
MCP6071 Datasheet

Parameters	Sym	Min	Typ	Max	Units	Conditions
Output Short-Circuit Current	I_{sc}	—	± 7	—	mA	$V_{DD} = 1.8V$
		—	± 28	—	mA	$V_{DD} = 6.0V$



Output Related Specs

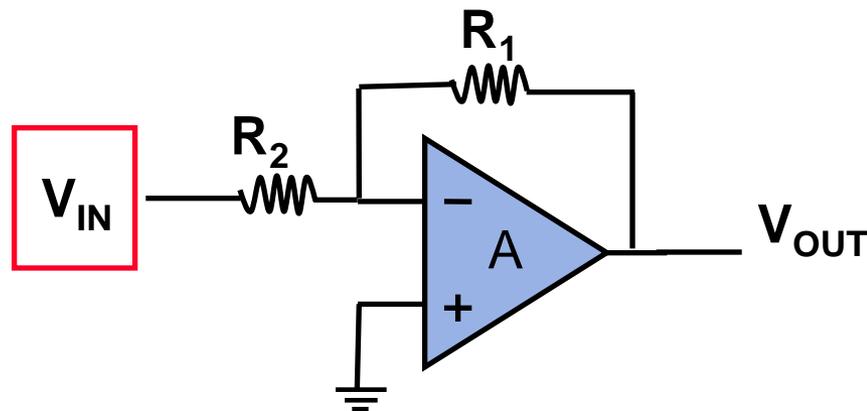
- **Application Challenge**
 - Power dissipation issue
 - **Continued short-circuit operation can cause internal junction temperature rise**
 - Limited power drive capability
 - **May not be able to drive too heavy load**
 - Output distortion when I_{OUT} is close to I_{SC}



Op Amp DC Specifications

– Application Challenge

- In a closed loop configuration, the signal input voltage range is normally much **smaller** than the op amp input voltage range.
- Using the voltage beyond the V_{IN} range, the amplifier's output will suffer from clipping.

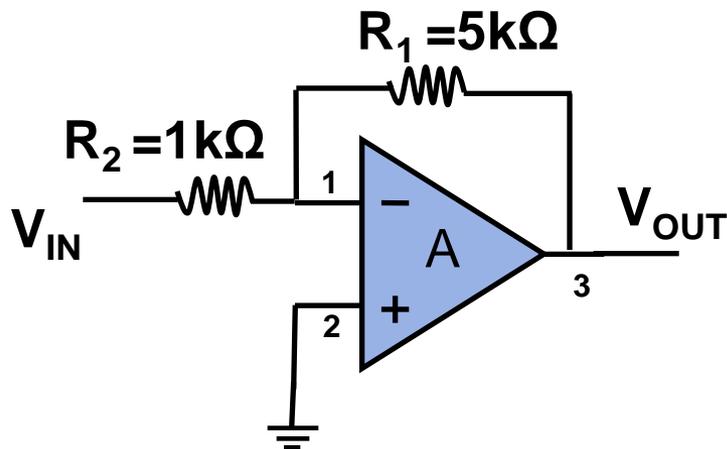




Op Amp DC Specifications

Exercise #8

- Refer to the inverting amplifier, assume $V_{DD} = +2.52V$, $V_{SS} = -2.52V$, $V_{OH} = +2.5V$, $V_{OL} = -2.5V$.
- What is the corresponding input voltage range?
For $V_{IN} = 0.1V$, $-0.2V$, $0.6V$, what is the V_{OUT} respectively?



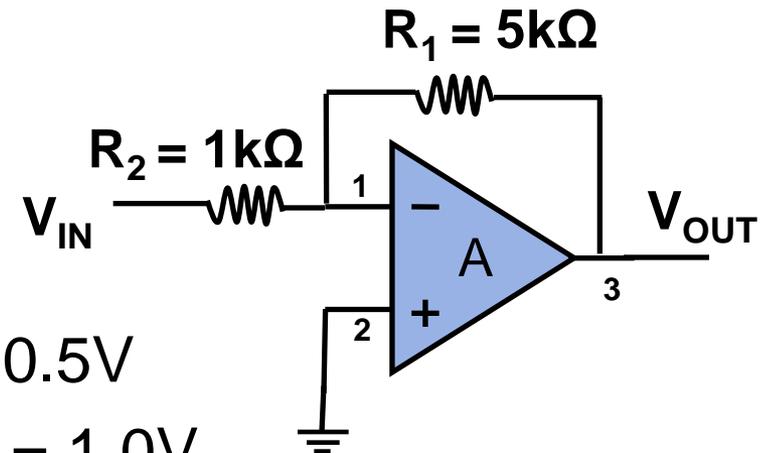
$$V_{OUT}/V_{IN} = -R_1/R_2$$



Op Amp DC Specifications

Solution #8

- $V_{OUT} = -(R_1/R_2)*V_{IN} = -5V_{IN}$
 $-2.5V \leq V_{OUT} \leq +2.5V$
So, $-0.5V \leq V_{IN} \leq +0.5V$



- $V_{IN} = 0.1V \rightarrow V_{OUT} = -5*0.1V = -0.5V$
 $V_{IN} = -0.2V \rightarrow V_{OUT} = -5*(-0.2V) = 1.0V$
- $V_{IN} = -0.6V \rightarrow V_{OUT} = -5*(-0.6V) = 3.0V? \text{ Right or Wrong?}$

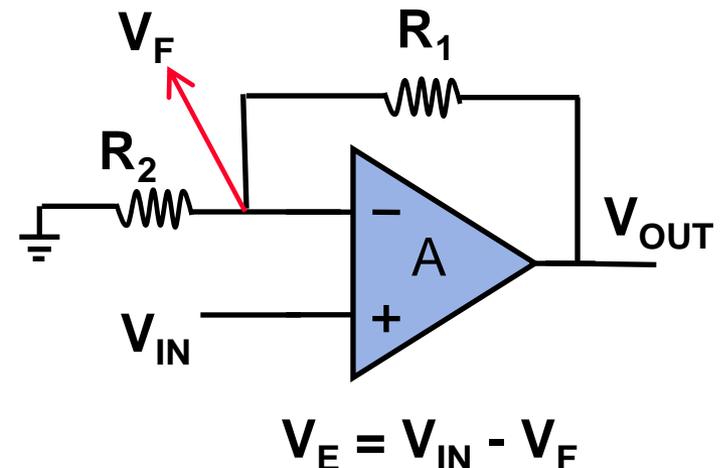
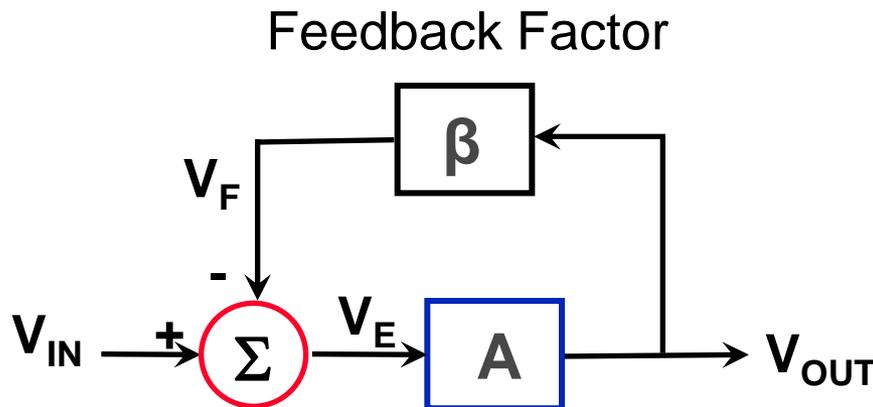
Answer: Wrong. V_{OUT} will be in positive saturation 2.5V (output clipping).



Op Amp DC Specifications

Issue : Open Loop Gain and Closed Loop Gain

- **Feedback** is a process whereby a fraction of the output signal is sensed ($V_F = \beta V_{OUT}$) and compared with the input (V_{IN}), generating a very small feedback error term ($V_E = V_{IN} - V_F$), thereby making the output feedback an accurate replica of the input.
- General feedback system

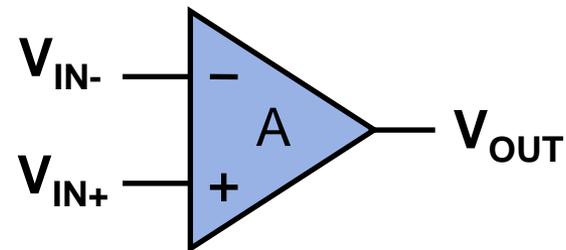
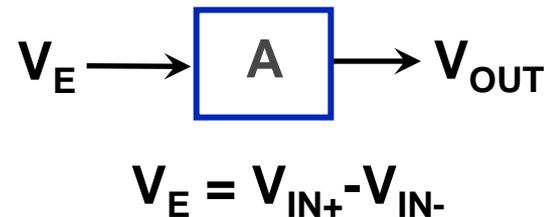
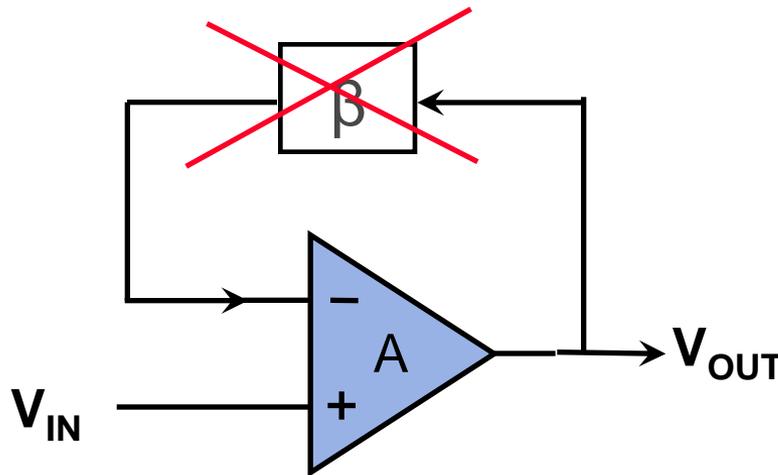




Op Amp DC Specifications

Open Loop Gain (A)

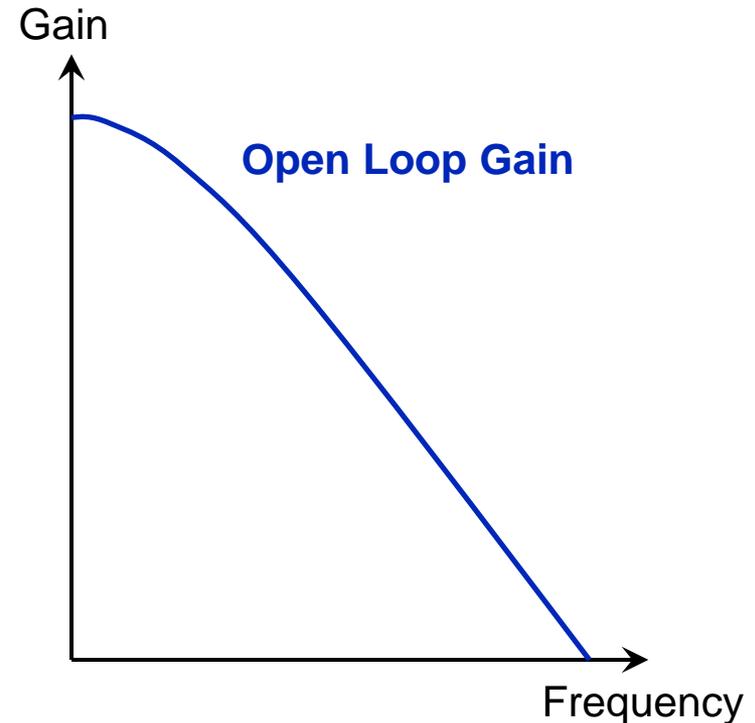
- Open loop gain of an op amp is the gain obtained when **no feedback** is used in the circuit.
- $A = V_{OUT}/V_E$ where $V_E = V_{IN+} - V_{IN-}$





Op Amp DC Specifications

- Ideally, the open loop gain should be infinite.
- **In reality, the open loop gain is less than ideal at DC ranging from 95dB to 120dB. (10^5 to 10^6)**
- Open loop gain will decrease when the frequency of the input signal increases.
- **It is a function of frequency.**



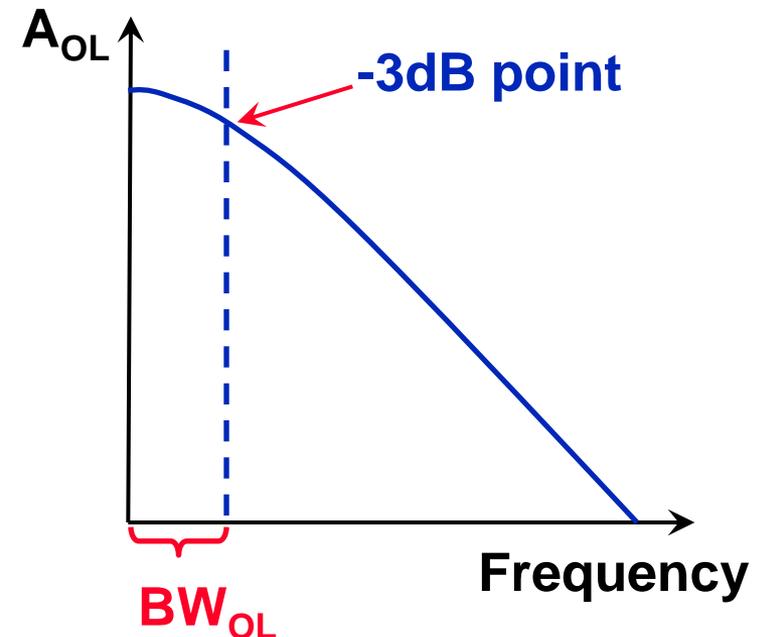


Op Amp DC Specs: Output

- **Emphasis**

- **Open Loop Gain Bandwidth (BW_{OL})**

- **It is measured at the point where gain falls to 0.707 of maximum gain (-3dB bandwidth)**
- **-3dB bandwidth is also called half-power bandwidth**





Op Amp DC Specifications

- **Example: MCP601 data sheet**

Electrical Characteristics: Unless otherwise indicated, all limits are specified for $V_{DD} = +1.4\text{ V to }+5.5\text{ V}$, $V_{SS} = \text{GND}$, $T_A = 25\text{ }^\circ\text{C}$, $V_{CM} = V_{DD}/2$, $R_L = 1\text{ M}\Omega$ to $V_{DD}/2$, and $V_{OUT} \sim V_{DD}/2$						
Parameters	Sym	Min	Typ	Max	Units	Conditions
Open Loop Gain: DC Open Loop Gain (large signal)	A_{OL}	95	115	—	dB	$R_L = 50\text{ k}\Omega$ to $V_{DD}/2$, $100\text{ mV} < V_{OUT} < (V_{DD} - 100\text{ mV})$

- Decibel (dB) can be translated into volts per volts with the formula

$$A(\text{dB}) = 20 \log \left(\frac{V_{OUT}}{V_{IN}} \right)$$



Op Amp DC Specifications

Example:

- If the open loop gain is 100dB, then

$$100 \text{ dB} = 20 \log \left(\frac{V_{\text{OUT}}}{V_{\text{IN}}} \right) \implies \frac{V_{\text{OUT}}}{V_{\text{IN}}} = 10^{(100/20)} = 10^5$$

- If the open loop gain is 10^6 , then

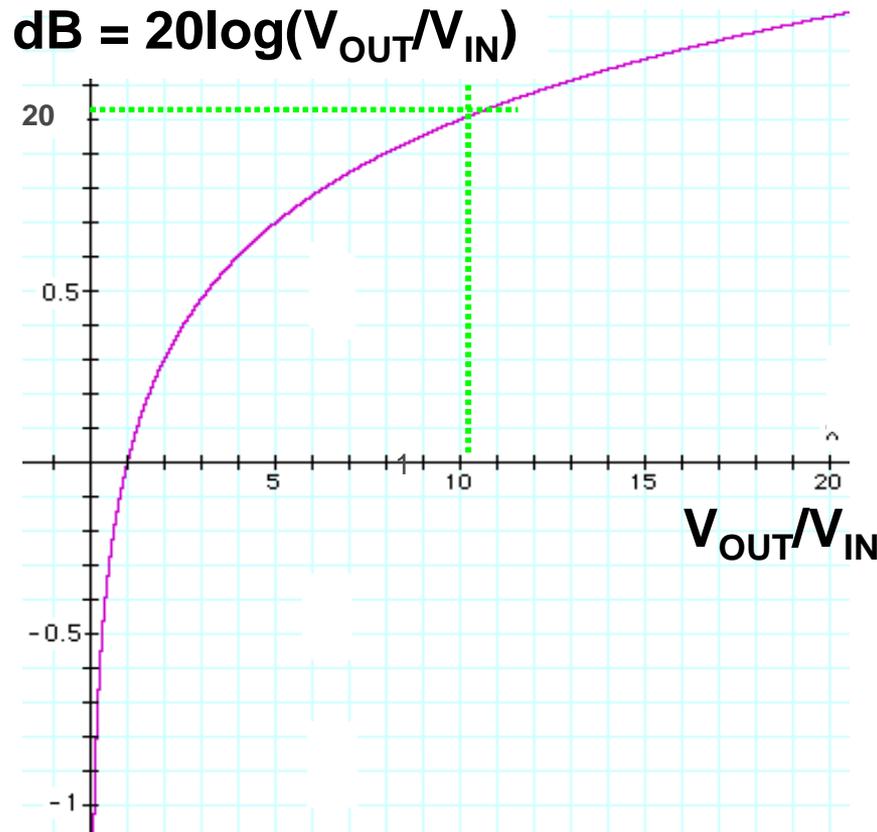
$$20 \log \left(\frac{V_{\text{OUT}}}{V_{\text{IN}}} \right) = 20 \log(10^6) = 120 \text{ dB}$$

- Decibels are useful because they allow even very large or small ratios to be represented with a conveniently small number (similar to scientific notation).



Op Amp DC Specifications

- Graph: how dB relates to the linear response



dB level	Ratio (V/V)
-60dB	1/1000
-40dB	1/100
-20dB	1/10
0dB	1
20dB	10
40dB	100
80dB	1.0 x 10 ⁴
120dB	1.0 x 10 ⁶



Op Amp DC Specifications

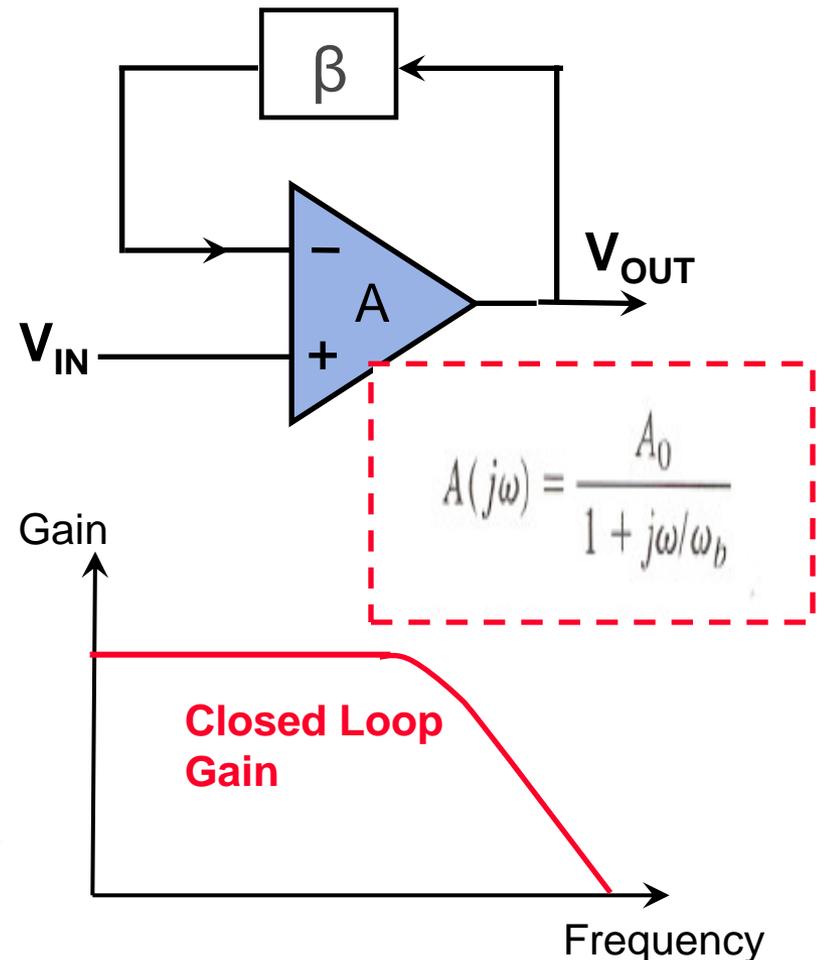
Closed Loop Gain (G)

- It, a transfer function, represents the relation between the input and output of a system.

$$G = \frac{A}{1 + \beta A}$$

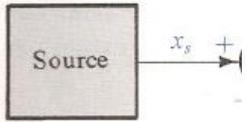
- **A**: open loop gain
- **β** : feedback factor
- **βA** : loop gain

- **G** is a function of frequency.





Feedback System Merits



負回饋之優點

1. 增益的穩定性提高
2. 帶寬的增大
3. 失真率的降低
4. 輸出、輸入電阻的改善

$$A_f \equiv \frac{x_o}{x_s} = \frac{A}{1 + A\beta}$$

Impedence Improvement

$$R_{if} = R_i(1 + A\beta) \quad R_{of} = \frac{R_o}{1 + A\beta}$$

Gain Desensi

Bandwidth Exten

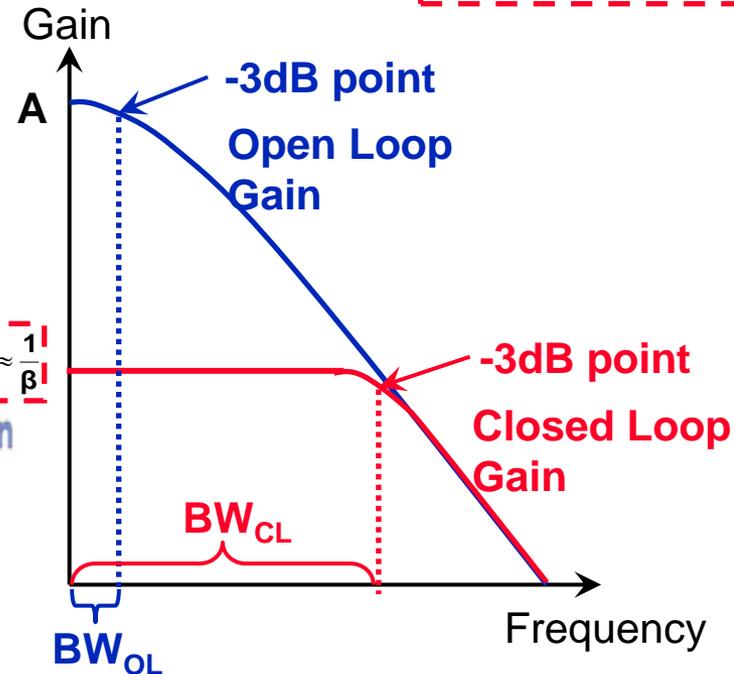
$$A_f(s) = \frac{A(s)}{1 + \beta A(s)} = \frac{A_M/(1 + A_M\beta)}{1 + s/\omega_H(1 + A_M\beta)}$$

$$|G| = \left| \frac{A}{1 + \beta A} \right| \approx \frac{1}{\beta}$$

Reduction in Nonlinear Distortion

Noise Reduction

$$\frac{S}{N} = \frac{V_s}{V_n} A_2$$





Op Amp DC Specifications

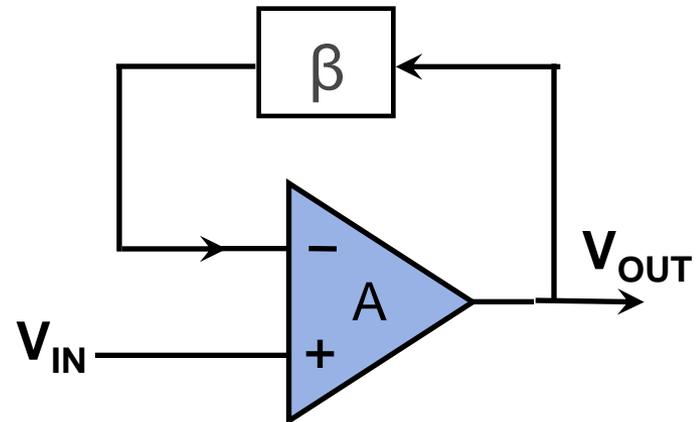
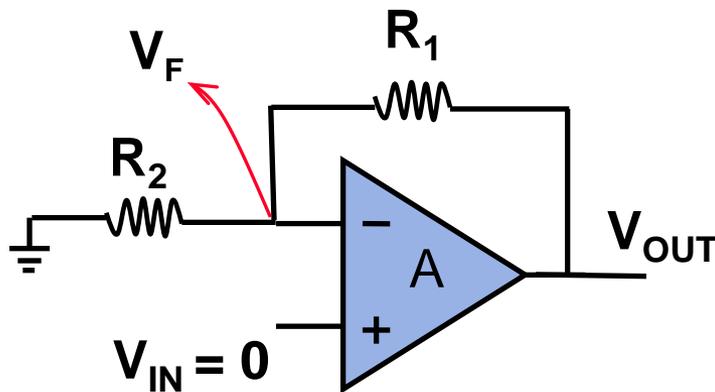
- **Open Loop vs. Close Loop (Comparison)**
 - **Open Loop**
 - Very high gain and poor stability.
 - Internal “noise” are amplified by the same gain factor.
 - Used in comparators and oscillators.
 - **Closed Loop**
 - Reduces and desensitizes the gain, good stability.
 - Internal “noise” amplified by the **noise gain ($G_N = 1/\beta$)**.
 - Most amplifiers are used in this configuration.
 - **Op amps are normally not used in open loop mode.**



Op Amp DC Specifications

Discussion: Feedback Factor β

- Feedback factor is the fraction of the amplifier output signal fed back to the amplifier input.
- It is determined by the feedback network that is connected around the amplifier.

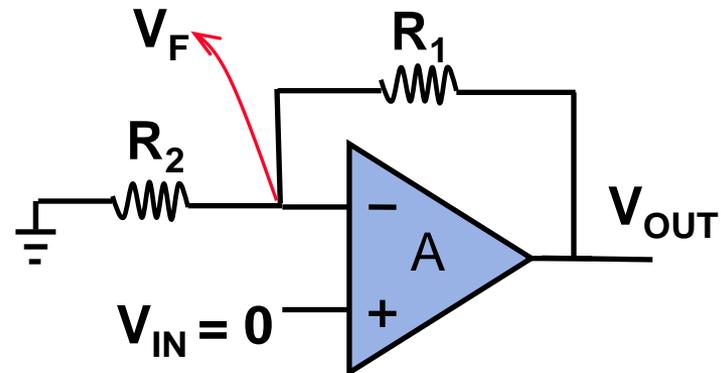
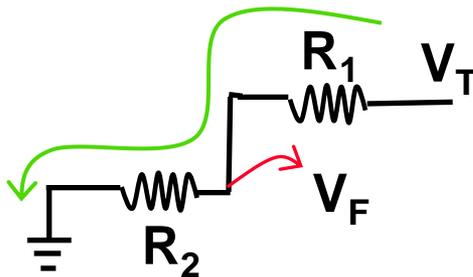




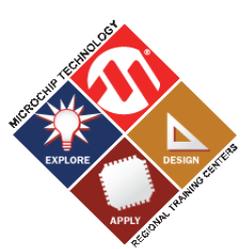
Op Amp DC Specifications

– Feedback factor calculation

- Break the loop at some points, only consider feedback network.
- Set $V_{IN} = 0$, inject a test signal V_T , then get the value of feedback signal V_F , $\beta = V_F/V_T$.



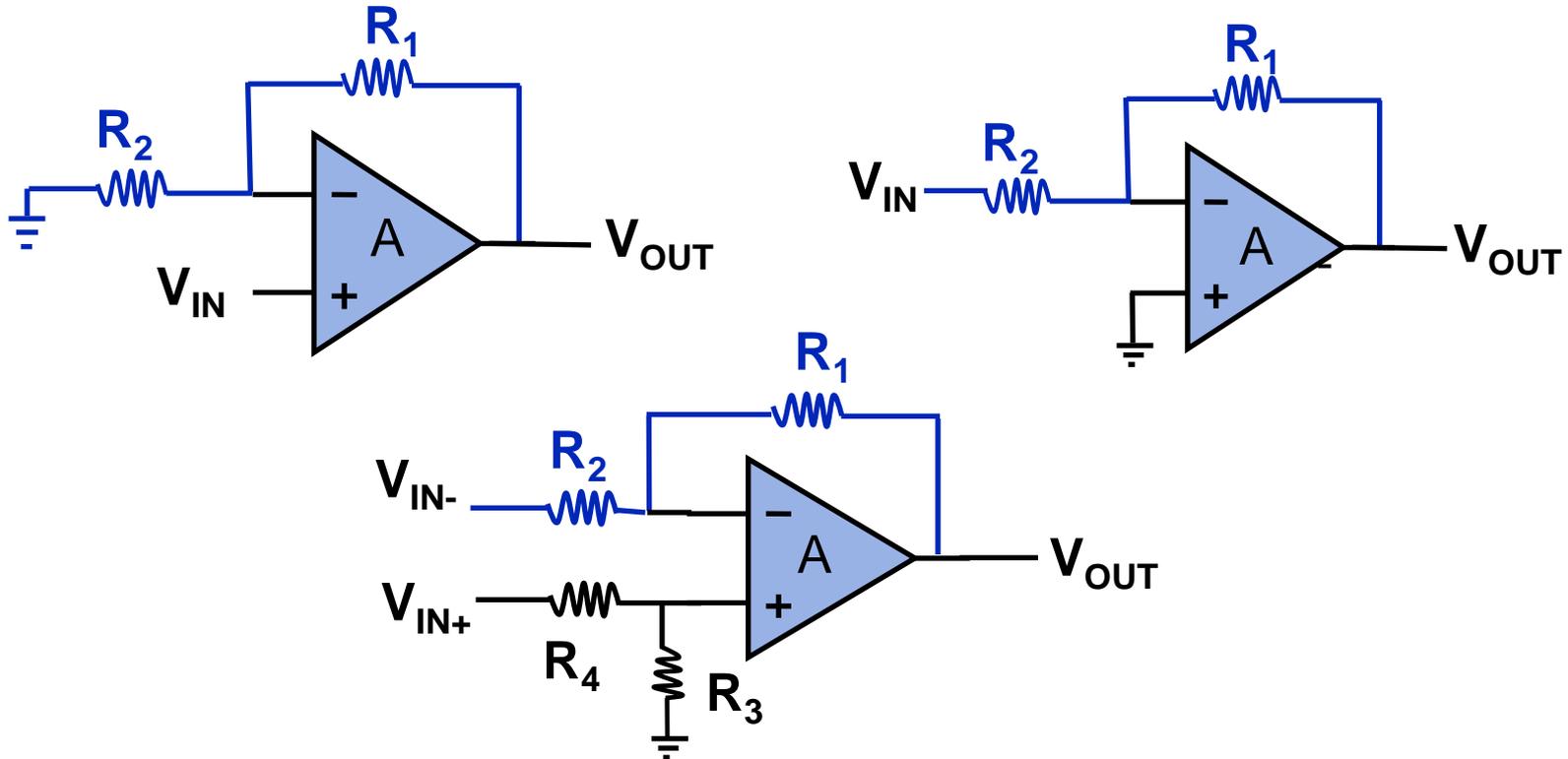
- As a general guideline, the feedback factor of an op amp circuit equals the **voltage divider ratio** of the feedback network.



Op Amp DC Specifications

Summary

- **General guideline:** The feedback factor (β) of an op amp circuit **equals** the **voltage divider ratio** of the feedback network.

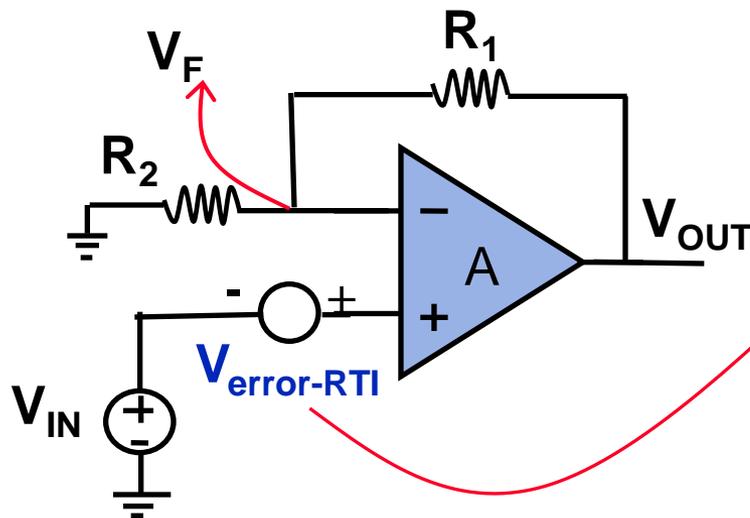




Op Amp DC Specifications

Emphasis: General Error Analysis

- $1/\beta$ is called **Noise Gain (G_N)**
- Internal noise is amplified by noise gain G_N .
- Internal noise manifests itself as input error signal.



Error Source: the error signals generated by non-ideal op amp specifications, such as V_{OS} , I_B , CMRR, etc.



Op Amp DC Specifications

$$\beta = \frac{R_2}{R_1 + R_2} \Rightarrow \frac{1}{\beta} = 1 + \frac{R_1}{R_2}$$

Non-Inverting $G = 1 + \frac{R_1}{R_2} = \frac{1}{\beta}$

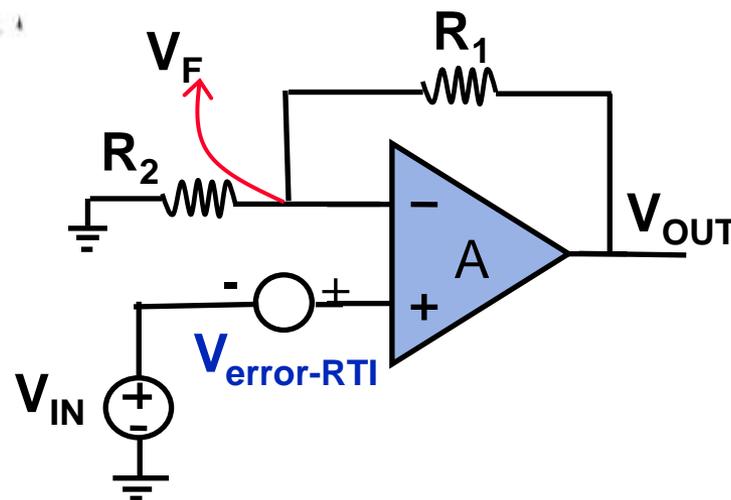
Inverting $G = -\frac{R_1}{R_2} = 1 - \frac{1}{\beta}$

Difference $G = \frac{R_1}{R_2} = \frac{1}{\beta} - 1$

Feedback Factor
用Gain表示之關係

and output errors

error-RTI



Recall:

Non-inverting amplifier: $G = 1/\beta$

Inverting amplifier: $|G| = (1/\beta) - 1$

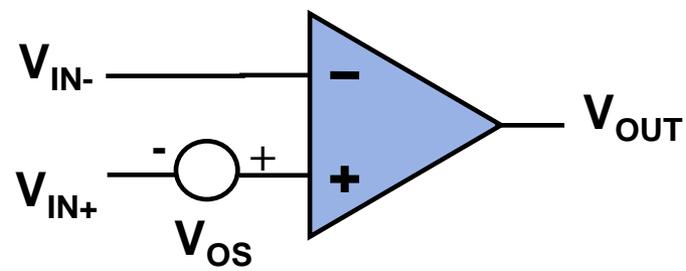
Difference amplifier: $G = (1/\beta) - 1$



Input Related Specs

Input Offset Voltage (V_{OS})

- Defines the DC error voltage which exists in the input stage of an op amp and can be either polarity.
- Circuit model for an op amp with V_{OS}
 - A dc source of value V_{OS} is placed in series with the non-inverting input of an offset-free op amp



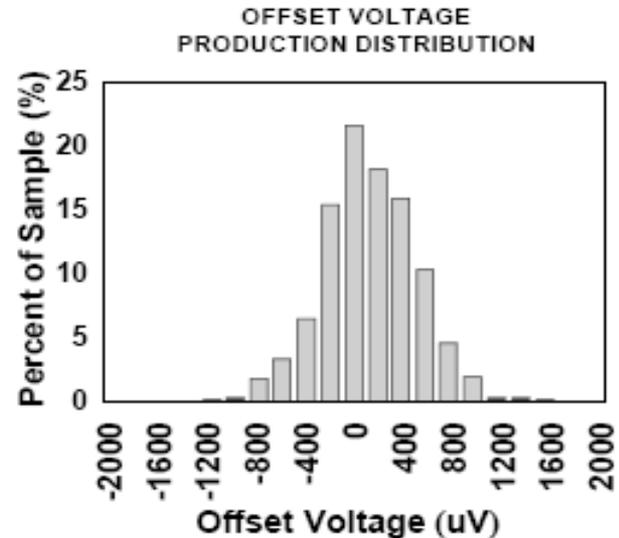
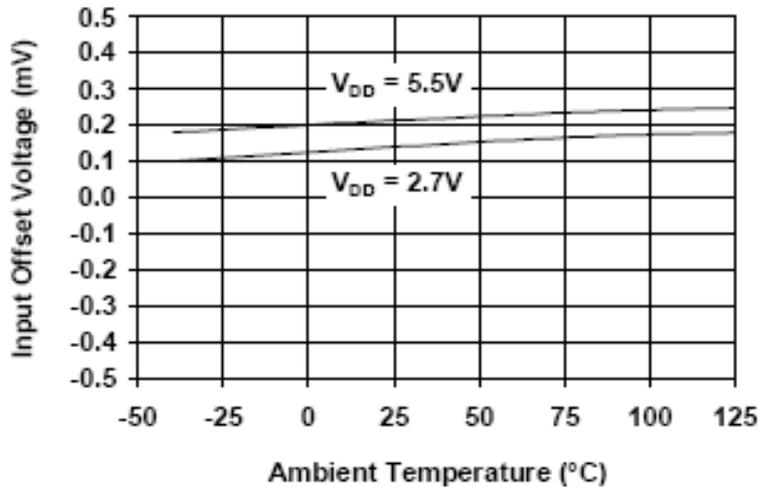
MCP6V01 Auto-zeroed Op Amp Datasheet

Parameters	Sym	Min	Typ	Max	Units	Conditions
Input Offset Voltage	V_{OS}	-2.0	—	+2.0	μV	$T_A = +25^\circ C$ (Note 1)



Op Amp DC Specifications

- V_{OS} varies with ambient temperature.
- V_{OS} typical value is the mean value of the normal distribution.



- **Example: MCP601 data sheet**

Electrical Specifications: Unless otherwise indicated, $T_A = +25^\circ C$, $V_{DD} = +2.7V$ to $+5.5V$, $V_{SS} = GND$, $V_{CM} = V_{DD}/2$, $V_{OUT} \approx V_{DD}/2$, $R_L = 100\text{ k}\Omega$ to $V_{DD}/2$ and $C_L = 50\text{ pF}$.

Parameters	Sym	Min	Typ	Max	Units	Conditions
Input Offset Voltage	V_{OS}	-2	± 0.7	+2	mV	
Input Offset Temperature Drift	$\Delta V_{OS}/\Delta T_A$	—	± 2.5	—	$\mu V/^\circ C$	$T_A = -40^\circ C$ to $+125^\circ C$

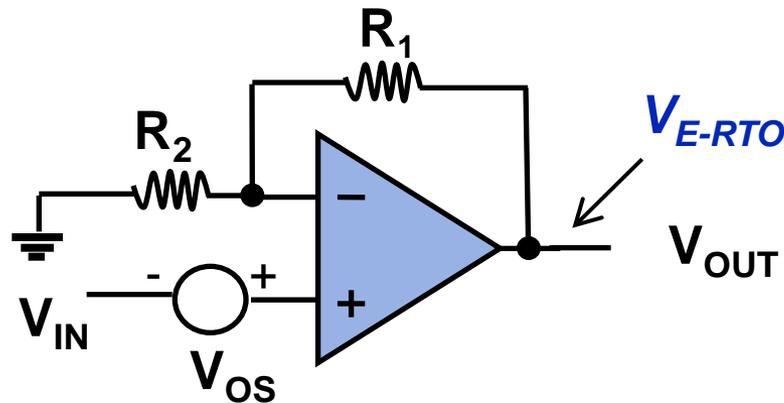


Input Related Specs

- **DC Error Analysis (due to V_{OS})**
 - In a closed loop system, the input offset voltage V_{OS} will be amplified by noise gain G_N .

$$V_{E-RTO} = G_N * V_{OS}$$

- **The lower the V_{OS} , the smaller the V_{E-RTO}**





Op Amp DC Specifications

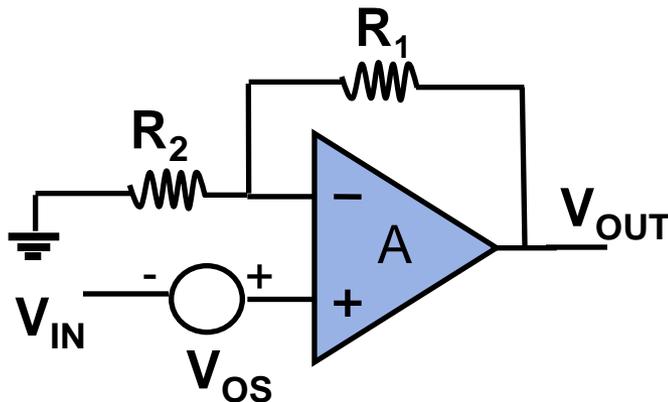
- **Application Challenge**

- Low V_{OS} is preferred in an high gain amplifier
 - **good accuracy and maximizing the output dynamic range**

- Assume input offset voltage is 1mv, $R_1 = 10k\Omega$, $R_2 = 100\Omega$. Express V_{OUT} by using V_{IN} and V_{OS} .

- What is the DC error at the output?

High Gain ex. $\frac{10000}{100} = 100$



Hint:

$$V_{\text{error-RTO}} = G_N * V_{OS}$$

$G_N = G$ for non-inverting amplifier

$$G = 1 + R_1/R_2$$

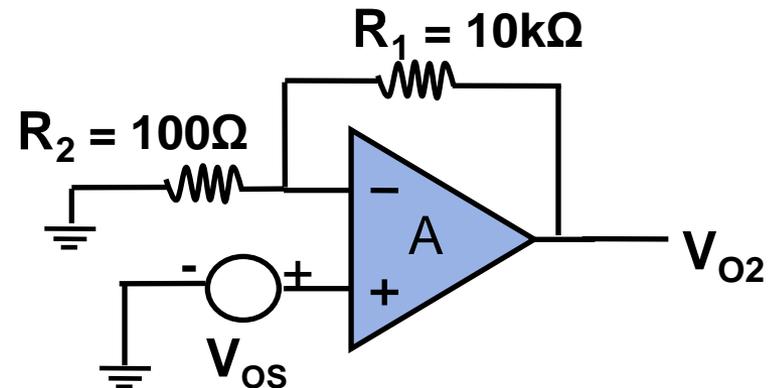
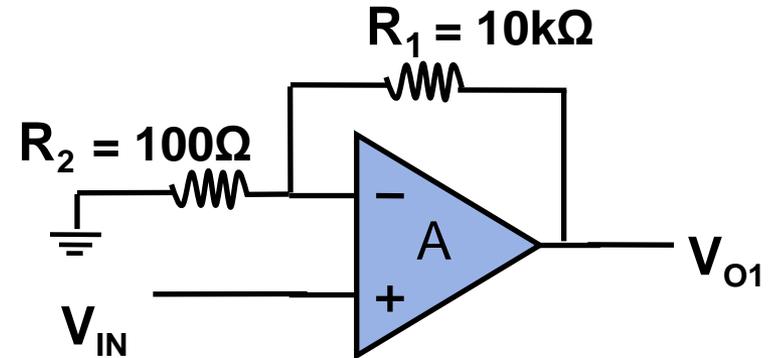


Op Amp DC Specifications

Solution #15

- **Superposition Principle**

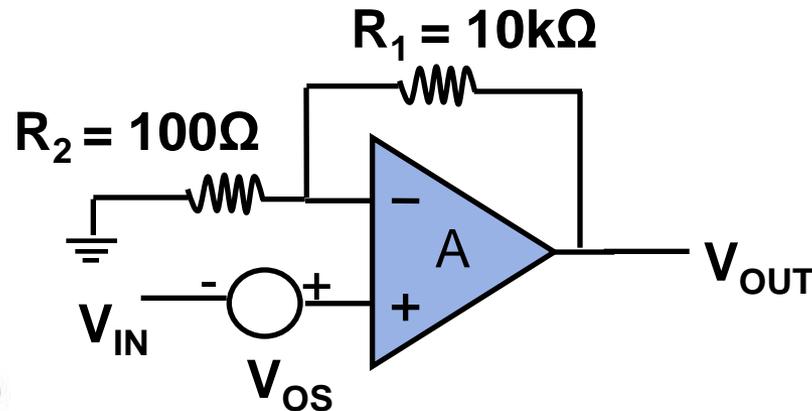
- First, let $V_{OS} = 0$
 - Find the corresponding output voltage V_{O1}
 - $V_{O1} = V_{IN}(1+R_1/R_2)$
- Next, let $V_{IN} = 0$,
 - Find the corresponding output voltage V_{O2}
 - $V_{O2} = V_{OS}(1+R_1/R_2)$





Op Amp DC Specifications

- Finally, $V_{OUT} = V_{O1} + V_{O2} = (1 + R_1/R_2) * (V_{IN} + V_{OS})$
 - For $V_{OS} = 1\text{mV}$, we have $V_{O2} = 1\text{mV} * (1 + 100) = 101\text{mV}$
 - In a 5V system, the DC error 101mV lessens the output dynamic range by $101\text{mV}/5\text{V} \approx 2\%$.



$$\frac{5\text{V}}{1024} = 5\text{mV}$$

$$\frac{101\text{mV}}{5\text{mV}} = 20 \text{ (steps or LSB)}$$

考慮 ADC 造成之誤差



Take a Break

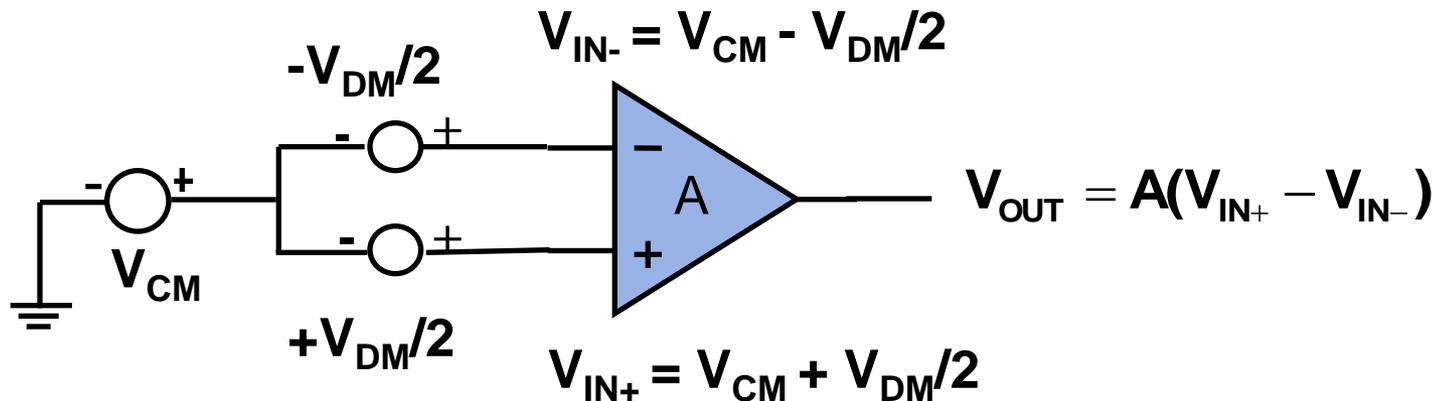
http://ezphysics.nchu.edu.tw/prophys/electron/new_page_7.htm



Op Amp DC Specifications

Common Mode Rejection Ratio (CMRR)

- CMRR is the ratio of differential gain (A_{DM}) to common mode gain (A_{CM}).
- It is a measure of the capability of an op amp to reject a signal that is common to both inputs.
- Ideally, CMRR is infinite.





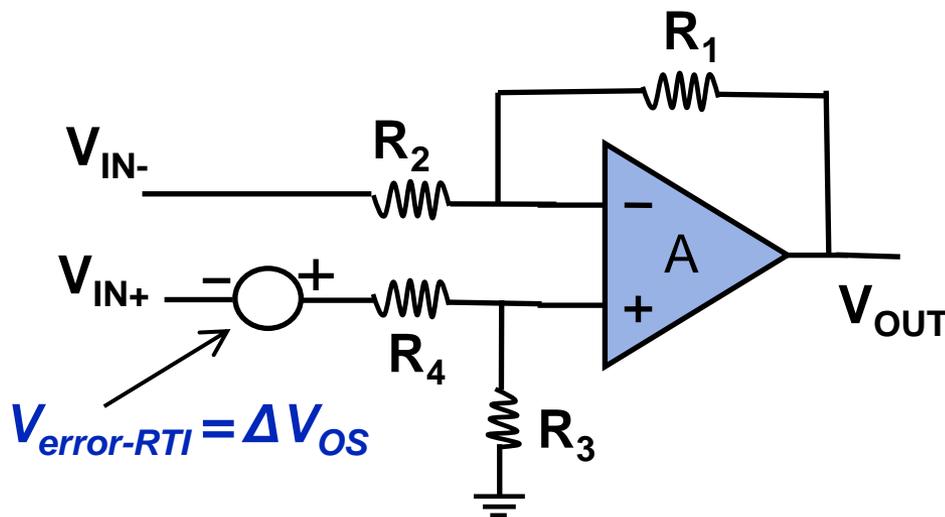
Op Amp DC Specifications

– Refer To Input

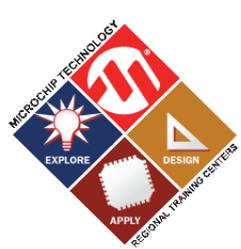
- Practically, CMRR is not infinite. In a closed loop system, an amplifier manifests ΔV_{CM} as input voltage error ΔV_{OS} .
- This error is described by the formula:

$$\text{CMRR (dB)} = 20\log(A_{DM}/A_{CM}) = 20\log(\Delta V_{CM}/\Delta V_{OS})$$

where $A_{DM} = \Delta V_{OUT}/\Delta V_{OS}$, $A_{CM} = \Delta V_{OUT}/\Delta V_{CM}$



$$\begin{aligned} V_{error-RTO} &= G_N * V_{error-RTI} \\ &= (1+G) * V_{error-RTI} \\ &= (1+R_1/R_2) * V_{error-RTI} \end{aligned}$$



Op Amp DC Specifications

- **Example: MCP601 data sheet**

Electrical Characteristics: Unless otherwise indicated, all limits are specified for $V_{DD} = +1.4\text{ V to }+5.5\text{ V}$, $V_{SS} = \text{GND}$, $T_A = 25\text{ }^\circ\text{C}$, $V_{CM} = V_{DD}/2$, $R_L = 1\text{ M}\Omega$ to $V_{DD}/2$, and $V_{OUT} \sim V_{DD}/2$						
Parameters	Sym	Min	Typ	Max	Units	Conditions
Common Mode Rejection Ratio	CMRR	75	90	—	dB	$V_{DD} = 5.0\text{V}$, $V_{CM} = -0.3\text{V to }3.8\text{V}$

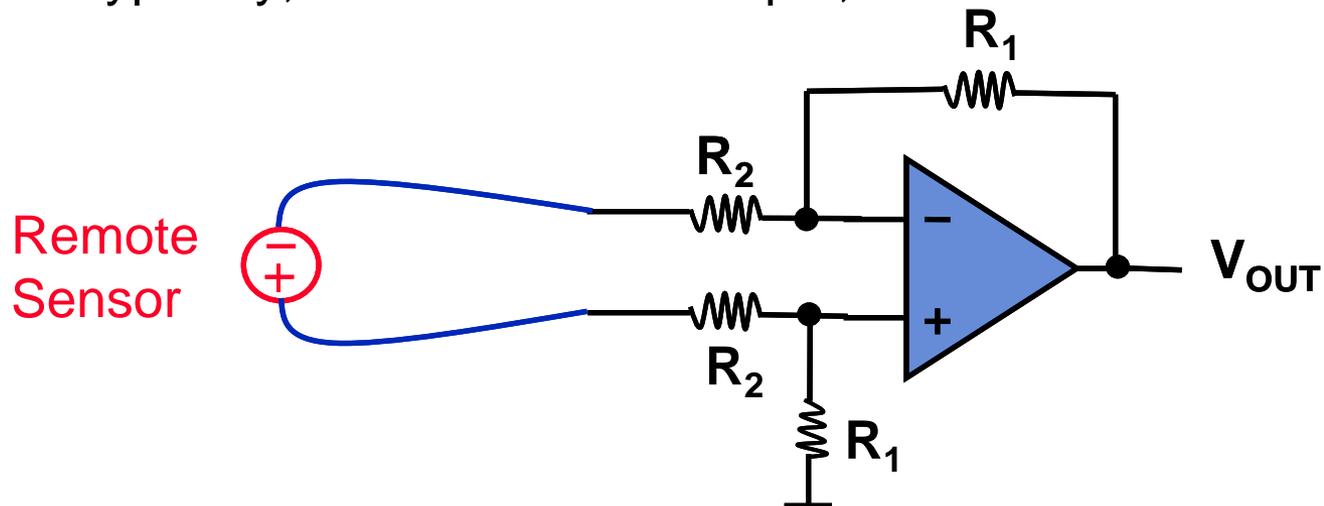
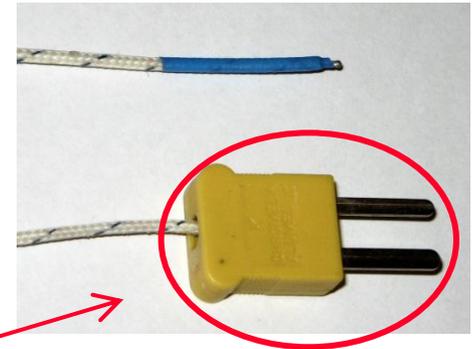
- **Application Challenge**
 - The lower the CMRR, the larger the effect on the output signal.
 - A value of 70dB is adequate for most of applications.

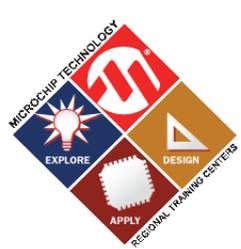


Input Related Specs

- **Application Challenge**

- High CMRR is preferred for most applications with remote sensors
- **Remote sensors with differential output are subject to high common mode noise.**
- Typically, such as thermocouple, etc

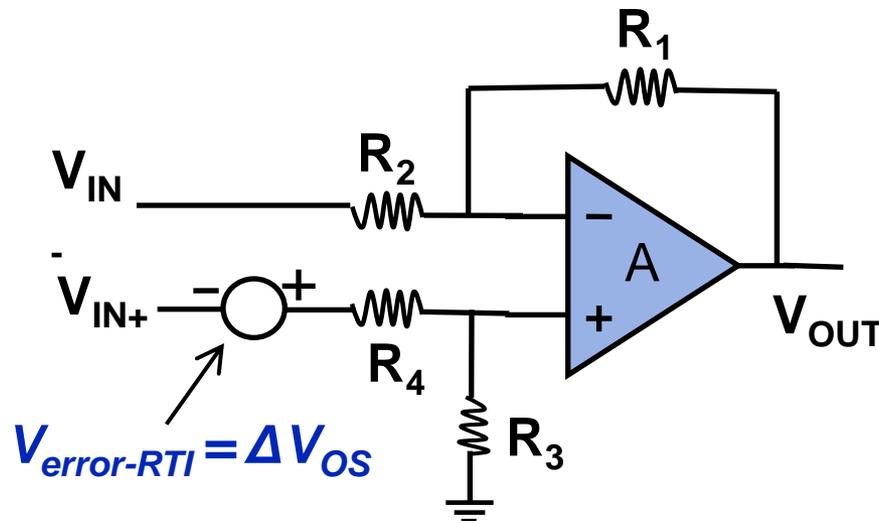




Op Amp DC Specifications

Exercise #16

- Refer to the **difference amplifier**. Assume **closed loop gain $G = 100$** , $CMRR = 80\text{dB}$. ΔV_{CM} , the change of the amplifier input CM level, is 1.0V .
- What is the error at the output? Repeat the calculation for $CMRR = 60\text{dB}$. Recall: **$CMRR(\text{dB}) = 20\log(\Delta V_{CM}/\Delta V_{OS})$**



$$\begin{aligned}
 V_{\text{error-RTO}} &= G_N * V_{\text{error-RTI}} \\
 &= (1+G) * V_{\text{error-RTI}} \\
 &= (1+R_1/R_2) * V_{\text{error-RTI}}
 \end{aligned}$$

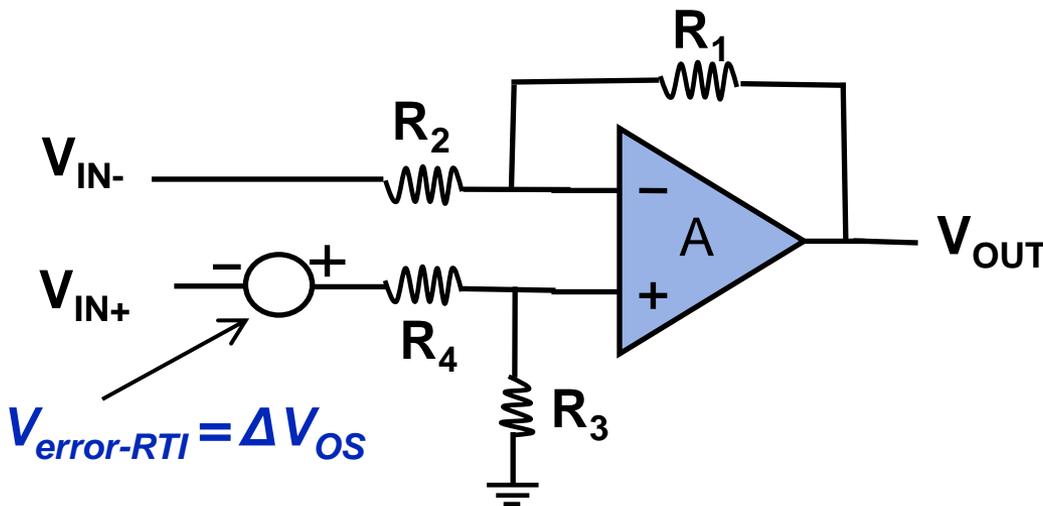


Op Amp DC Specifications

Solution #16

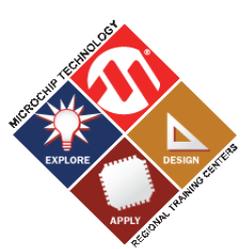
- $CMRR = 20\log(\Delta V_{CM}/\Delta V_{OS})$, $CMRR = 80\text{dB}$, $\Delta V_{CM} = 1.0\text{V}$
 $\rightarrow 80\text{dB} = 20\log(1.0\text{V}/\Delta V_{OS}) \rightarrow \Delta V_{OS} = 0.1\text{mV}$.
- $V_{\text{error-RTO}} = G_N * V_{\text{error-RTI}} = (1+R_1/R_2) * V_{\text{error-RTI}}$
 $= 101 * 0.1\text{mV} = \mathbf{10.1\text{mV}}$.

The output range will be decreased by 10.1mV.



$V_{\text{error-RTI}} = \Delta V_{OS}$

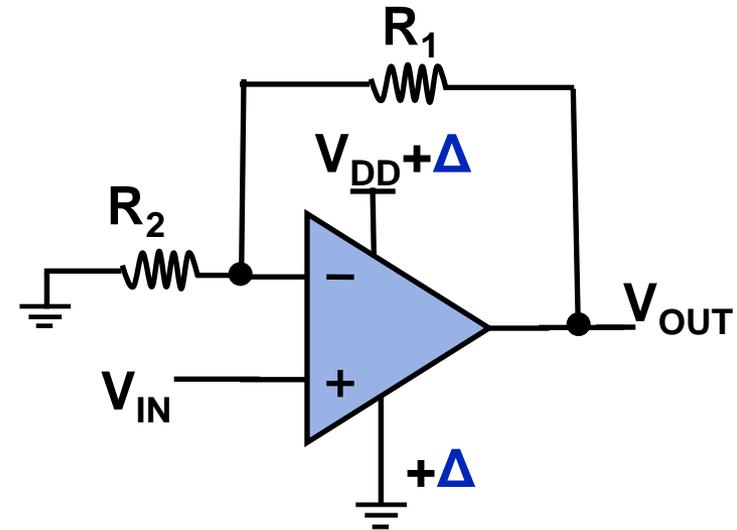
If $CMRR = 60\text{dB}$, the output range will be decreased by $\mathbf{101\text{mV}}$.



Power Supply Related Specs

Power Supply Rejection Ratio

- Quantifies an op amp's capability to reject a change on power supply.
- **Such as power drift (from batteries)**



MCP6071 Datasheet

Parameters	Sym	Min	Typ	Max	Units	Conditions
Power Supply Rejection Ratio	PSRR	70	87	—	dB	$V_{CM} = V_{SS}$



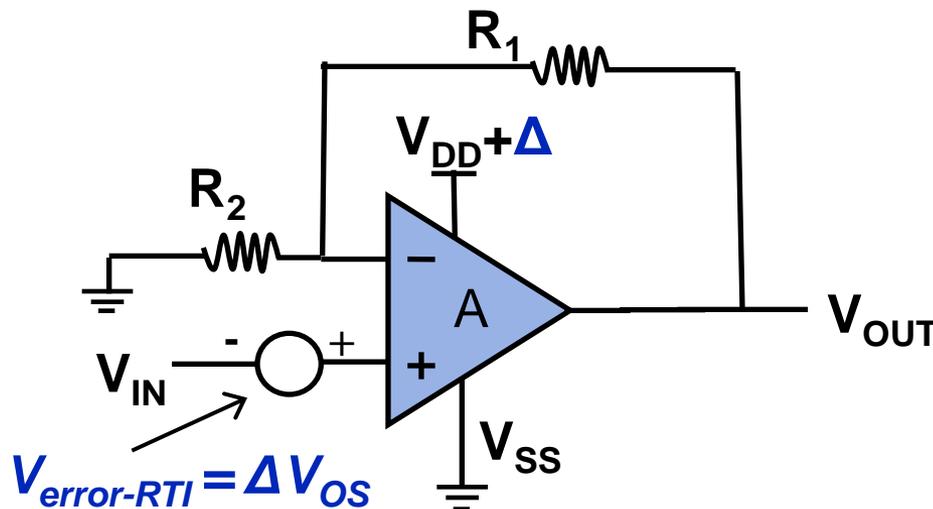
Op Amp DC Specifications

– Refer To Input

- Practically, PSRR is not infinite. In a closed loop system, an amplifier manifests ΔV_{SUPPLY} as offset voltage error ΔV_{OS} at the input.
- This error is described with the formula:

$$\text{PSRR (dB)} = 20\log[(\Delta V_{\text{OUT}}/\Delta V_{\text{OS}})/(\Delta V_{\text{OUT}}/\Delta V_{\text{SUPPLY}})]$$

$$= 20\log(\Delta V_{\text{SUPPLY}}/\Delta V_{\text{OS}})$$



$$V_{\text{error-RTO}} = G_N * V_{\text{error-RTI}}$$

$$= G * V_{\text{error-RTI}}$$

$$= (1 + R_1/R_2) * V_{\text{error-RTI}}$$



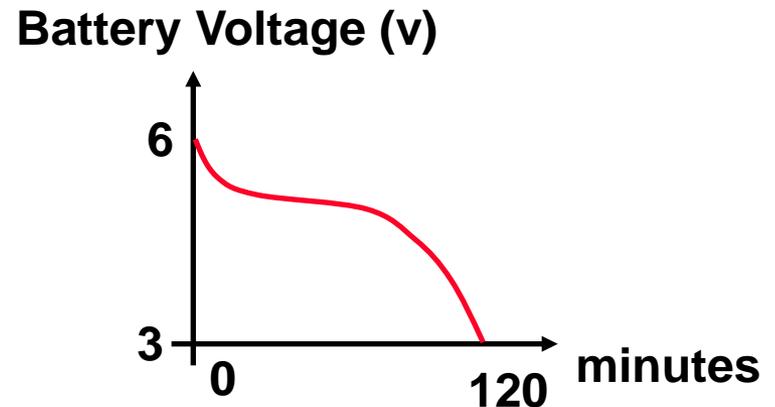
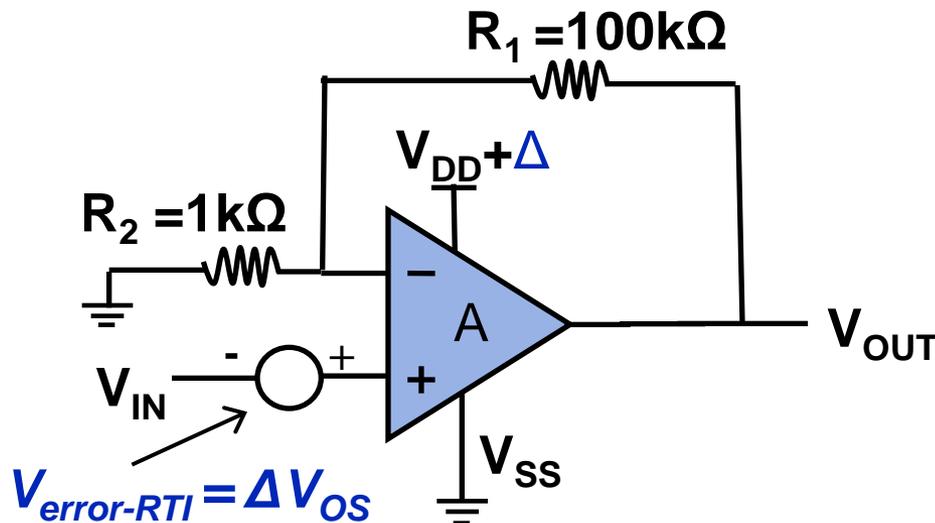
Op Amp DC Specifications

Exercise #17

A Battery Powered Application

- During the life of the battery, the output voltage ranges from 6.0V to 3.0V, PSRR = 80dB.
- What is the error at the output of the amplifier over time?

Recall: $PSRR \text{ (dB)} = 20\log(\Delta V_{\text{SUPPLY}} / \Delta V_{\text{OS}})$





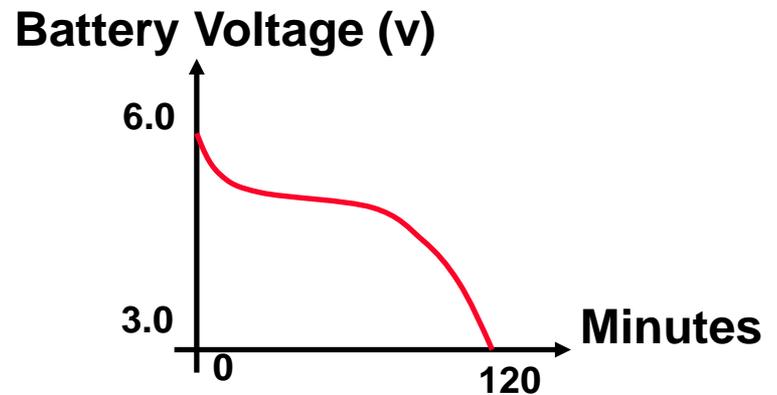
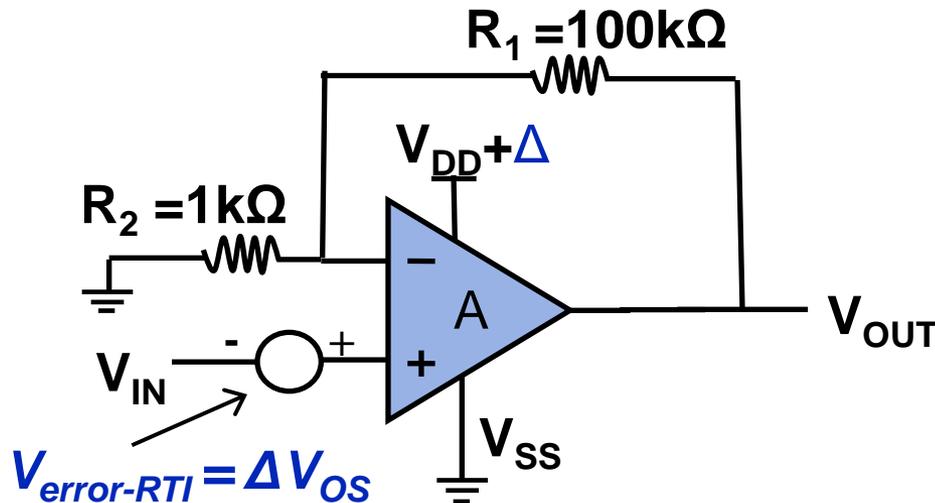
Op Amp DC Specifications

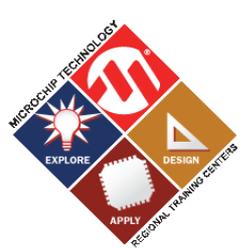
Solution #17

- PSRR = 80dB, $\Delta V_{\text{supply}} = 6.0\text{V} - 3.0\text{V} = 3.0\text{V}$,
 PSRR (dB) = $20\log(\Delta V_{\text{supply}}/\Delta V_{\text{os}}) \rightarrow \Delta V_{\text{os}} = 0.3\text{mV}$.
- The error at the output is

$$V_{\text{error-RTO}} = G_N * V_{\text{error-RTI}} = (1 + R_1/R_2) * \Delta V_{\text{OS}},$$

$$\rightarrow V_{\text{error-RTO}} = (1 + 100) * (0.3\text{mV}) \approx 30.3\text{mV}$$





Power Supply Related Specs

● Application Challenge

- High DC PSRR is needed when
 - Using battery power
 - Using unregulated power
- High AC PSRR is required when
 - Using line power (50 Hz to 400 Hz)
 - Using switched mode power supply
 - Using an op amp with digital logic (*which typically causes a lot of power supply noise*)

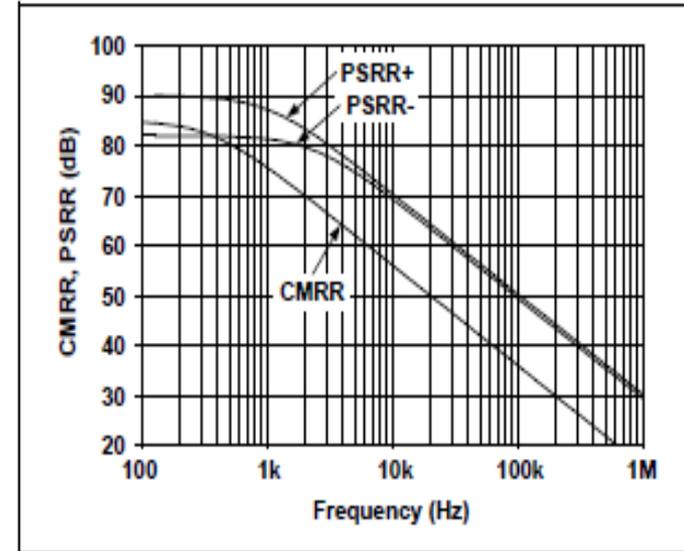


FIGURE 2-9: CMRR, PSRR vs. Frequency.



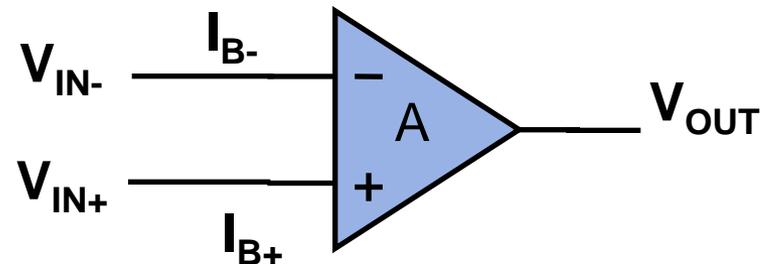
Op Amp DC Specifications

Input Bias Current (I_B , I_{B+} , I_{B-} , and I_{OS})

- **Input bias current (I_B)**
 - The input bias current is the average current drawn by the input terminals.
 - Depending on the type of input transistor, the bias current can flow in or out of the input terminals.
- **Input offset current (I_{OS})**
 - It is equal to the difference between I_{B+} and I_{B-} . It will be either positive or negative.

$$I_B = (I_{B+} + I_{B-})/2$$

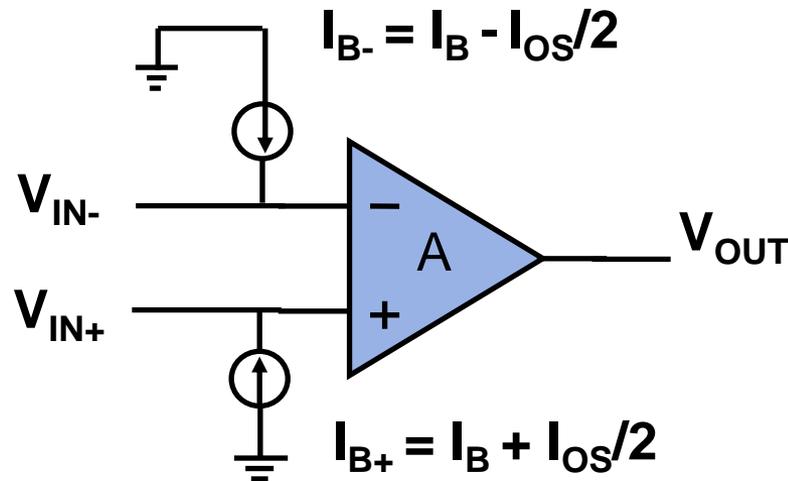
$$I_{OS} = I_{B+} - I_{B-}$$





Op Amp DC Specifications

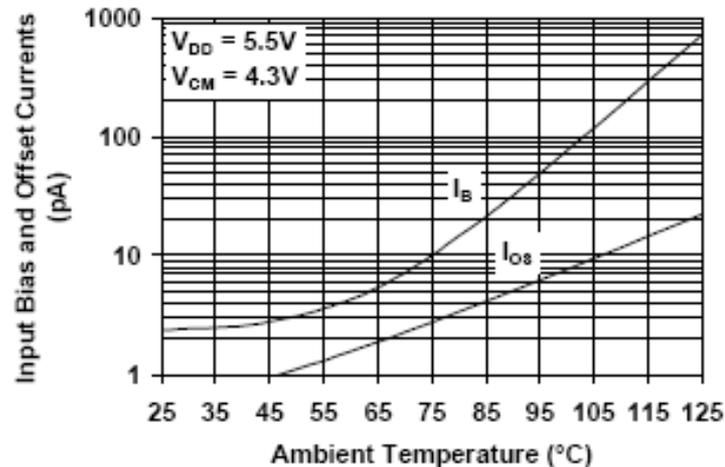
- **Circuit Model** for an op amp with I_B
 - The input current is modeled as current sources, I_{B+} and I_{B-} , in parallel with the positive and negative input terminals.





Op Amp DC Specifications

- I_B and I_{OS} vary with ambient temperature.



- **Example: MCP601 data sheet**

Electrical Characteristics: Unless otherwise indicated, all limits are specified for $V_{DD} = +1.4 \text{ V to } +5.5 \text{ V}$, $V_{SS} = \text{GND}$, $T_A = 25 \text{ }^\circ\text{C}$, $V_{CM} = V_{DD}/2$, $R_L = 1 \text{ M}\Omega \text{ to } V_{DD}/2$, and $V_{OUT} \sim V_{DD}/2$

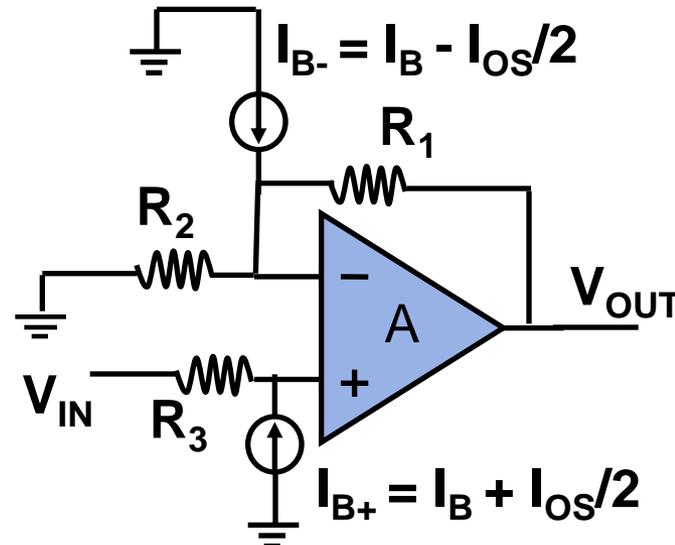
Parameters	Sym	Min	Typ	Max	Units	Conditions
Input Bias Current	I_B	—	1.0	—	pA	$T_A = -40^\circ\text{C to } +85^\circ$
Input Bias Current Over Temperature	I_B	—	—	100	pA	
Input Offset Current	I_{OS}	—	1.0	—	pA	



Op Amp DC Specifications

Application Challenge

- The lower the I_B , the smaller the effect on the output signal.
- The most **sensitive** configurations for the op amp's input bias current error.
- Circuits that use **high value** resistors at the input of the amplifier.





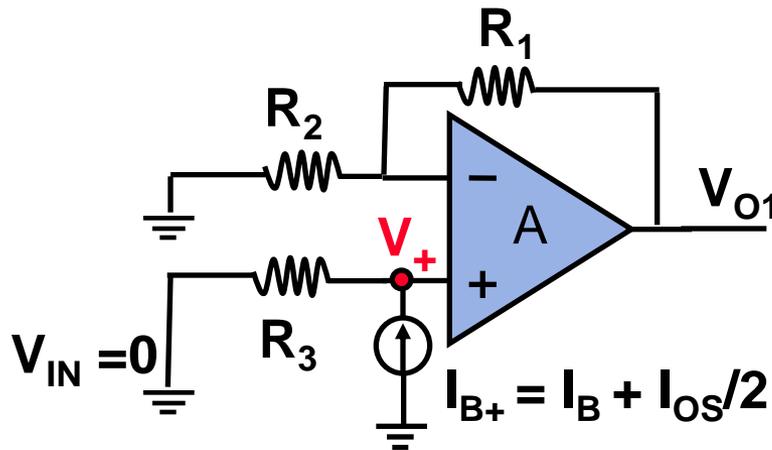
Op Amp DC Specifications

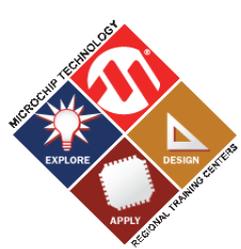
- Effect of input bias current I_{B+} and I_{B-} on the output
- **Using Superposition Principle**
 - **Effect of I_{B+} on the output**

Let $V_{IN} = 0$, $I_{B-} = 0$

$$V_{O1} = V_+ * (1 + R_1/R_2); \quad V_+ = I_{B+} R_3$$

$$\text{So, } V_{O1} = (I_{B+} R_3) * (1 + R_1/R_2)$$





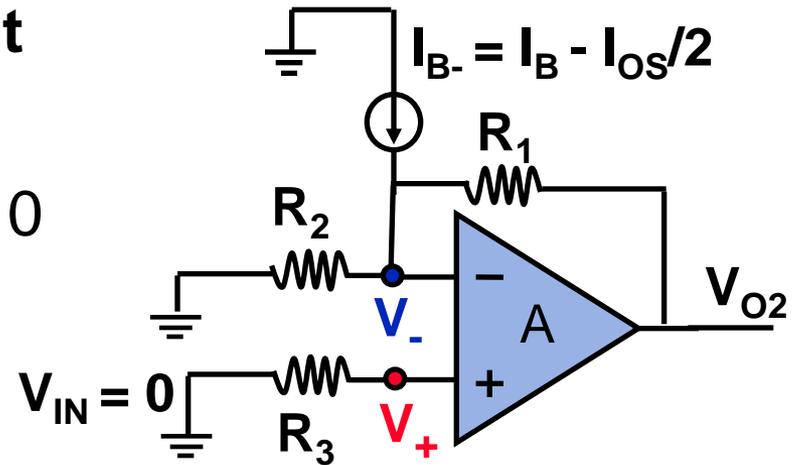
Op Amp DC Specifications

- **Effect of I_{B-} on the output**

Let $V_{IN} = 0$, $I_{B+} = 0$

$V_- - V_{O2} = I_{B-}R_1$; $V_- = V_+ = 0$

So, $V_{O2} = - I_{B-}R_1$



- **Total effect of input bias current I_{B+} and I_{B-} on the output**

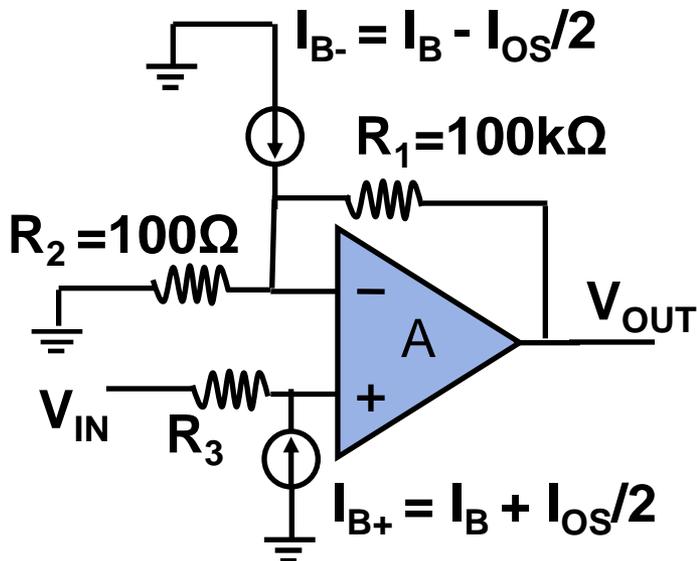
$$V_O = V_{O1} + V_{O2} = (I_{B+}R_3) * (1 + R_1/R_2) - I_{B-}R_1$$



Op Amp DC Specifications

Exercise #18

- Refer to the non-inverting amplifier, $I_B = 16\text{nA}$, $I_{OS} = 1\text{nA}$. Assume $R_3 = 100\text{k}\Omega$, what is the DC error at the output? If $R_3 = R_1 // R_2 \approx 100\Omega$, repeat the calculation.

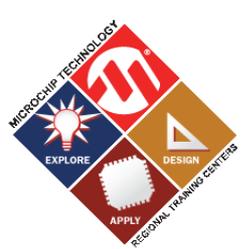


Hint:

Effect of I_{B+} on V_{OUT} : $V_{O1} = I_{B+} R_3 (1 + R_1/R_2)$

Effect of I_{B-} on V_{OUT} : $V_{O2} = - (I_{B-} R_1)$

Total Effect: $V_o = I_{B+} R_3 (1 + R_1/R_2) - (I_{B-} R_1)$



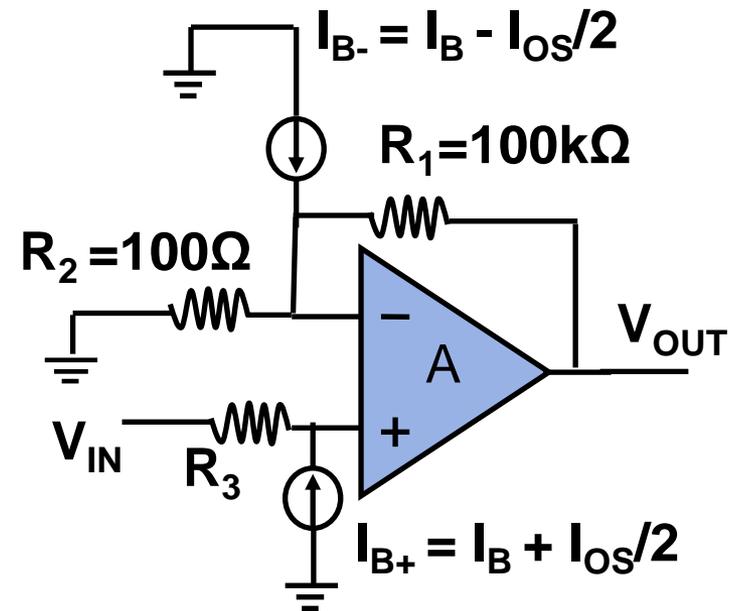
Op Amp DC Specifications

Solution #18

- $I_B = 16\text{nA}$, $I_{OS} = 1\text{nA}$,
 $I_{B-} = I_B + I_{OS}/2$; $I_{B+} = I_B - I_{OS}/2$

If $R_3 = R_1 = 100\text{k}\Omega$,
 then

$$\begin{aligned}
 V_o &= (I_{B+} R_3) * (1 + R_1/R_2) - (I_{B-} R_1) \\
 &= I_B * (100\text{M}\Omega - 100\text{k}\Omega) + \\
 &\quad I_{OS} * (50\text{M}\Omega + 50\text{k}\Omega) \\
 &\approx 1.6\text{V}
 \end{aligned}$$





Op A

Assume $I_{B+} = I_{B-} = I_B$

$$\rightarrow V_o = I_B [R_2 - R_3 (1 + R_2/R_1)]$$

$$\text{for } V_o = 0$$

$$\Rightarrow R_3 = \frac{R_2}{1 + R_2/R_1} = \frac{R_2 R_1}{R_1 + R_2} = R_1 // R_2$$

- If $R_3 = R_1 // R_2 \approx 100k$ then

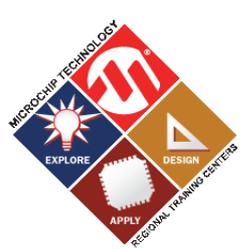
$$\begin{aligned}
 V_o &= (I_{B+} R_3) * (1 + R_2/R_1) \\
 &= (100k\Omega) * (I_{B-}) \\
 &= (100k\Omega) * I_{OS} \\
 &= \mathbf{0.1mV}
 \end{aligned}$$

R_3 is called a **balanced resistor**.
 For minimum error due to the input bias current, R_3 should be equal to $R_1 // R_2$.



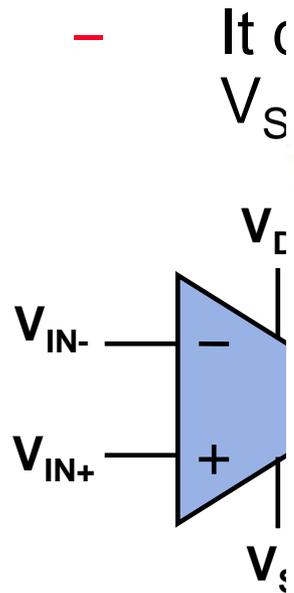
Input Related Specs

- **For CMOS and FET input op amps**
 - I_B is low enough not to cause appreciable error
 - I_B : ~ **1pA to several nA** (from 25°C to 125°C)
- **For BJT input op amps**
 - I_B may become an issue
 - I_B : ~ **10nA to several thousand nA** (from 25°C to 125°C)



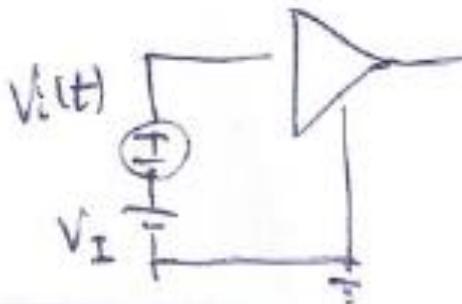
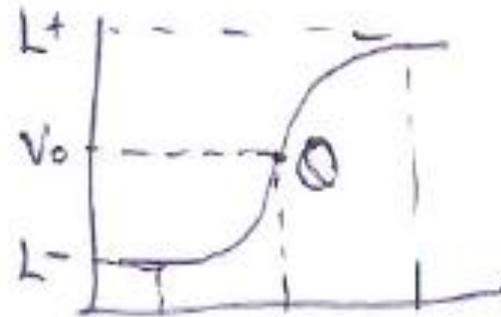
Op Amp DC Specs: Power

Power S



Single (Positive) Power Supply.
 → nonlinearity due to single supply operation, not centered around the origin.
 → biasing → apply a DC voltage V_I .

$$A_V = \left. \frac{dV_o}{dV_i} \right|_{at Q}$$



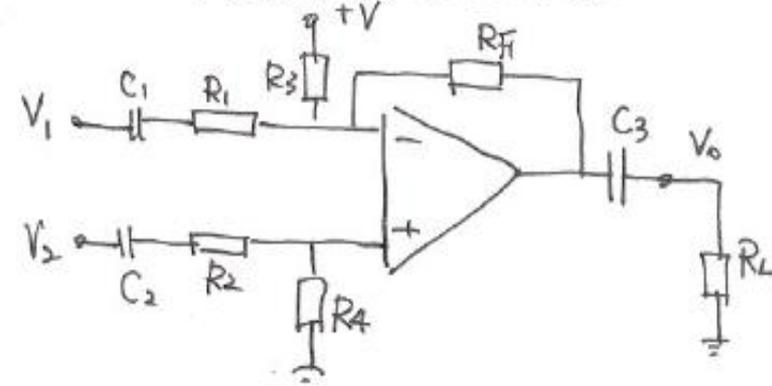
MCP6031 Datasheet

Parameters	Sym	Min	Typ	Max	Units	Conditions
Supply Voltage	V_{DD}	1.8	—	5.5	V	



Single Power Supply Amp Circuit

單電源、供電之差分放大器



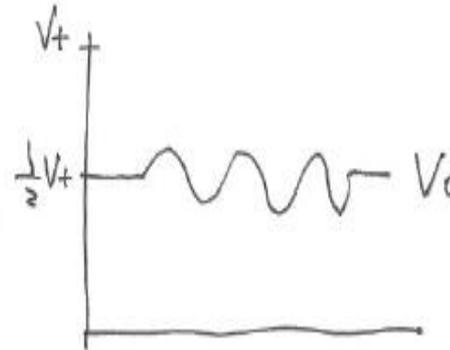
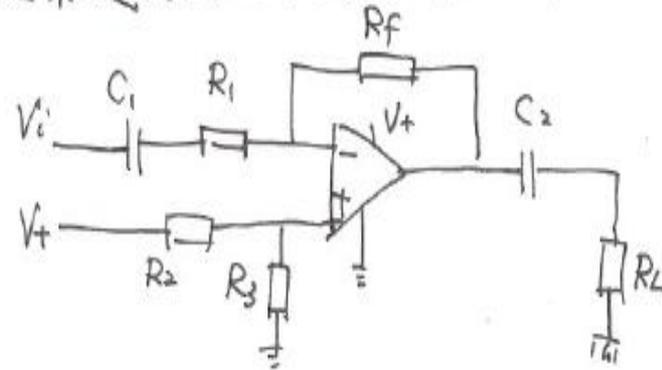
$$V_0 = \frac{R_F}{R_1} (V_2 - V_1), \quad \frac{R_F}{R_1} = \frac{R_3}{2R_2}$$

if $R_F = R_1 \rightarrow$ 模擬減法器.

缺點: 無信號輸入時, 輸出為電源電壓之一半.
即所謂甲類放大器之輸出狀態.

— 靜態功耗較大.

單電源供電的反相放大器 (在輸入, 輸出信號端加交流耦合電容)

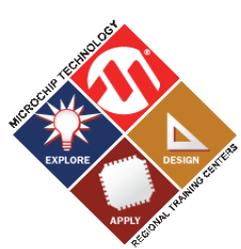


$$G = -\frac{R_F}{R_1}$$

$$C_1 = 1000 / (2\pi f_c R_1) \text{ (}\mu\text{F)}$$

$$C_2 = 1000 / (2\pi f_c R_L) \text{ (}\mu\text{F)}$$

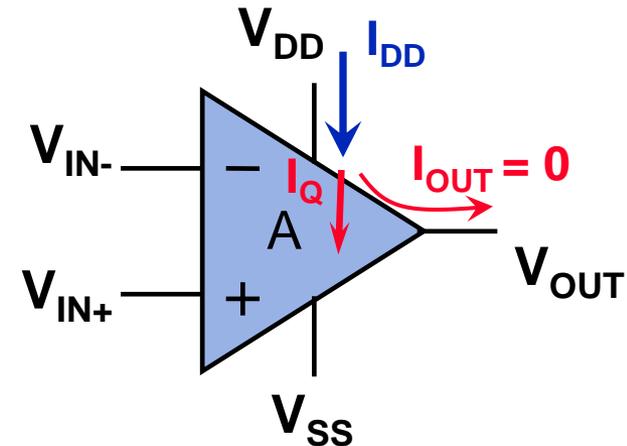
一般 $R_2 = R_3 = 2R_1$.



Op Amp DC Specifications

Power Supply Requirements

- Power Supply Voltage
 - It defines the acceptable difference between V_{DD} and V_{SS} which allows **linear** operation of the op amp.
- Quiescent Current (I_Q)
 - It is the amount of current consumed by op amp when it is not performing any work.
 - **Usually, the order of mA ~ μ A.**
 - **Low I_Q is preferred for power-saving .**

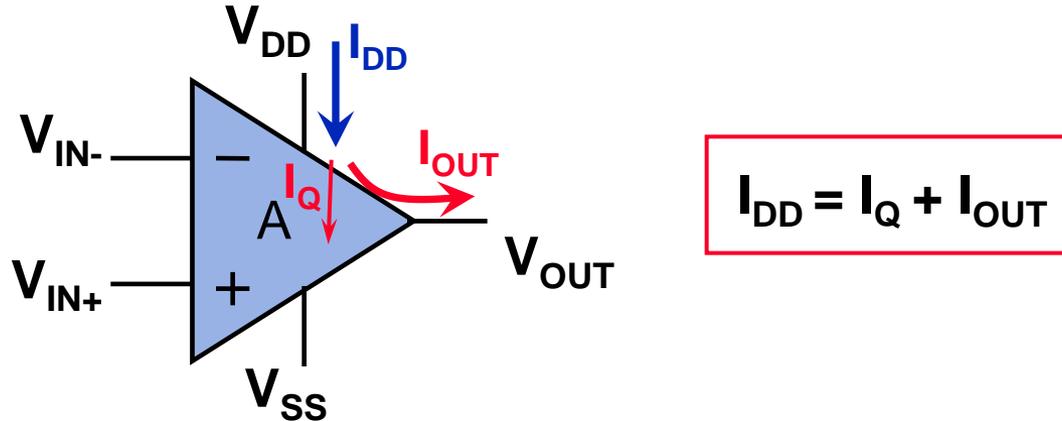


$$I_{DD} = I_Q + I_{OUT}$$



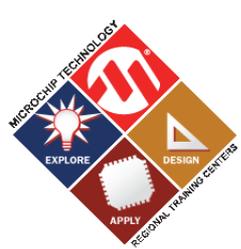
Op Amp DC Specifications

- Typically, if a load is applied to op amp, the current into V_{DD} pin will primarily goes through the op amp output stage, and then through the load.



- **Example: MCP601 data sheet**

Parameters	Sym	Min	Typ	Max	Units	Conditions
Power Supply						
Supply Voltage	V_{DD}	2.7	—	5.5	V	
Quiescent Current per Amplifier	I_Q	—	230	325	μA	$I_O = 0$



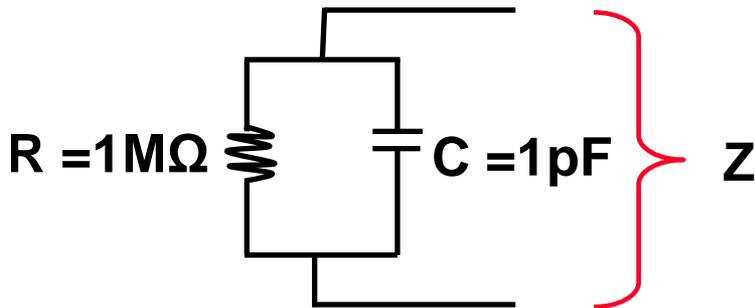
Op Amp DC Specifications

Input Impedance/Output Impedance (Z_{IN} , Z_{OUT})

- Impedance:

Generalizes Ohm's law to AC circuit analysis. Unlike resistance, the impedance of an electric circuit is **a function of frequency**.

- **Example:** Impedance (Z) at different frequency.



f (Hz)	$ Z_C $ (Ω)	$ Z $ (Ω)
1	1.6×10^{11}	1M
0.1M	1.6M	0.85M
0.5M	0.32M	0.30M

$$Z = R // Z_C, Z_C = 1/(j\omega C), \omega = 2\pi f$$

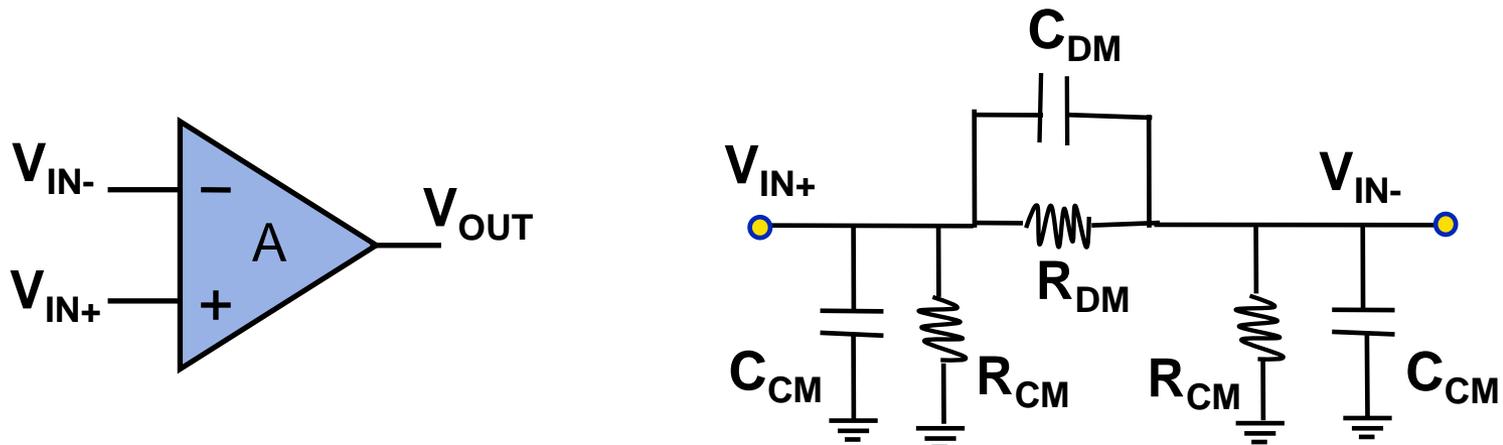


Op Amp DC Specifications

- Example: MCP601 data sheet

Parameters	Sym	Min	Typ	Max	Units
Common Mode Input Impedance	Z_{CM}	—	$10^{13} \parallel 6$	—	$\Omega \parallel pF$
Differential Input Impedance	Z_{DIFF}	—	$10^{13} \parallel 3$	—	$\Omega \parallel pF$

**Recall: The input impedance of an ideal op amp is infinity.
For a real op amp, high input impedance is preferred.**

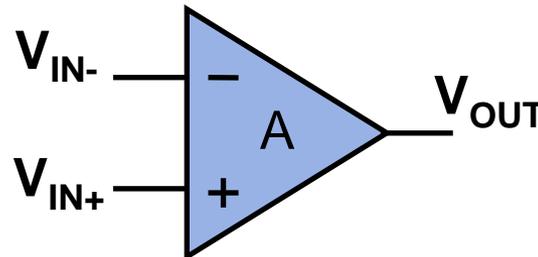




Op Amp DC Specifications

Output Impedance (Z_{OUT})

- **Low** output impedance of an op amp is an important characteristic.
- Ideally, it should be zero and it is usually very small.
 - This minimizes the loading effect of the op amp output stage.
- Normally, it is not specified in our data sheet.





Op Amp

AC Specifications



Op Amp AC Specifications

Primary AC performance specifications

- **Frequency Domain Spec.**

--- Describe the response to **Sine Wave Input** and **Bode Plot Analysis** method will be introduced.

- **Gain Bandwidth Product (GBWP)**
- **Phase Margin/Gain Margin (PM, GM)**
- **Full Power Bandwidth (FPBW)**

- **Time Domain Spec.**

--- Describe the response to a **Step Input**.

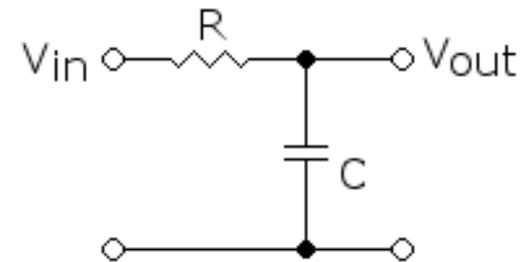
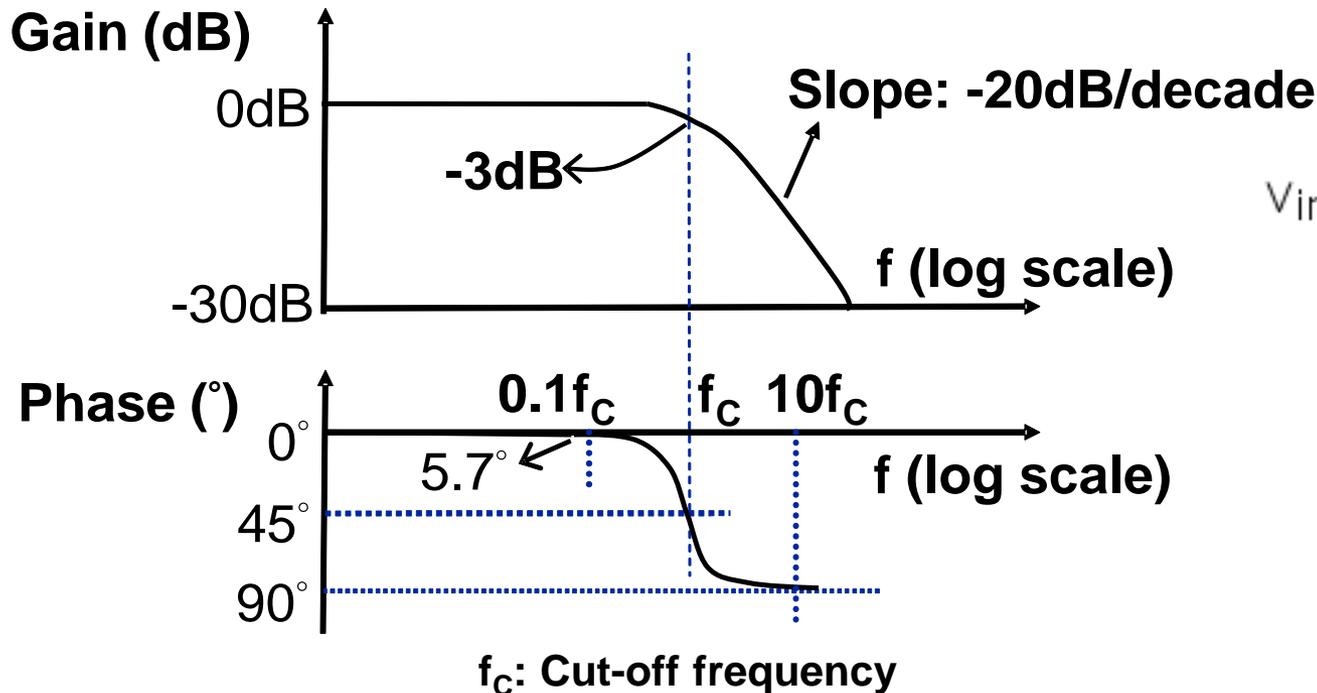
- **Slew Rate (SR)**
- **Settling Time**
- **Overshoot**



Op Amp AC Specifications

Bode Plot Analysis Method

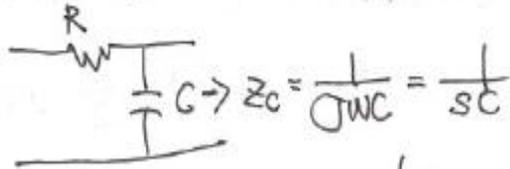
- The Bode plot describes the output response of a frequency-dependent system for a sine wave input. It is a combination of **magnitude plot** and **phase plot**.



Low Pass Filter
 $G = V_{out} / V_{in}$



Bode Plot Analysis



$$\frac{V_o(s)}{V_i(s)} = \frac{Z_c}{R + Z_c} = \frac{\frac{1}{sC}}{R + \frac{1}{sC}} = \frac{1}{1 + sRC} = \frac{1}{1 + \frac{s}{\omega_0}}$$

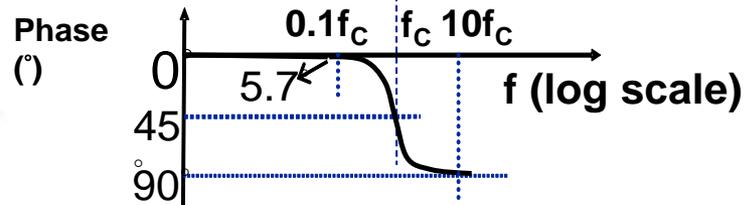
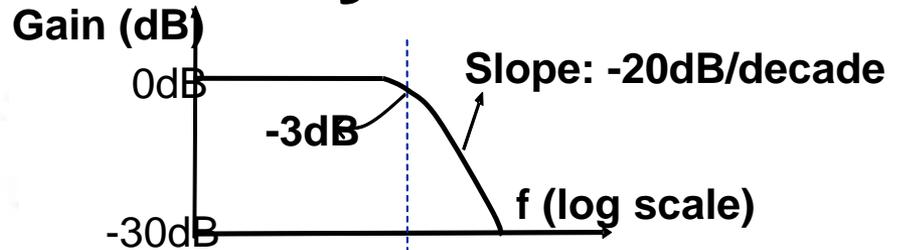
$$\Rightarrow \frac{V_o(j\omega)}{V_i(j\omega)} = \frac{1}{1 + j\frac{\omega}{\omega_0}} \quad (\omega_0 = \frac{1}{RC})$$

$$|H(j\omega)| = \left| \frac{1}{1 + j\frac{\omega}{\omega_0}} \right| = -20 \log(\sqrt{1 + (\frac{\omega}{\omega_0})^2}) \text{ dB}$$

(i) $\omega \ll \omega_0$ $|H(j\omega)| = -20 \log(1) = 0 \text{ dB}$

(ii) $\omega \gg \omega_0$ $|H(j\omega)| = -20 \log(\frac{\omega}{\omega_0}) \text{ dB}$

(iii) $\omega = \omega_0$ $|H(j\omega)| = -20 \log(\sqrt{2}) \text{ dB} = -3.01 \text{ dB} \approx -3 \text{ dB}$



f_c : Cut-off frequency

$$\angle H(j\omega) = -\angle \left[1 + j\frac{\omega}{\omega_0} \right] = -\tan^{-1} \left(\frac{\omega}{\omega_0} \right)$$

$\angle H(j\omega) \approx -\tan^{-1}(0) = 0^\circ = 0 \text{ radian}$

$\angle H(j\omega) \approx -\tan^{-1}(\infty) = -90^\circ = -\frac{\pi}{2} \text{ (radian)}$

$\angle H(j\omega) = -\tan^{-1}(1) = -45^\circ = -\frac{\pi}{4} \text{ (radian)}$

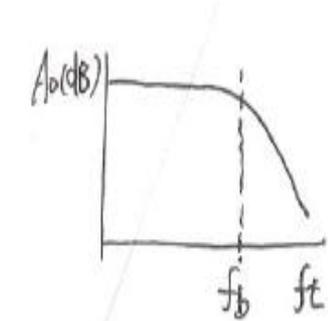
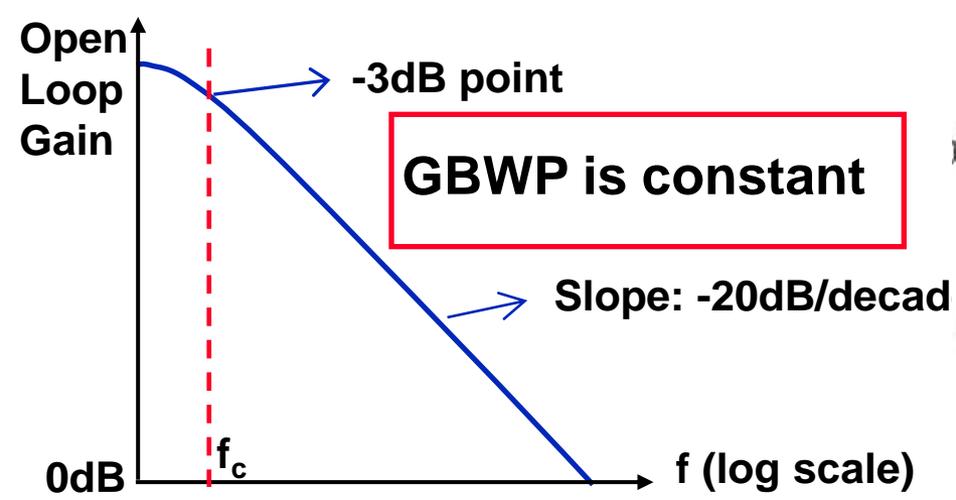
Bode plot for magnitude at 0dB until the break frequency and then drop at 20 dB per decade.



Op Amp AC Specifications

Gain Bandwidth Product (GBWP)

- GBWP is the product of op amp **open loop gain times the frequency** at any point where the amplifier response is attenuating at a rate of -20dB/decade of frequency.



* Internal Compensated.

$$A(s) = \frac{A_0}{1 + s/w_b}$$

$$A(j\omega) = \frac{A_0}{1 + j\omega/w_b}$$

(i) $\omega = w_b$, $|A(j\omega)| = \frac{A_0}{\sqrt{2}}$, (-3dB point)

(ii) $\omega \gg w_b$, $A(j\omega) \approx \frac{A_0 w_b}{j\omega}$

if $\omega = \omega_t = A_0 w_b$

$|A(j\omega)| = 1 = 0 \text{ dB}$

- Unit Gain Bandwidth
- Gain Bandwidth Product.



Op Amp AC Specifications

- GBWP is used to estimate closed loop gain bandwidth when the gain is known.

$$BW \approx GBWP/G_N$$

- **BW: Closed loop gain bandwidth**
 - **G_N : Noise gain**
 - **Recall: For $|G| \gg 1$, $G_N \approx |G|$.**
- The larger GBWP, the wider BW for a certain closed loop gain.
- **Example: MCP601 data sheet**

Parameters	Sym	Min	Typ	Max	Units	Conditions
Gain Bandwidth Product	GBWP	—	2.8	—	MHz	



BW \approx GBWP/ G_N

Frequency Response of Closed-Loop Amplifiers

the inverting circuit

$$\frac{V_o}{V_i} = \frac{-R_2/R_1}{1 + (1 + R_2/R_1)A}$$

finite op amp open-loop gain A

$$\frac{V_o(s)}{V_i(s)} = \frac{-R_2/R_1}{1 + \frac{1}{A_0} \left(1 + \frac{R_2}{R_1}\right) + \frac{s}{\omega_t/(1 + R_2/R_1)}}$$

For $A_0 \gg 1 + R_2/R_1$

$$\frac{V_o(s)}{V_i(s)} \approx \frac{-R_2/R_1}{1 + \frac{s}{\omega_t/(1 + R_2/R_1)}}$$

noninverting circuit

$$\frac{V_o}{V_i} = \frac{1 + R_2/R_1}{1 + (1 + R_2/R_1)A}$$

For $A_0 \gg 1 + R_2/R_1$

$$\frac{V_o(s)}{V_i(s)} \approx \frac{1 + R_2/R_1}{1 + \frac{s}{\omega_t/(1 + R_2/R_1)}}$$

$$A(j\omega) = \frac{A_0}{1 + j\omega/\omega_b}$$

$$\omega_{3dB} = \frac{\omega_t}{1 + R_2/R_1}$$



Op Amp AC Specifications

Exercise #19

- Assume $GBWP = 1\text{MHz}$ and unity gain stable, what is the closed loop gain bandwidth for $G = 1, 11, -1, -10$?

	G (closed loop gain)		G_N (noise gain)
R_1/R_2	Non-inverting	Inverting	$1/\beta$
0.1	1.1	- 0.1	1.1
1	2	-1	2
10	11	-10	11

Recall $BW = GBWP/G_N$, Inverting amplifier: $G_N = 1 + |G|$,
 Non-inverting amplifier: $G_N = G$.



Op Amp AC Specifications

Solution #19

- For $G = 1$ (unity gain stable) $\rightarrow G_N = G = 1$;
 $BW = 1\text{MHz}/1 = 1\text{MHz}$
- For $G = 11 \rightarrow G_N = G = 11$;
 $BW = 1\text{MHz}/11 = 91 \text{ kHz}$
- For $G = -1 \rightarrow G_N = 1 + |G| = 2$; $BW = 1\text{MHz}/2 = 500 \text{ kHz}$
- For $G = -10 \rightarrow G_N = 1 + |G| = 11$; $BW = 1\text{MHz}/11 = 91 \text{ kHz}$

R_1/R_2	G		G_N
	Non-inverting	Inverting	$1/\beta$
0.1	1.1	- 0.1	1.1
1	2	-1	2
10	11	-10	11

$$BW = GBWP/G_N$$

Non-inverting amplifier: $G_N = G$

Inverting amplifier: $G_N = 1 + |G|$

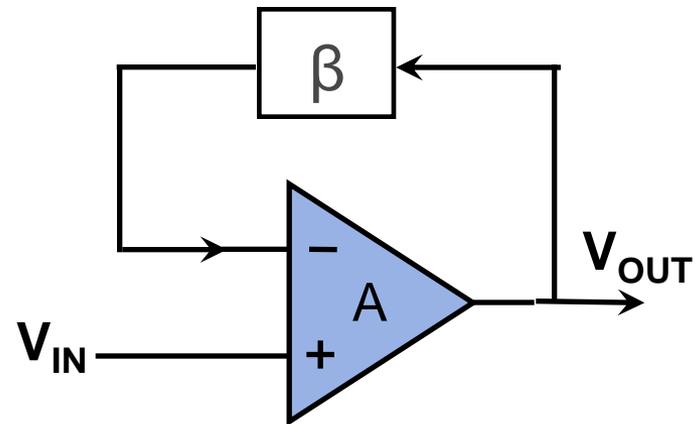


Op Amp AC Specifications

Stability of Op Amp and its Feedback Loop

$$G = \frac{A}{1 + \beta A}$$

G: closed loop gain
A: open loop gain
 βA : loop gain



- If **$\beta A = -1$** at frequency f_0 , $G = A/(1-1) = \infty \rightarrow$ Instability.
- $\beta A = -1 : |\beta A| = 1$ and $\angle \beta A = -180^\circ$, at $f = f_0$
- This observation leads us to the concepts “Phase Margin”.



Op Amp AC Specifications

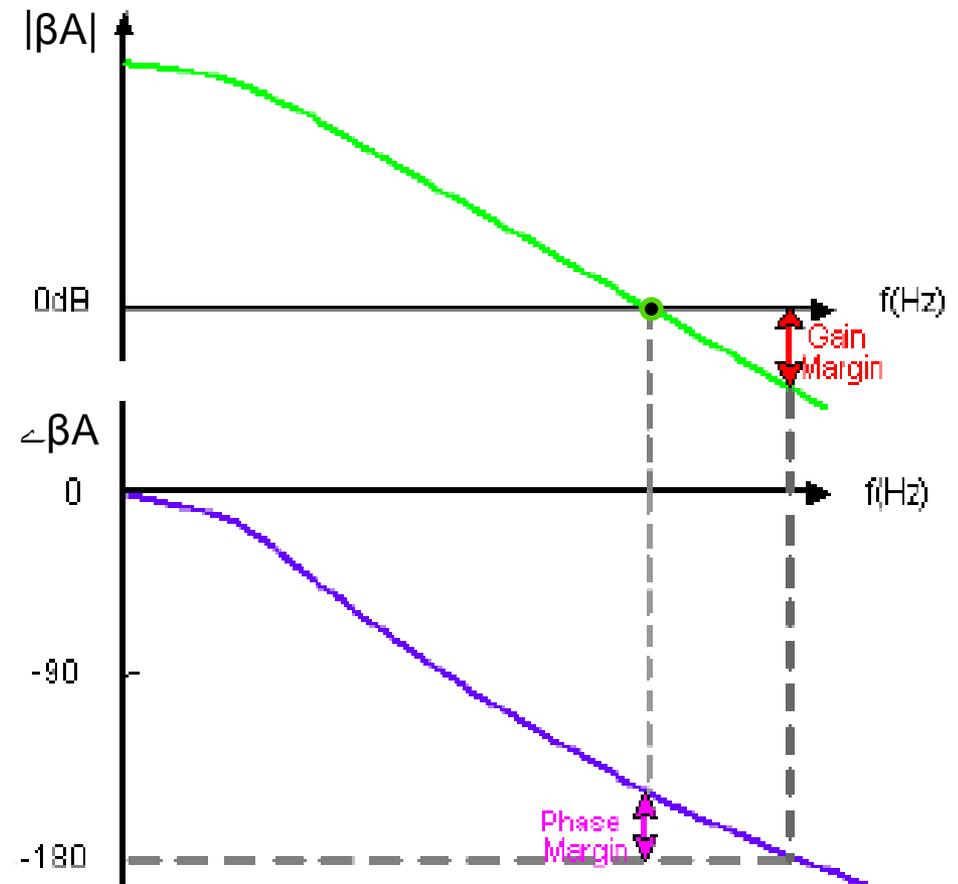
Phase Margin (PM) and Gain Margin (GM)

- Phase Margin:

The phase difference between $\angle\beta A(f_{0dB})$ and -180° , where f_{0dB} is the frequency at which $|\beta A|=1$.

- Gain Margin:

The difference between 0dB and $|\beta A|$ where the loop gain phase is -180° .





Op Amp AC Specifications

Emphasis

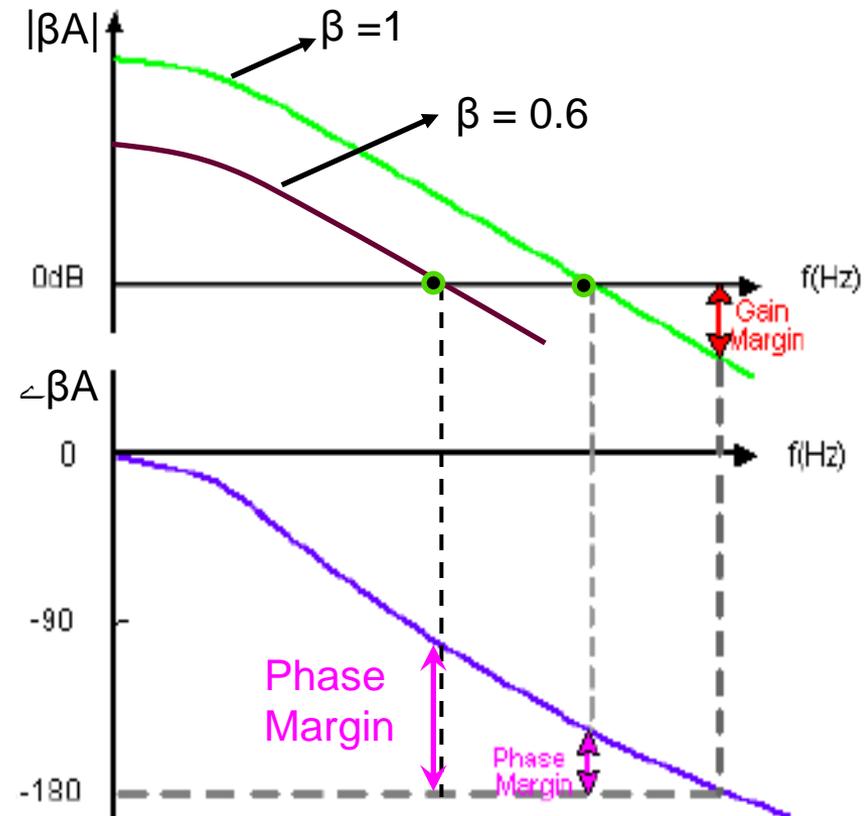
PM $\leq 0^\circ$ indicates instability and oscillation.

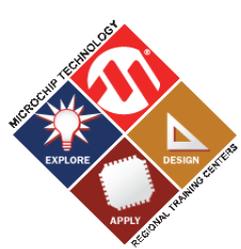
PM $> 0^\circ$ indicates stability (in theory) .

— **Our data sheet specifies PM of the worst case stability. (G =1, $\beta =1$)**

➤ Recall: $0 \leq \beta \leq 1$, when $\beta =1$, $G = \frac{A}{(1+\beta A)} = \frac{A}{(1+A)} \approx 1$

➤ $\beta < 1$, PM is bigger, which makes the feedback system more stable.





Op Amp AC Specifications

- **PM > 0°** indicates stability. How far from **0°** is enough?
 - PM = 65° is adequate for the stability (at G=1).
 - PM = 90° is more stable but it has slow time response.

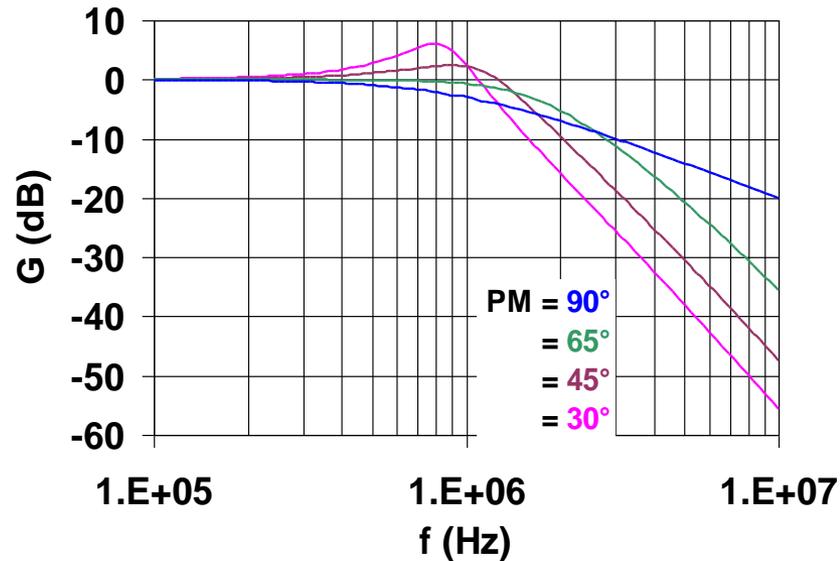


Figure: Frequency response for PM = 30°, 45°, 65°, 90° at G = 1

$$\boxed{A(j\omega_1)\beta = 1 \times e^{-j\theta}} \quad \theta = 180^\circ - \text{phase margin}$$

$$A_f(j\omega_1) = \frac{A(j\omega_1)}{1 + A(j\omega_1)\beta} = \frac{(1/\beta)e^{-j\theta}}{1 + e^{-j\theta}}$$

$$|A_f(j\omega_1)| = \frac{1/\beta}{|1 + e^{-j\theta}|}$$

phase margin of 45°, $\theta = 135^\circ$

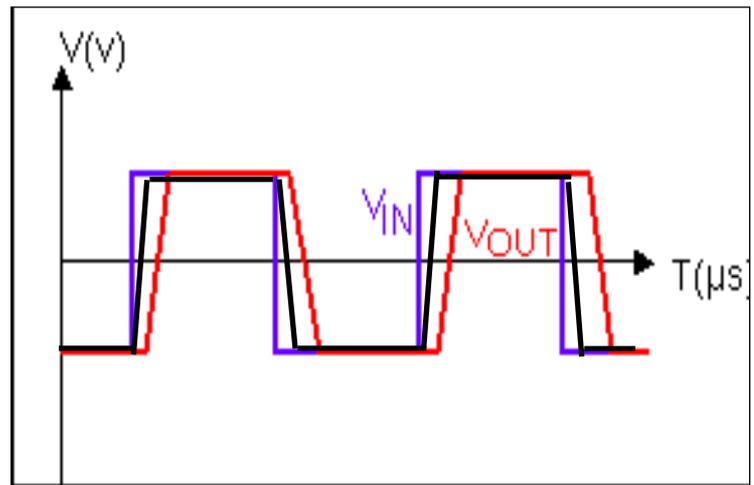
$$\boxed{|A_f(j\omega_1)| = 1.3 \frac{1}{\beta}}$$



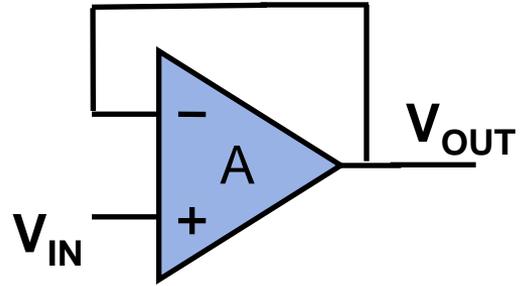
Op Amp AC Specifications-- SR

Emphasis (Slew-Rate Limiting on Output Transient Step)

- Slew Rate is the maximum rate of change at the output of an op amp. Basically says how fast the output can “follow” the input.
- The bigger the SR is, the faster the output of op amp can follow the input.



$$SR = \left. \frac{\Delta V_{OUT}}{\Delta t} \right|_{MAX}$$



Example: MCP601 data sheet

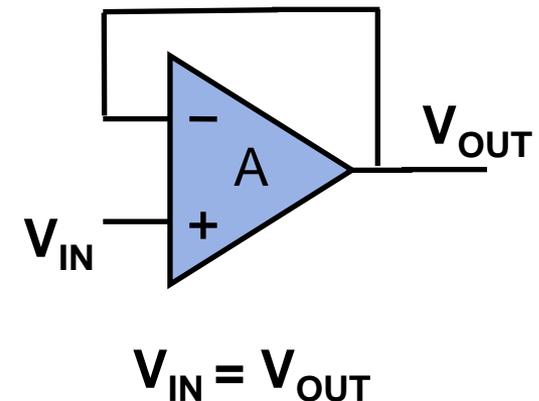
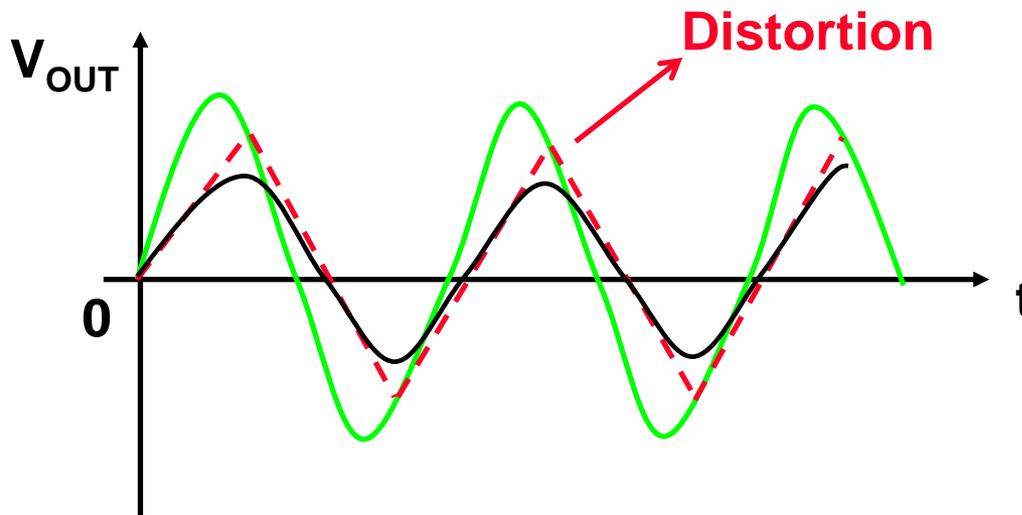
Parameters	Sym	Min	Typ	Max	Units	Conditions
Slew Rate	SR	—	2.3	—	V/μs	G = +1 V/V



Op Amp AC Specifications

Slew-Rate Limiting

- Effect of slew-rate limiting on output sine waveforms.
 - Theoretical output 
 - Output when op amp is slew-rate limited 
 - The fastest changing input signal without slew-rate limiting 

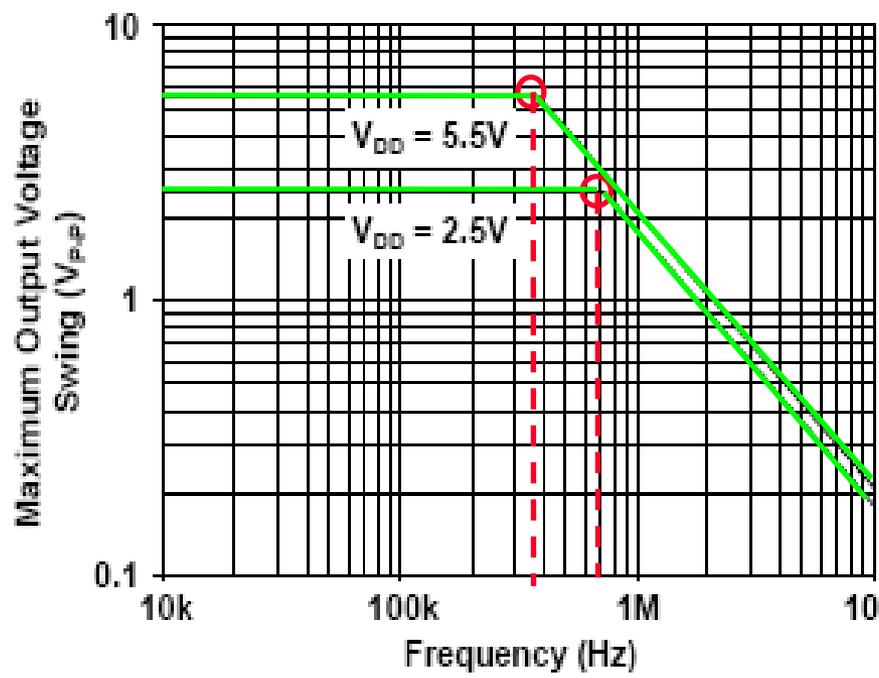




Op Amp AC Specifications

Full Power Bandwidth (FPBW)

- FPBW gives the **highest frequency sine** wave that will not be distorted by the slew rate limit and it is still at the **maximum output voltage swing**.



$$FPBW = SR / (2\pi V_{OMAX})$$

SR: slew rate

V_{OMAX}: maximum output voltage

$$V_I = \hat{V}_i \sin \omega t$$

$$\frac{dV_o}{dt} \approx \frac{dV_i}{dt} = \omega \hat{V}_i \cos \omega t$$

$$\omega_M V_{omax} = SR \text{ (Voltage follower)}$$

$$\Rightarrow f_M = \frac{SR}{2\pi V_{omax}}$$
 (Voltage Follower)



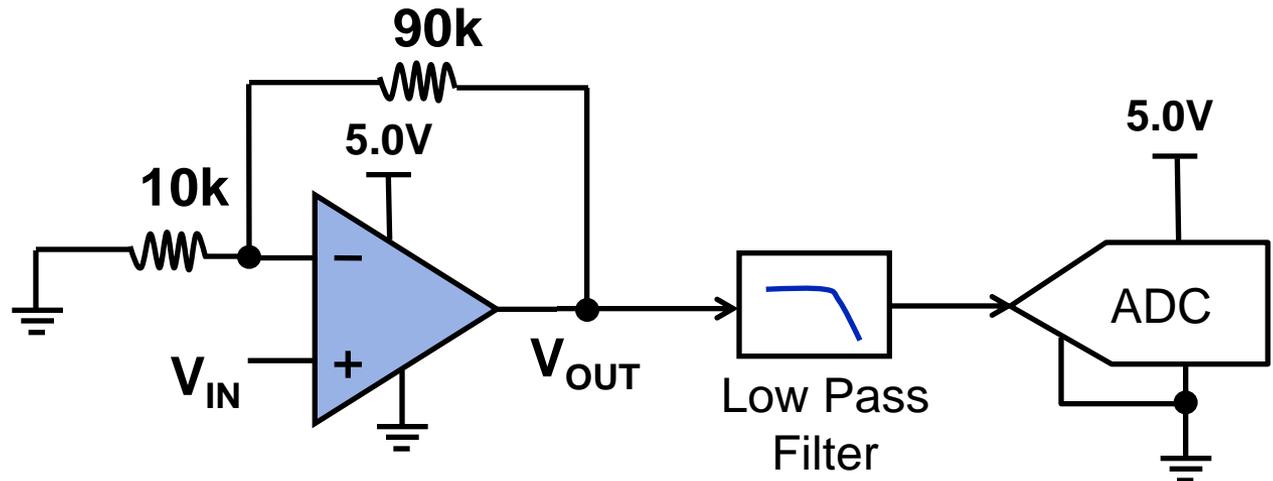
Speed Related Specs

● Application Challenge

- FPBW is important when an amplifier drives the input of ADC which requires full dynamic range.
- **Example:** $FPBW = SR / (2\pi * V_{OUT-PP})$
 $= (0.6V/\mu s) / (2\pi * 5.0V_{P-P}) \approx 19kHz$
- **(Note: Small signal BW = GBWP/G_N = 1.0 MHz/10 = 100 kHz)**

Op amp:

Rail-to-rail Output
SR = 0.6 V/ μ s
GBWP = 1.0 MHz





Op Amp AC Specifications

Em

CMOS製程 OP 之特色.

- 優點:
1. 低 I_{bias} .
 2. 低 $I_{supply} < 1\mu A$.
 3. 易做到 Rail-to-Rail Input/output
 4. Low Noise, Small nV/\sqrt{Hz} .

} 適合 portable Application.

ent

F

- 缺點:
1. 低 Supply 電壓
 2. 低 GBWP (10MHz)
 3. 低 Slew Rate ($5V/\mu s$)

} 不適合高速放大或影像.

Audio is O.K. (41 ~ 20kHz).

0V
step

Time

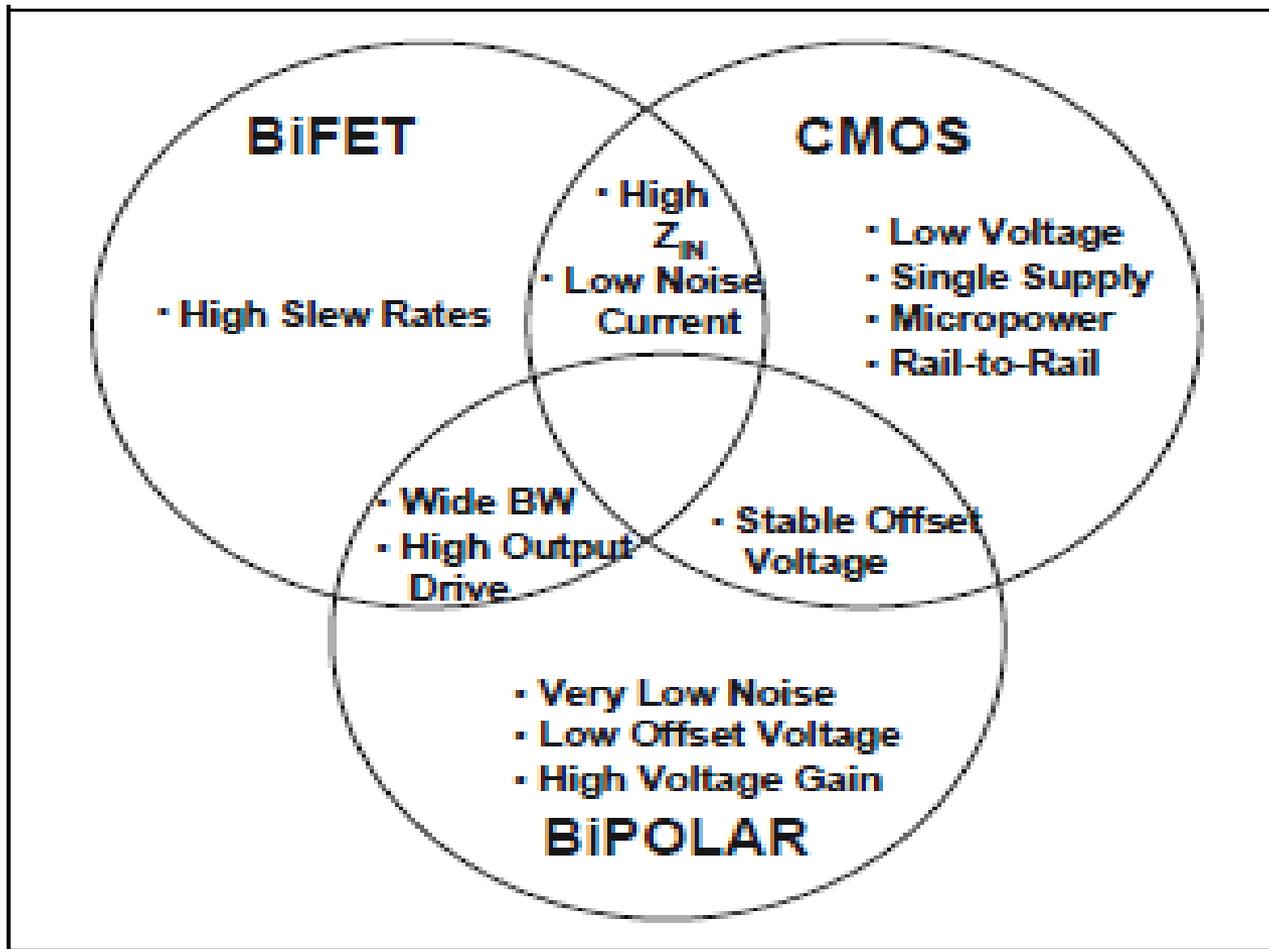


FIGURE 2: Different IC processes render different advantages for amplifiers. The choices in processes for single supply amplifiers are Bipolar, CMOS and BiFET, which is a combination of Field Effect Transistors (FET) and Bipolar transistors.



Example-Thermocouple Solution

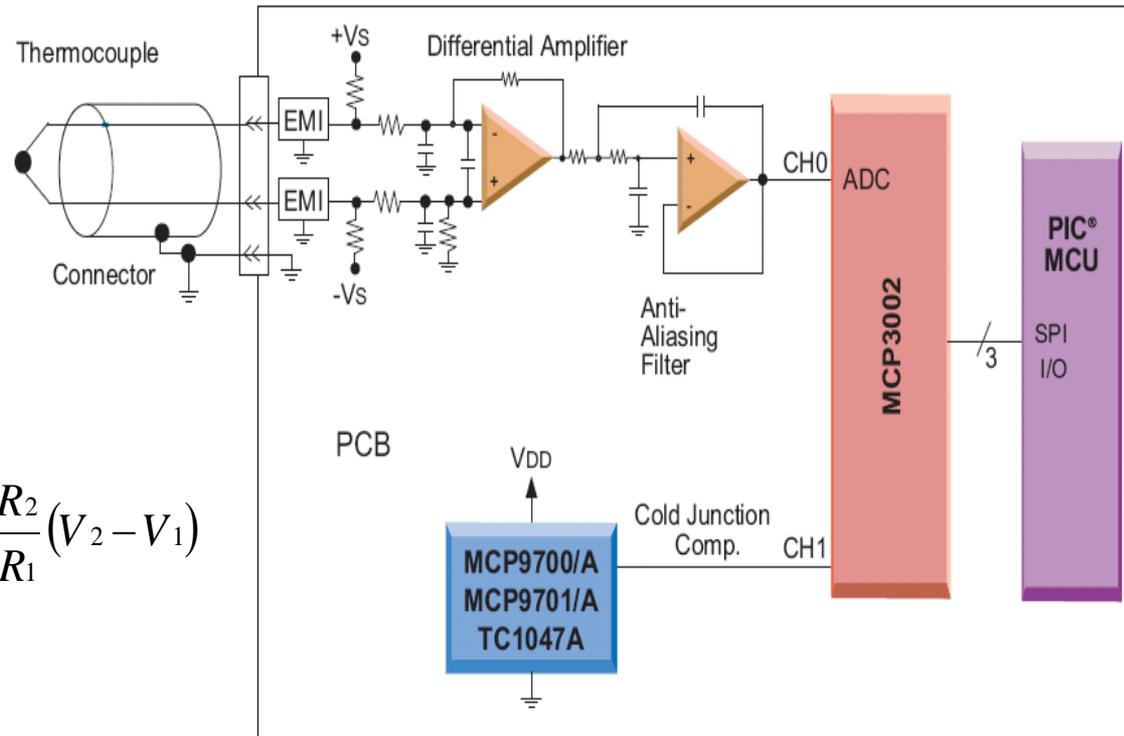
Filtered signal requires amplification

- Thermocouple output typically $\sim 40 \mu\text{V}/1^\circ\text{C}$
- A differential amplifier provides voltage gain and signal buffering
- Gain may be on the order of 50x to 500x

Critical design parameters:

- Input offset voltage
- Voltage offset drift
- Input bias current

$$V_{out} = \frac{R_2}{R_1} (V_2 - V_1)$$



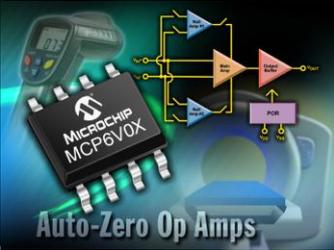


Offset Voltage and Drift

- **Large offset will affect temperature measurement if not calibrated out**
 - Thermocouple output typically $\sim 40 \mu\text{V}/1^\circ\text{C}$
 - Large offset limits ADC range which reduces sensing range
- **Voltage offset drifts over temperature**
 - Circuitry can experience wide temperature ranges
- **Three architectures that address these issues**
 - EPROM – Corrects input offset voltage through trimming algorithm completed at production final test
 - mCal – Implements onboard calibration circuit that calibrates input offset voltage at power up and by input on external pin
 - Auto-zero - Implements a nulling amplifier to continuously correct the input offset voltage of the main amplifier



Microchip Solutions

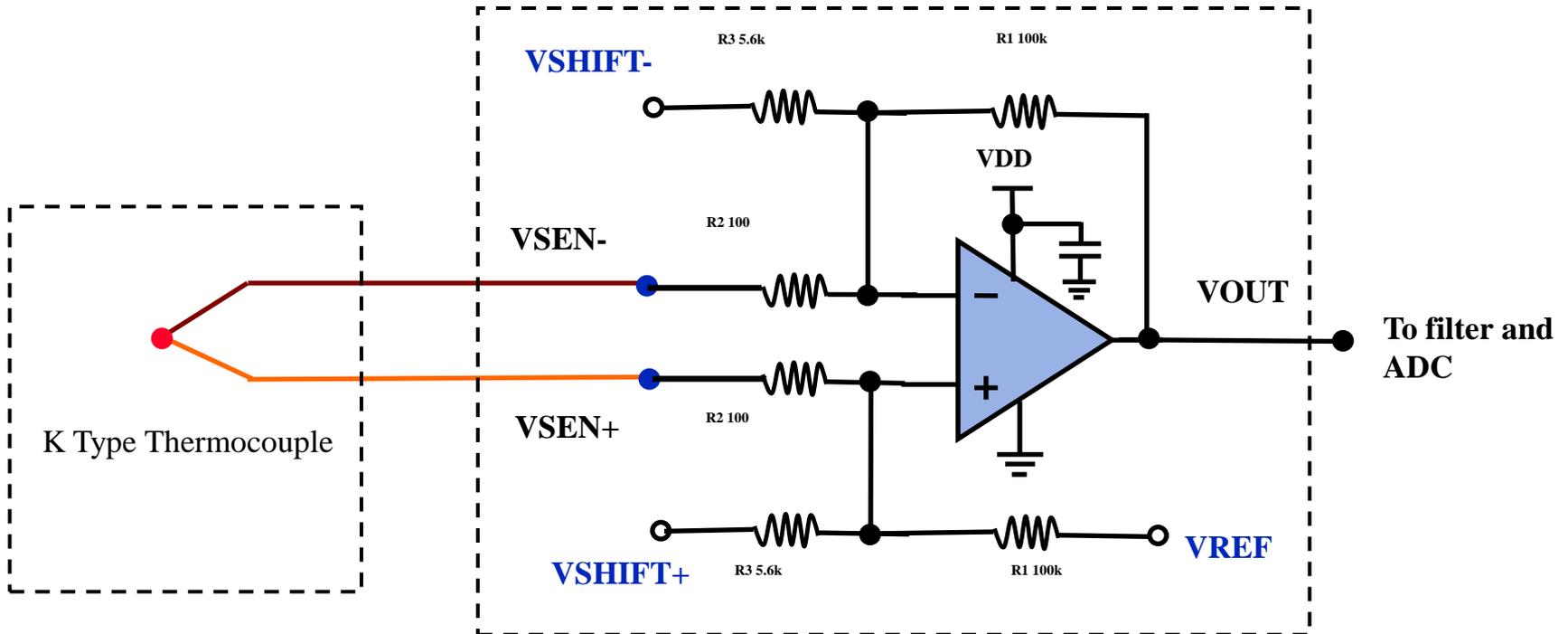
Types	Families	Max V_{os}	Advantages (+) / Disadvantages (-)
EPROM Trim 	MCP603X, MCP605X, MCP607X	150 μ V	+ Accurate initial offset + Competitive cost + Low power (0.9 μ A – Ideal for portable) - Experiences Offset drift
mCal 	MCP62X, MCP65X	200 μ V	+ External recalibration pin reduces drift + Accurate (initial and when recalibrated) + Very high GBWP (20-50 MHz) + User controlled recalibration - Higher current consumption
Auto-zero 	MCP6V0X	2-3 μ V	+ Extremely accurate + Not subject to drift + Continuous calibration (10000/sec) + No 1/f noise - Higher cost



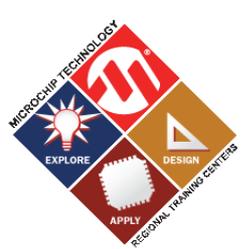
Thermocouple Conditioning Example

- Difference Amplifier
- It is implemented using the MCP6V01 auto-zeroed op amp and 0.1% tolerance resistors.

$$V_{OUT} = (R1/R2) * (V_{SEN+} - V_{SEN-}) + (R1/R3) * (V_{SHIFT+} - V_{SHIFT-}) + V_{REF}$$



Note: Refer to the board User's Guide for details



High Precision Circuits: Thermocouple Reference Design

– MCP6V01/2/3 & MCP6V06/7/8

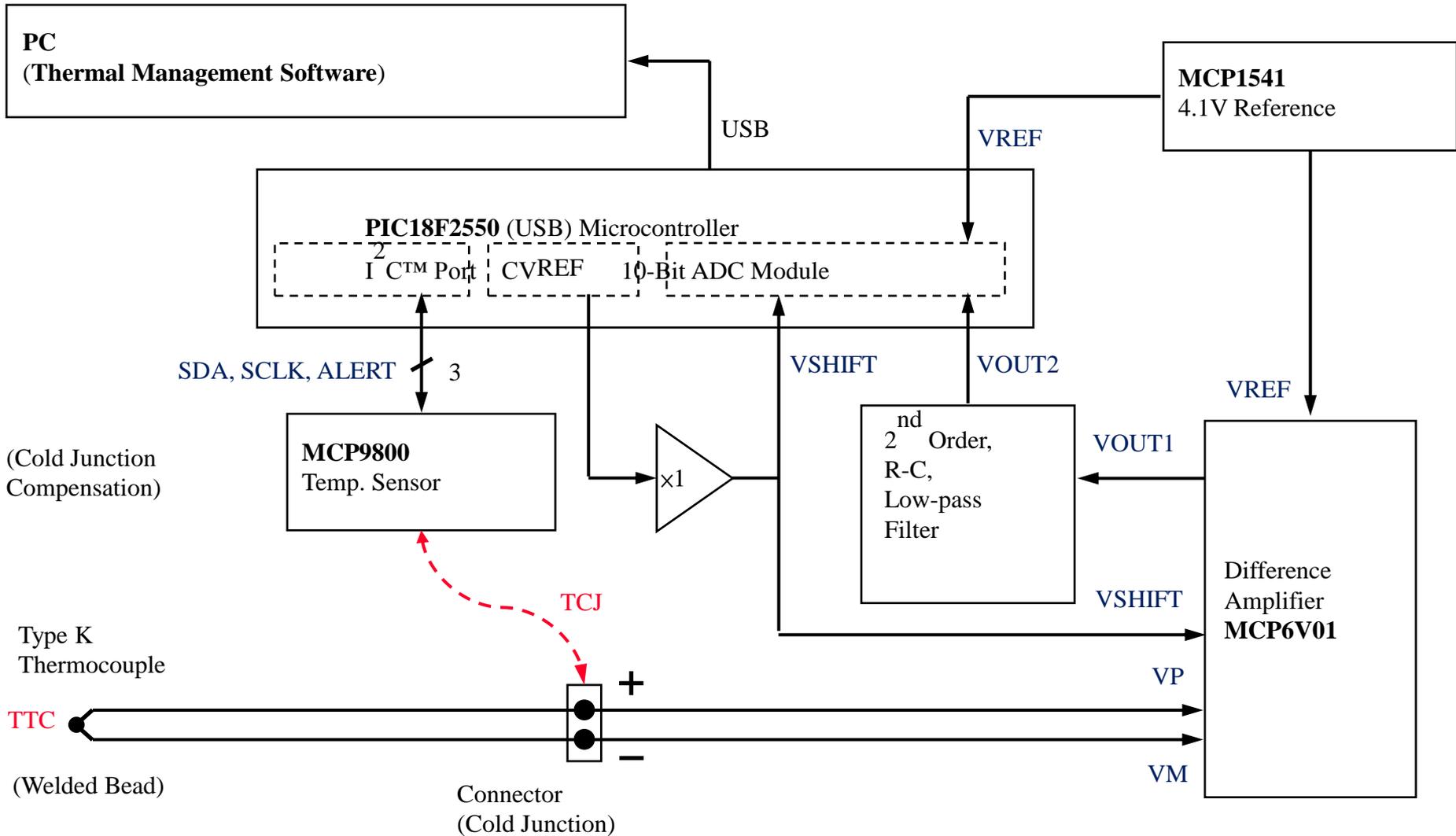
- V_{OS} Drift $\leq \pm 50$ nV/°C
- $V_{OS} \leq \pm 2$ μ V
- A_{OL} , CMRR, PSRR ≥ 130 dB

– Reference Design Features

- AZ OA Provides Gain for Thermocouple Voltage
- IC Temp Sensor for Cold Junction
- 14-Bit Resolution, 10-Bit ADC
 - PIC[®] device's V_{REF} (16 levels) subdivides input ranges
 - PIC device's ADC (10-bit) converts result and calibrates PIC device's CV_{REF}
 - Automatically searches for correct CV_{REF} value

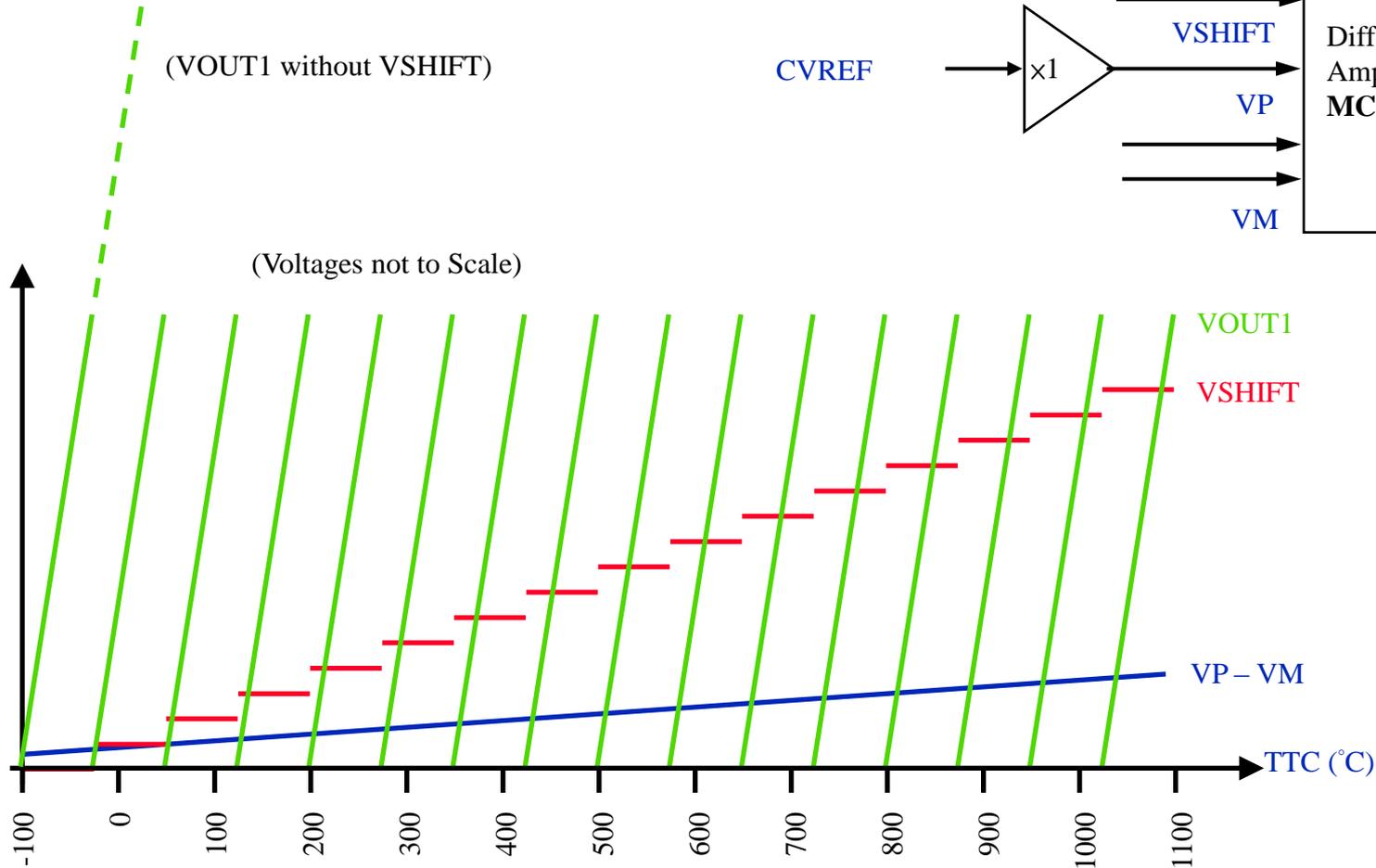
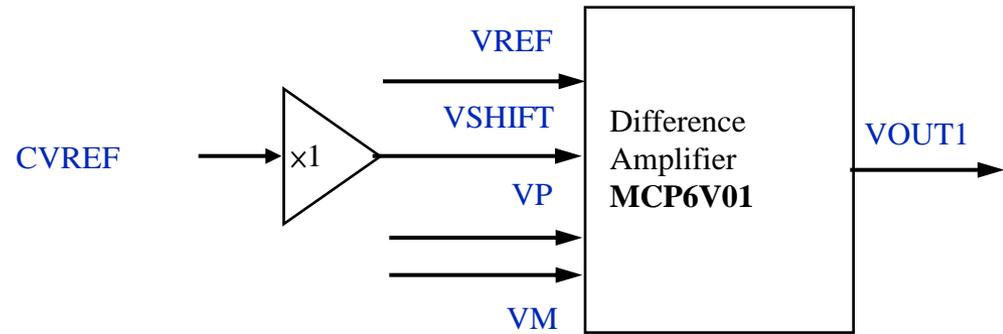


High Precision Circuits: Thermocouple Reference Design





High Precision Circuits: Thermocouple Reference Design

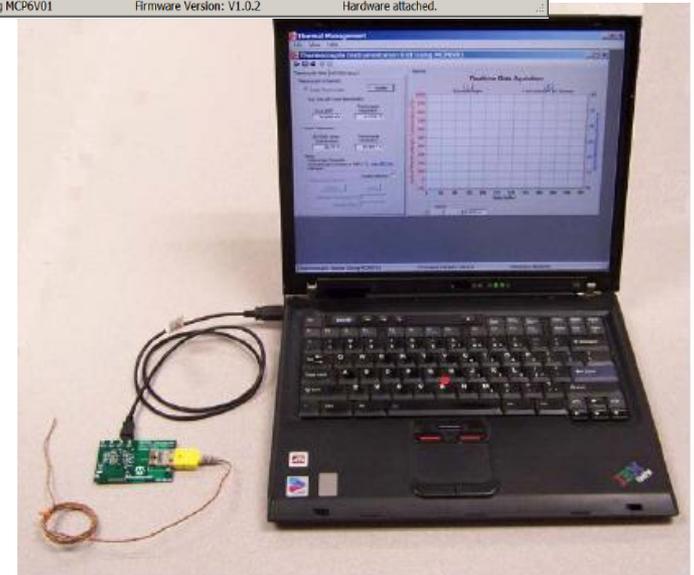
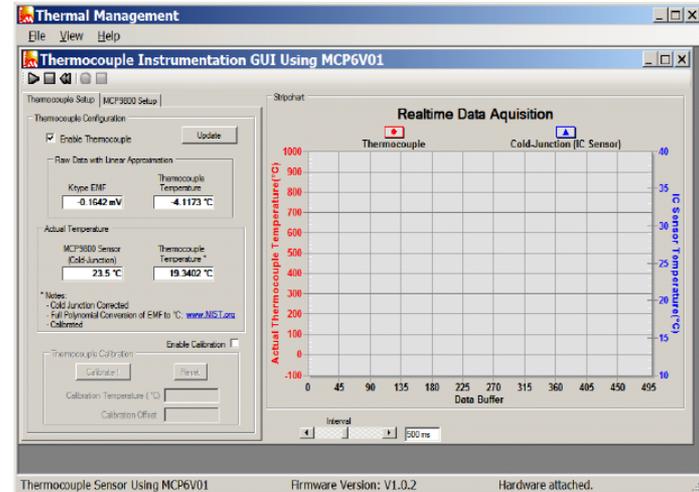




Auto-zero Thermocouple Reference Design

Features:

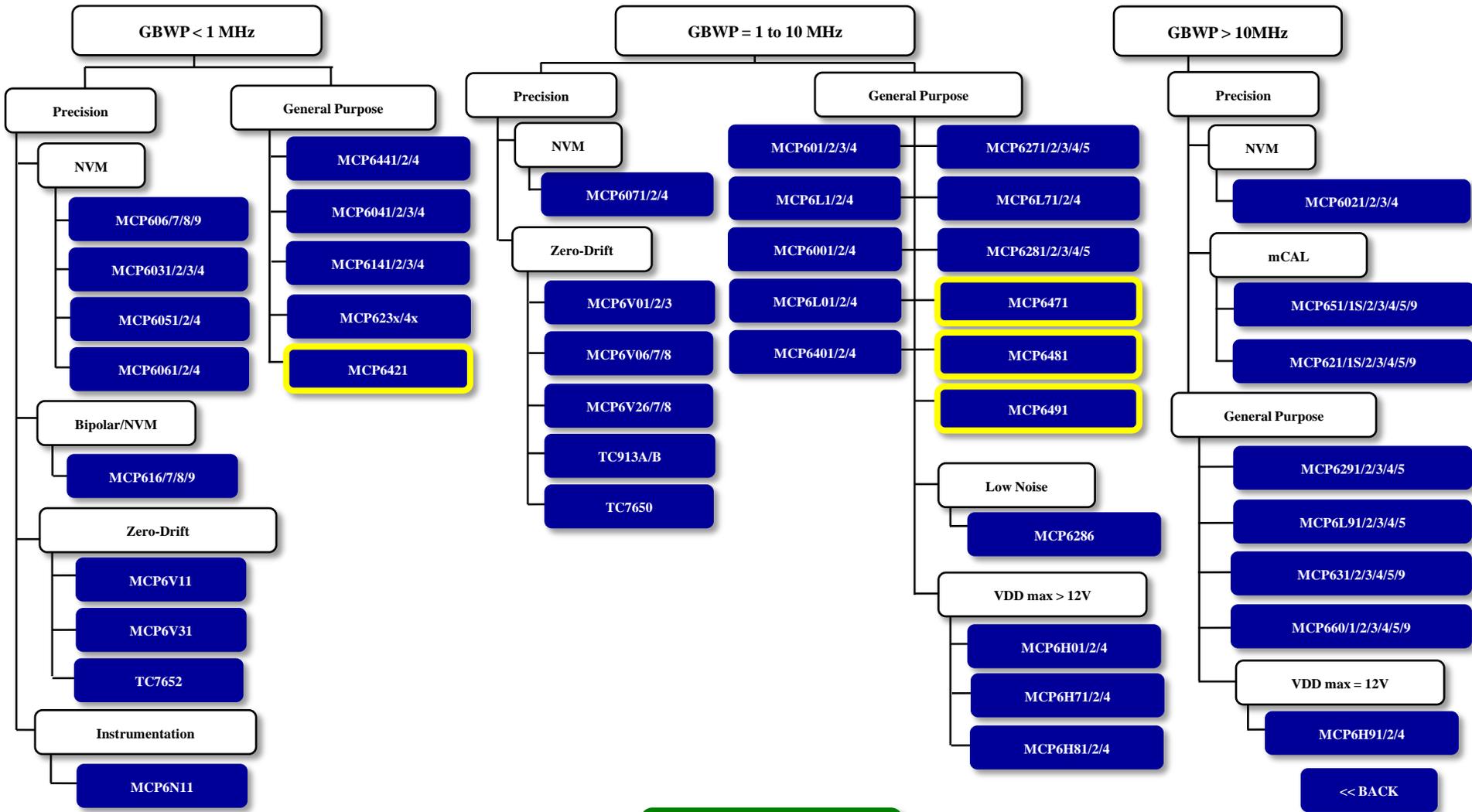
- Difference amplifier system for sensor conditioning
- Use the K-type thermocouple to sense temperature
- Temperature range is from -100°C to $+1000^{\circ}\text{C}$
- MCP9800 Temp Sensor used for cold junction compensation
- USB interface to transfer data to PC
- Test points for bench work



www.microchip.com/MCP6V0X
MCP6V01RD-TCPL



Operational Amplifiers



Linear
Demo & Eval Boards

<< BACK



High Speed Op Amps

● MCP62X/63X/65X/66X Key Specifications

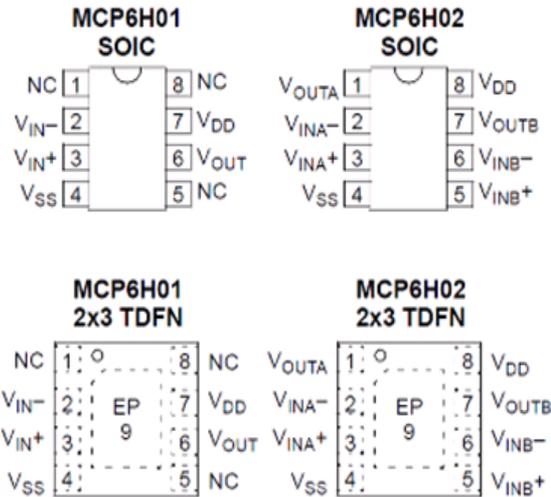
- **$I_{sc} = 70$ to 100 mA (typ.)**
 - Drive heavy loads (e.g., H-bridge, Transmission Line Driver, Audio Speaker)

- **GBWP = 20, 24, 50 and 60 MHz**
 - High speed (e.g., optical detector)
 - High gain (e.g., audio amplifier)

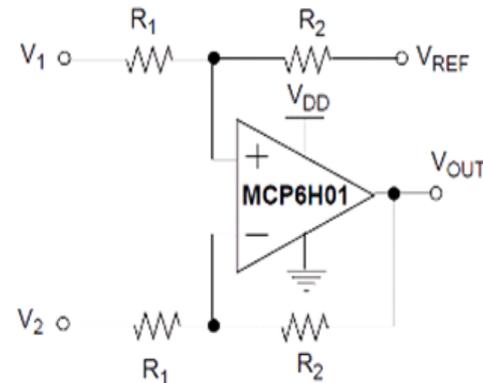
- **$e_{ni} = 13, 10, 7.5$ and 6.8 nV/ $\sqrt{\text{Hz}}$**
 - Very low white noise for CMOS (e.g., sensor amplifier)

Features

- Gain Bandwidth Product: 1.2 MHz (typ.)
- Low Power and Supply Voltages:
 - I_Q : 135 μA /amplifier (typ.)
 - Wide Supply Voltage Range: 3.5V to 16V
- High DC Precision:
 - Input Offset Voltage: ± 3.5 mV (max.)
 - V_{OS} Drift: ± 2.5 $\mu V/^\circ C$ (max.)
 - PSRR: 87 dB (min.)
 - CMRR: 78 dB (min.)
- Rail-to-Rail Output
- Unity Gain Stable
- Available in Single and Dual
- Extended Temperature Range: $-40^\circ C$ to $125^\circ C$



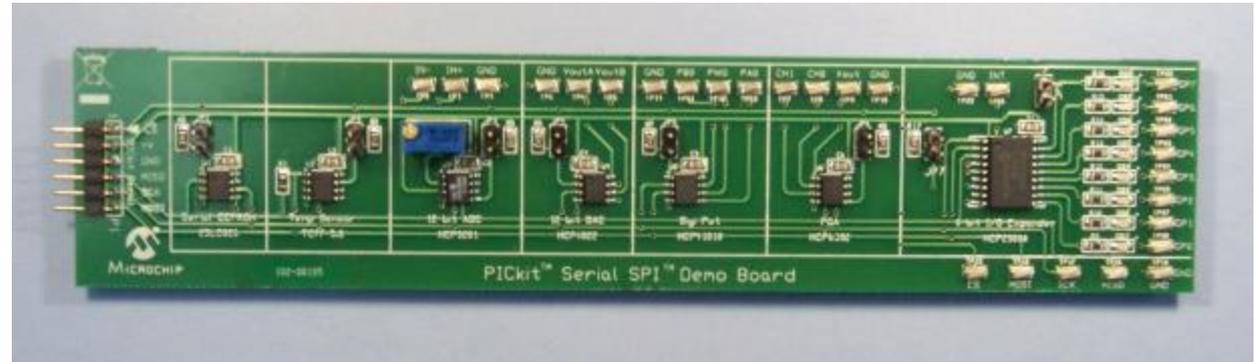
* Includes Exposed Thermal Pad (EP); see Table 3-1.



Difference Amplifier

<< BACK

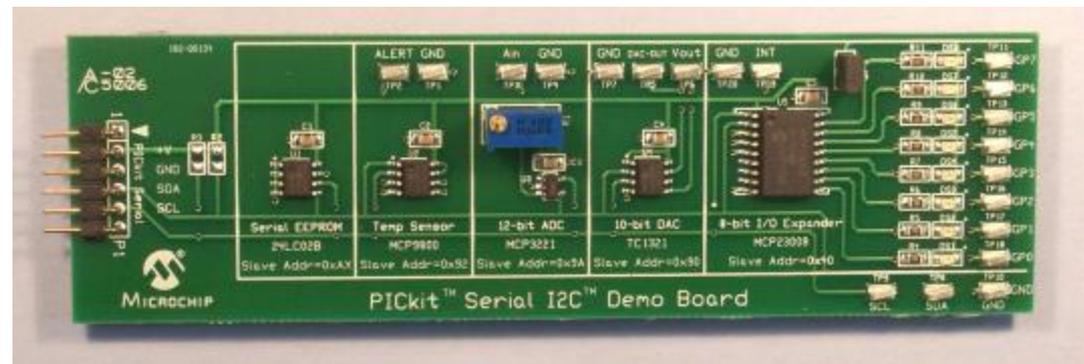
Reference Tools



SPI Demo Board



PICKit Serial Analyzer



I2C Demo Board



Product Selector Tools

● **Treelink** www.microchip.com/treelink

(2014-MAR, All New AIPD Inside, R&E)

- Gives brief overview of Microchip's Analog & Interface products
- View products of interest by clicking on dynamic links on the product trees

The screenshot shows the Microchip website's product selector tool for Analog & Interface products. The interface is organized into a grid of product categories, each with a list of specific components. The categories are: THERMAL MANAGEMENT, LINEAR, POWER MANAGEMENT, MIXED SIGNAL, and INTERFACE. At the bottom, there are buttons for 'Updates', 'Go to Analog & Interface Overview', and 'Go to Demo & Eval Boards'.

THERMAL MANAGEMENT	POWER MANAGEMENT	MIXED SIGNAL	INTERFACE
Temperature Sensors	Linear Regulators	Delta-Sigma A/D Converters	CAN/LIN Peripherals
Brushless DC Fan Speed Controllers Fan Fault Detectors	Switching Regulators/Controllers	SAR A/D Converters	Serial Peripherals
	Charge Pump DC/DC Converters	Energy Measurement ICs	Ethernet Controller
LINEAR	Voltage References	Dual Slope / Display A/D Converters	RF & Infrared
Single Supply CMOS Op Amps	CPU/System Supervisors	D/A Converters	SAFETY AND SECURITY
Comparators	Voltage Detectors	V/F and F/V Converters	Smoke Detectors IC
Programmable/Selectable Gain Amps	Power MOSFET Drivers	Digital Potentiometers	Piezoelectric Horn Drivers
	Battery Management		
	PWM Controller	Go to Analog & Interface Overview	Go to Demo & Eval Boards



Stand-Alone Analog and Interface Solutions

Analog and Interface Solutions Brochure

DS20001060AD → Download from **WEBSITE**

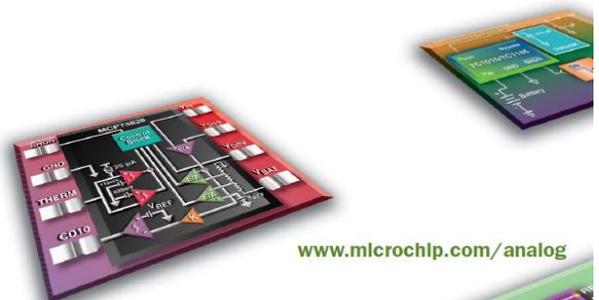
Provides quick overview of critical parameters, features and packages

Analog and Interface Product Solutions
Summer 2010



Analog and Interface Product Selector Guide

- Thermal Management
- Battery Management
- Interface Peripherals
- Power Management
- Linear & Mixed-Signal
- Safety & Security



www.microchip.com/analog

THERMAL MANAGEMENT

THERMAL MANAGEMENT PRODUCTS – Temperature Sensors							
Part #	Typical Accuracy (°C)	Maximum Accuracy @ 25°C (°C)	Maximum Temperature Range (°C)	Vcc Range (V)	Maximum Supply Current (µA)	Features	Packages
Logic Output Temperature Sensors							
TC601	±0.5	±3	-55 to +125	+2.7 to +5.5	40	Cross to MAX6011, Open-drain	5-pin SOT-23A
TC602	±0.5	±3	-55 to +125	+2.7 to +5.5	40	Cross to MAX6012, Push-pull	5-pin SOT-23A
TC603	±0.5	±3	-55 to +125	+2.7 to +5.5	40	Cross to MAX6013, Open-drain	5-pin SOT-23A
TC604	±0.5	±3	-55 to +125	+2.7 to +5.5	40	Cross to MAX6014, Push-pull	5-pin SOT-23A
TC620	±1	±3	-40 to +125	+4.5 to +18	400	Two resistor-programmable IIP points	8-pin PDIP, 8-pin SOIC
TC621	Note 1	Note 1	-40 to +65	+4.5 to +18	400	Requires external divider, resistor-programmable IIP points	8-pin PDIP, 8-pin SOIC
TC622	±1	±5	-40 to +125	+4.5 to +18	600	Dual output, TO-220 for heat sink mounting, resistor-programmable IIP points	8-pin PDIP, 8-pin SOIC, 5-pin TO-220
TC623	±1	±3	-40 to +125	+2.7 to +4.5	250	Two resistor-programmable IIP points	8-pin PDIP, 8-pin SOIC
TC624	±1	±5	-40 to +125	+2.7 to +4.5	300	Dual output, resistor-programmable IIP points	8-pin PDIP, 8-pin SOIC
Voltage Output Temperature Sensors							
MCP9700	±1	±4	-40 to +125	+2.3 to +5.5	12	Linear Active Thermistor ¹ IC, Temperature slope: 10 mV/°C	3-pin TO-92, 5-pin SC-70, 3-pin SOT-23
MCP9701	±1	±4	-30 to +125	+3.1 to +5.5	12	Linear Active Thermistor ¹ IC, Temperature slope: 19.53 mV/°C, cross to MAX6912	3-pin TO-92, 5-pin SC-70, 3-pin SOT-23
MCP9700A	±1	±2	-40 to +125	+2.3 to +5.5	12	Linear Active Thermistor ¹ IC, Temperature slope: 10 mV/°C	3-pin TO-92, 5-pin SC-70, 3-pin SOT-23
MCP9701A	±1	±2	-40 to +125	+3.1 to +5.5	12	Linear Active Thermistor ¹ IC, Temperature slope: 19.53 mV/°C, cross to MAX6912	3-pin TO-92, 5-pin SC-70, 3-pin SOT-23
TC1046	±0.5	±2	-40 to +125	+2.7 to +4.4	80	High precision temperature-to-voltage converter, 6.25 mV/°C	3-pin SOT-23B
TC1047	±0.5	±2	-40 to +125	+2.7 to +4.4	80	High precision temperature-to-voltage converter, 10 mV/°C	3-pin SOT-23B
TC1047A	±0.5	±2	-40 to +125	+2.5 to +5.5	80	High precision temperature-to-voltage converter, 10 mV/°C	3-pin SOT-23B
Serial Output Temperature Sensors							
MCP9800	±0.5	±1	-55 to +125	+2.7 to +5.5	400	5Mbit/s ² compatible interface, 0.0625°C to 0.5°C adj. resolution, power-saving one-shot temperature measurement	5-pin SOT-23
MCP9801	±0.5	±1	-55 to +125	+2.7 to +5.5	400	5Mbit/s ² compatible interface, 0.0625°C to 0.5°C adj. resolution, power-saving one-shot temperature measurement, multi-drop capability	8-pin MSOP, 8-pin SOIC
MCP9802	±0.5	±1	-55 to +125	+2.7 to +5.5	400	5Mbit/s ² compatible interface with time-out, 0.0525°C to 0.5°C adj. resolution, power-saving one-shot temperature measurement, multi-drop capability	5-pin SOT-23
MCP9803	±0.5	±1	-55 to +125	+2.7 to +5.5	400	5Mbit/s ² compatible interface with time-out, 0.0525°C to 0.5°C adj. resolution, power-saving one-shot temperature measurement, multi-drop capability	8-pin MSOP, 8-pin SOIC
MCP9805	±0.5	±1 ¹	-20 to +125	+3.0 to +3.5	400	JTEC compatible register set, 5Mbit/s ² compatible interface, programmable, shut-down mode and EVENT output	8-pin TSSOP, 8-pin 2cd DFN
MCP98042	±0.5	±1 ¹	-20 to +125	+3.0 to +3.5	400	Serial temperature sensor on MCP9805 plus integrated I2C ² Serial Presence Detect EEPROM	8-pin TSSOP, 8-pin 2cd DFN
TC77	±0.5	±1	-55 to +125	+2.7 to +5.5	400	SPI compatible interface, 0.0625°C temperature resolution	8-pin SOT-23A, 8-pin SOIC
TC72	±0.5	±1	-55 to +125	+2.65 to +5.5	400	SPI compatible interface, power-saving one-shot temperature measurement, 0.25°C temperature resolution	8-pin MSOP, 8-pin 2cd DFN
TC74	±0.5	±2	-40 to +125	+2.7 to +5.5	350	5Mbit/s ² compatible interface, 1°C temperature resolution	5-pin SOT-23A, 5-pin TO-220

Note 1: These devices use an external temperature sensor. Accuracy of the total solution is a function of the accuracy of the external sensor.
Note 2: Maximum accuracy measured at 85°C.



Take a Break

Treelink for AIPD Introduction

1. Product Portfolio
2. Demo Board
3. Company profile



Op Amp

Application Circuits



Op Amp Application Circuits

Applications

- **Inverting Amplifier / Non-inverting Amplifier / Voltage Follower / Difference Amplifier**
- **Instrumentation Amplifier**
- **Summing Amplifier**
- **Current to Voltage Amplifier**
- **Voltage to Current Amplifier**
- **Comparator**
- **Electronic Filters**
- **Others**



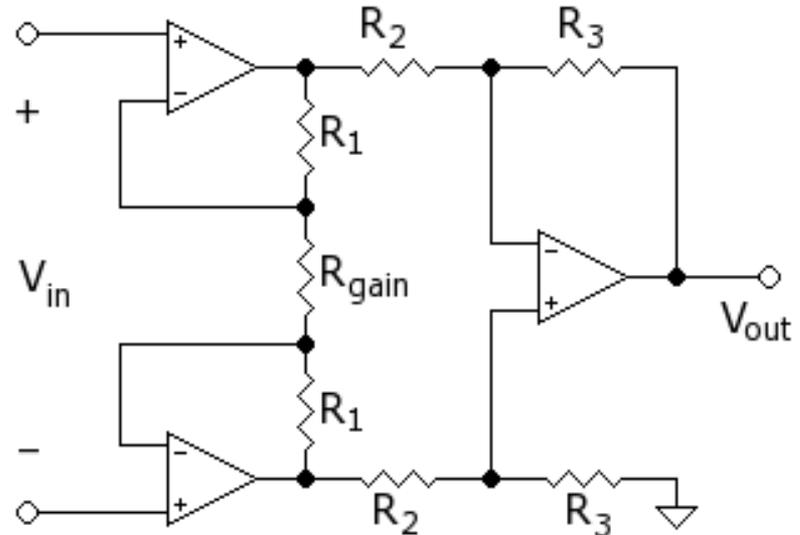
Op Amp Application Circuits

Instrumentation Amplifier (MCP6N11: New)

- It is widely used in the very accurate, low noise measurements because of the following properties:
 - Very high input impedance
 - High common-mode rejection ratio
 - Low DC offset

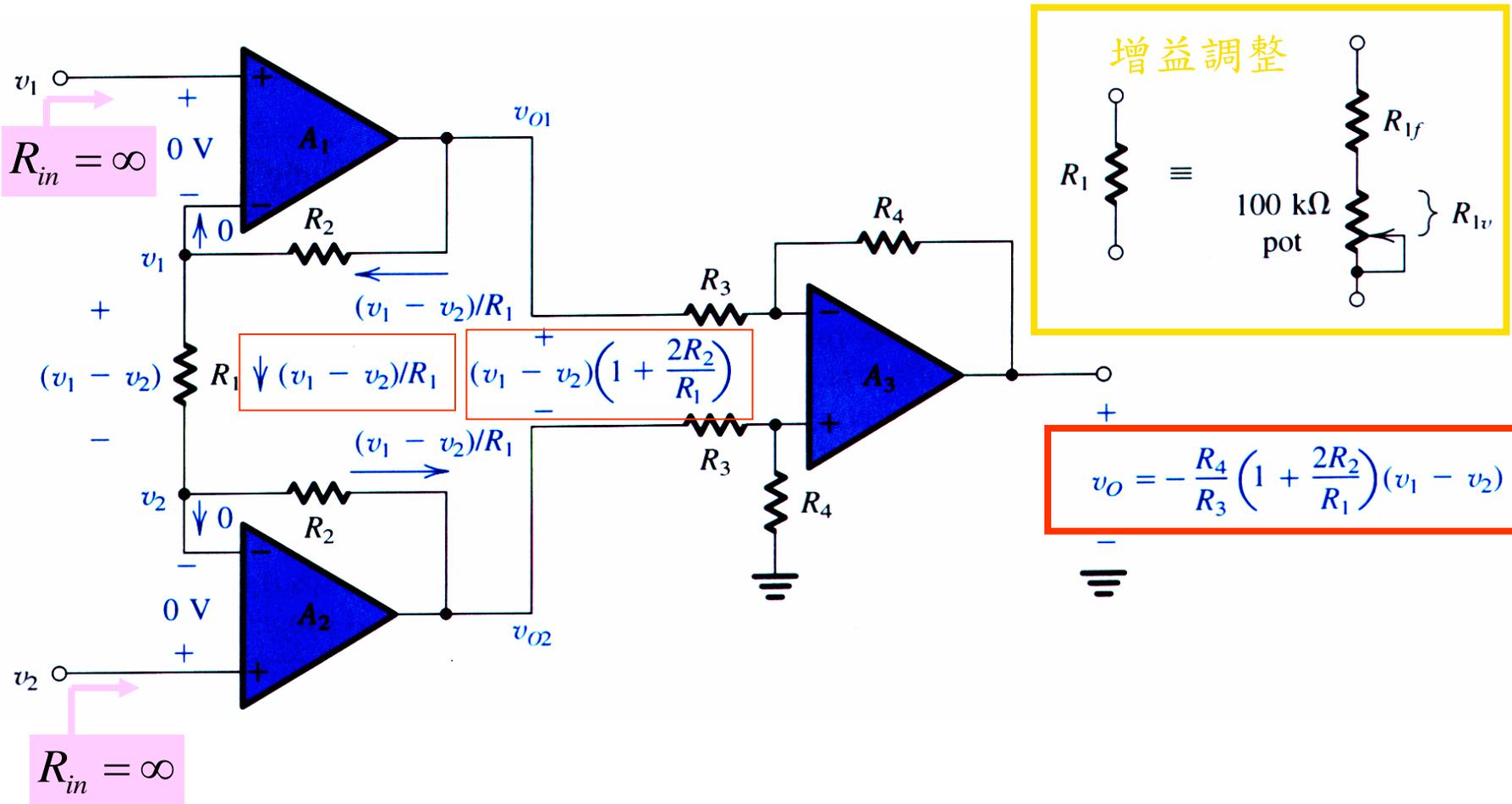
It is made by adding a non-inverting buffer to each input of the difference amplifier.

$$V_{OUT}/V_{IN} = (1 + 2R_1/R_{gain})(R_3/R_2)$$





儀器放大器 (instrumentation amplifier)





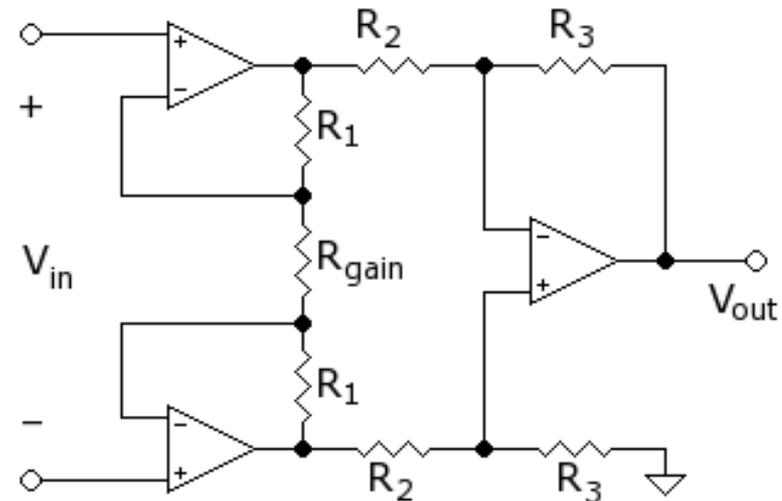
Op Amp Application Circuits

Exercise #22

- The instrumentation amplifier has a differential gain, variable in the range 1 to 50, the second stage for a gain of 0.5, $R_1 = 50\text{k}\Omega$. Give the value range of variable resistor R_{gain} . [Recall: $G = V_{\text{OUT}}/V_{\text{IN}} = (1+2R_1/R_{\text{gain}})(R_3/R_2)$]

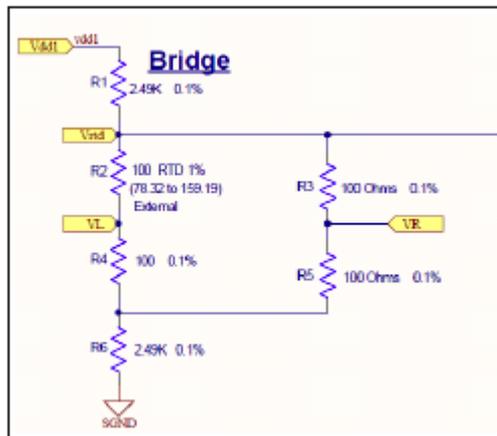
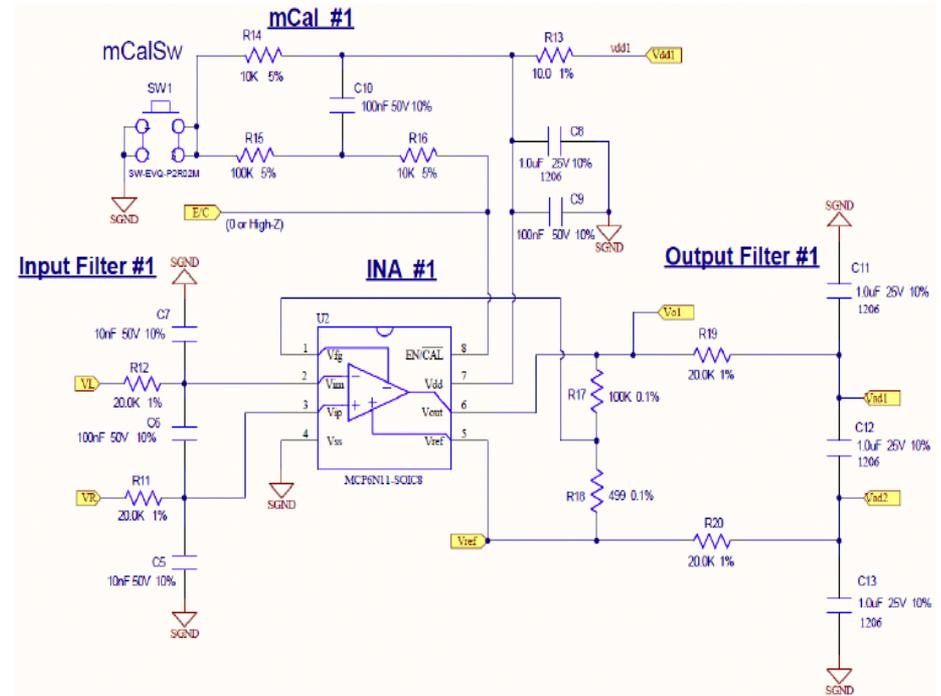
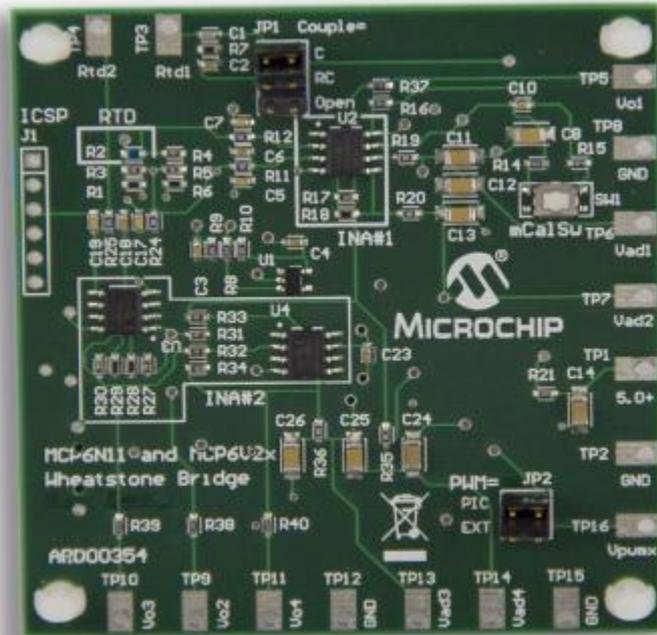
Solution #22

- $G = (1+2R_1/R_{\text{gain}})(R_3/R_2)$
 $= (1+100\text{k}\Omega/R_{\text{gain}})(0.5)$
- When $G = 1$, $R_{\text{gain}} = 100\text{k}\Omega$
 When $G = 50$, $R_{\text{gain}} \approx 1\text{k}\Omega$





MCP6N11 v.s. MCP6V0X Demo Board



$$G_{DM} = 1 + R_F/R_G$$

$$V_{OUT} = V_{CNT}$$

$$V_M = V_{REF} + G_{DM}(1 + g_E)V_E$$



Op Amp Application Circuits

Summing Amplifier (Inverting/Non-Inverting)

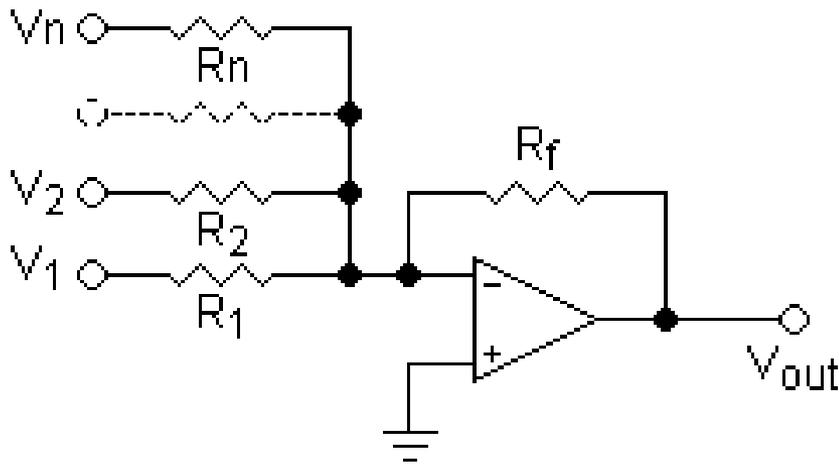
- The output voltage is a weighted sum of the input signals V_1, V_2, \dots, V_n

Hint: Superposition Principle

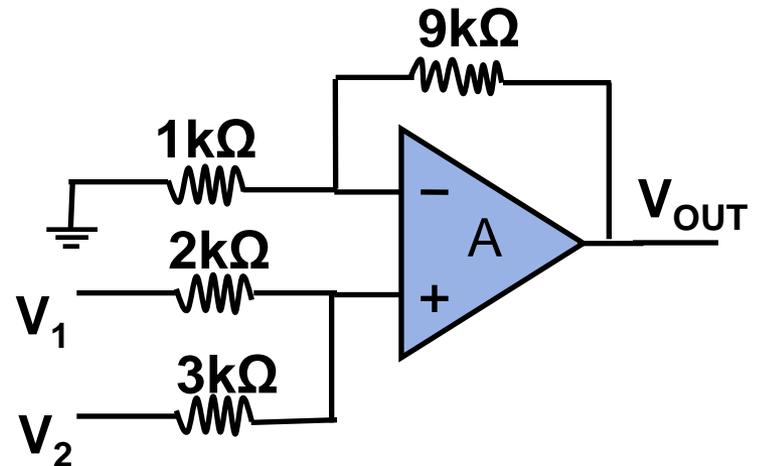
Let $V_1 = 0$, calculate V_{O1}

Let $V_2 = 0$, calculate V_{O2}

Finally, $V_{OUT} = V_{O1} + V_{O2}$



$$V_{out} = -R_f \left(\frac{V_1}{R_1} + \frac{V_2}{R_2} + \dots + \frac{V_n}{R_n} \right)$$

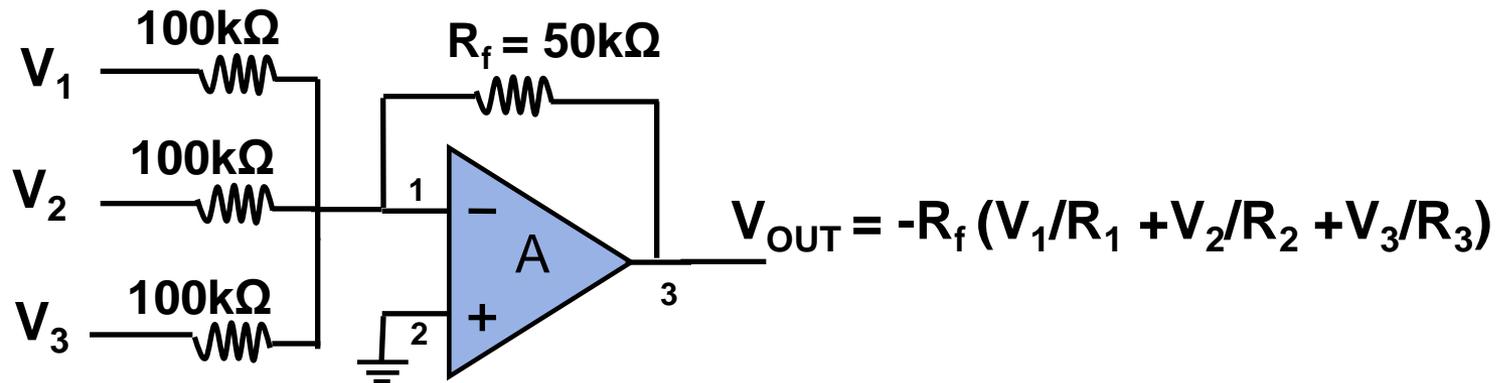




Op Amp Application Circuits

Exercise #23

- An inverting summing amplifier has three inputs using 100kΩ resistors and a feedback resistor of 50kΩ.
- Express V_{OUT} in terms of V_1 , V_2 , V_3 .
- If $V_1 = V_2 = 2V$ and $V_3 = -1V$, what is V_{OUT} ?



Solution #23

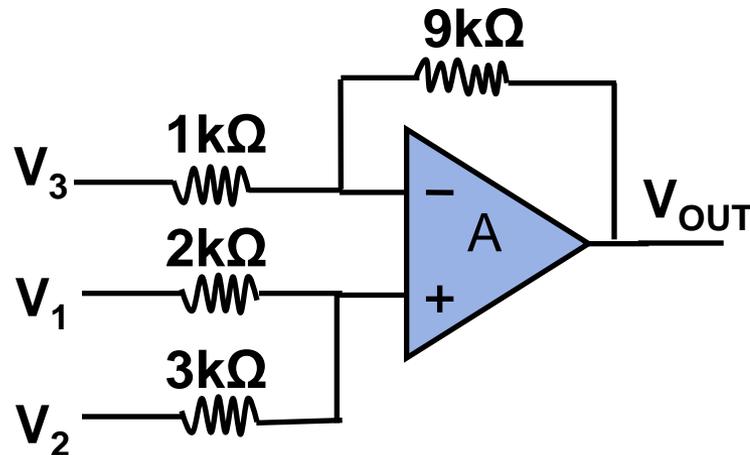
- $V_{OUT} = -50 * (V_1/100 + V_2/100 + V_3/100) = -1.5V$



Op Amp Application Circuits

Exercise #24

- If the $1\text{k}\Omega$ resistor is disconnected from ground and connected to a third signal source V_3 , please use superposition to determine V_{OUT} in terms of V_1 , V_2 , and V_3 .



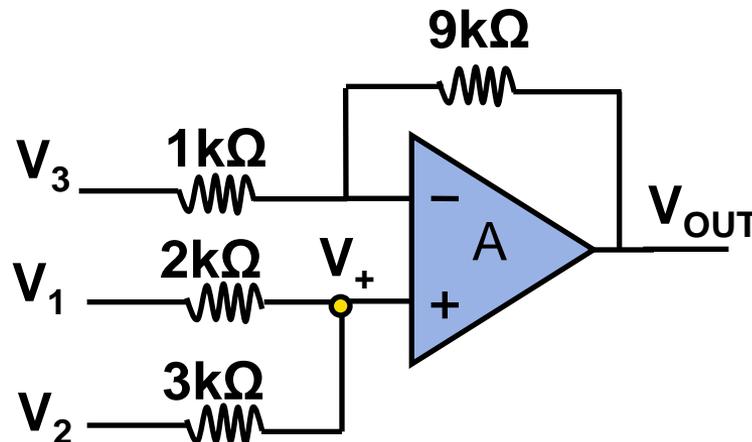
Hint: Superposition Principle



Op Amp Application Circuits

Solution #24

- For V_3 , let $V_1 = 0$, $V_2 = 0 \rightarrow V_{O3} = -(9k/1k)*V_3 = -9V_3$
From Exercise #23, we already got
For $V_1 \rightarrow V_{O1} = 6V_1$; For $V_2 \rightarrow V_{O2} = 4V_2$
- Finally, $V_{OUT} = V_{O1} + V_{O2} + V_{O3} = 6V_1 + 4V_2 - 9V_3$

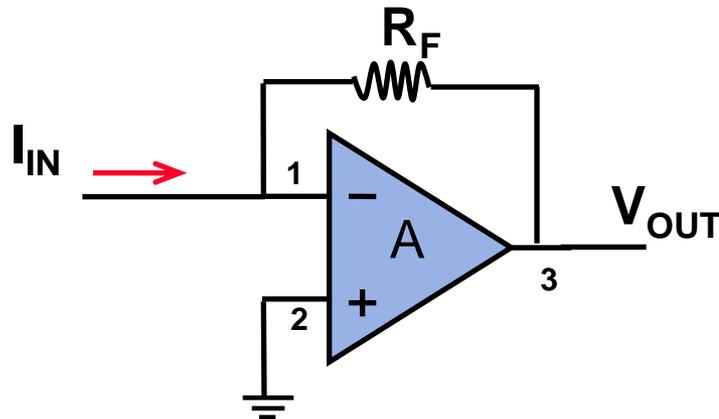




Op Amp Application Circuits

Current to Voltage Amplifier (Transimpedance Amplifier)

- A circuit for converting small current signals to a more easily measured proportional voltage signals.
- I_{IN} must flow through R_F and the output voltage is expressed by $V_{OUT} = -I_{IN}R_F$.

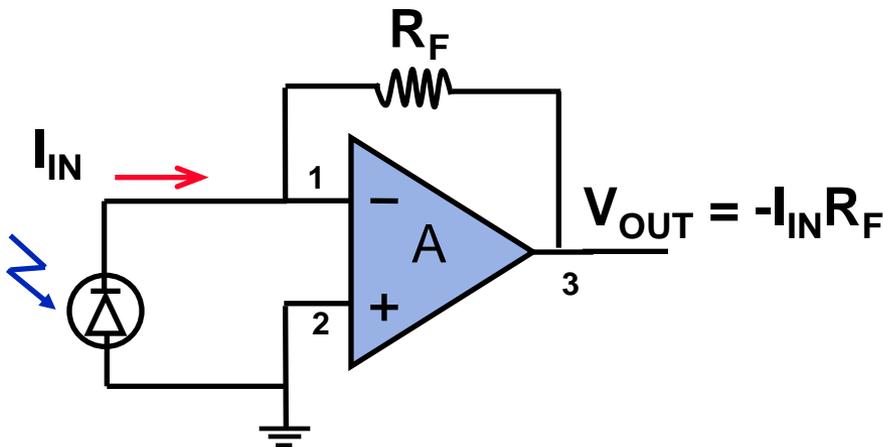




Op Amp Application Circuits

Example: Photodiode Light Detector

- This light detector is a current-to-voltage converter.
 - The generated photocurrent is proportional to incident light.
 - $V_{OUT} = -I_{IN}R_F$
 - **V_{OUT} is proportional to the incident light.**



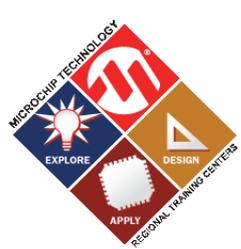
The value of R_F should be chosen to ensure V_{OUT} swings within the maximum output voltage dynamic range.



Technical Support

- **Documentation links**
 - **User's Guide: [MCP6031 Photodiode PICtail Plus Demo Board User's Guide](#)**
 - **Product Datasheet: [MCP6031](#)**
 - **Application Note: [AN951](#)**
 - **[Product Selection Tools](#)**

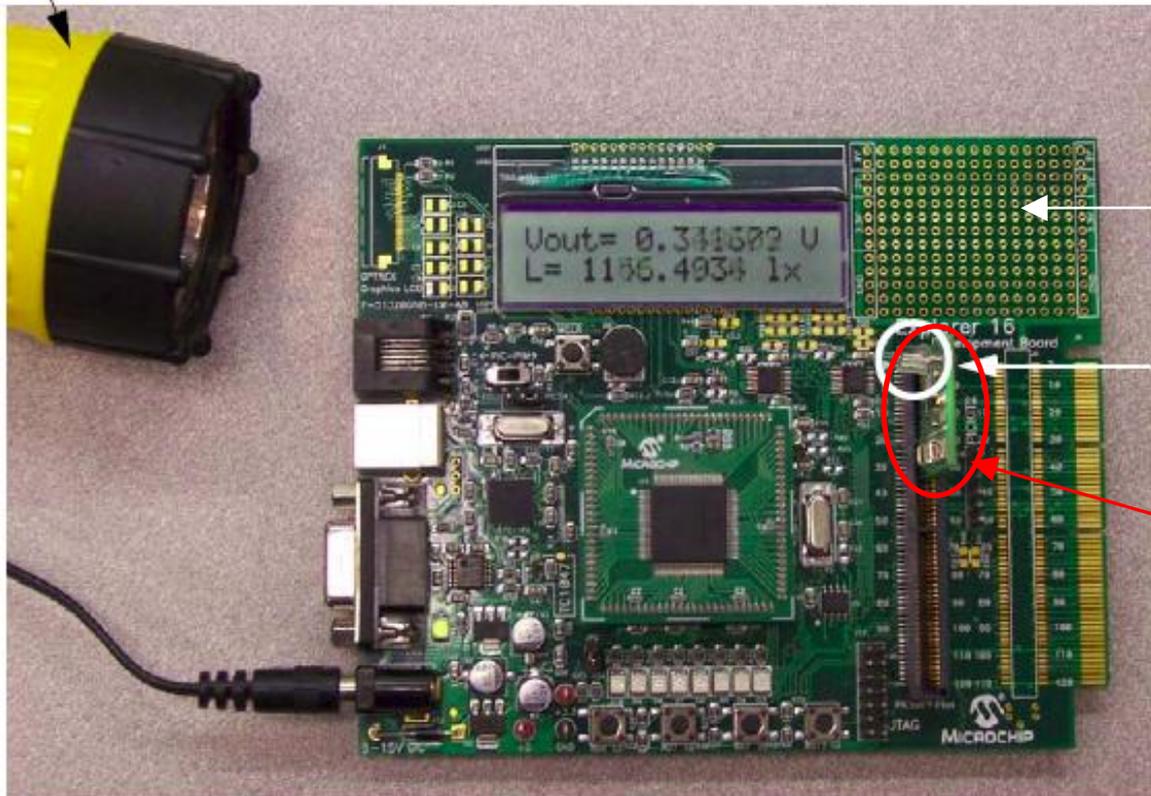




Board Operation

- The figure shows data taken near an incandescent lamp powered by a battery

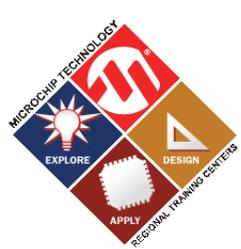
Incandescent lamp



Explorer 16
Development Board

PIN Photodiode

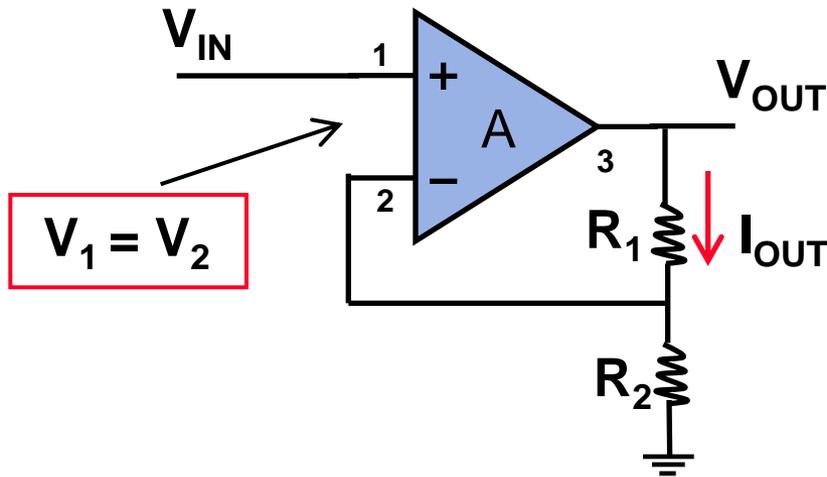
MCP6031 Photodiode
PICtail Plus Demo Board



Op Amp Application Circuits

Voltage to Current Amplifier

- The current output through the load resistor is proportional to the input voltage.
- $I_{OUT} = V_{IN}/R_2$, which is independent of R_1 .



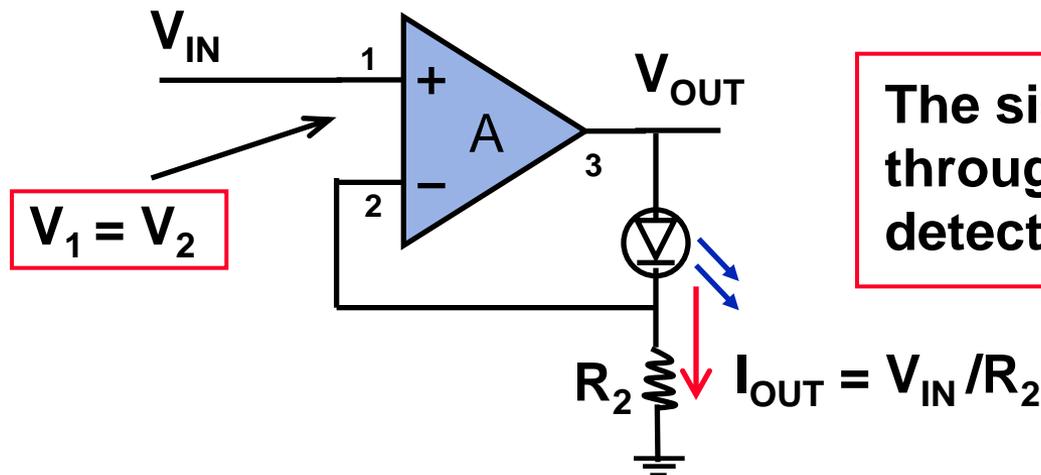
R_1 is the load and the current through it is the desired output signal.



Op Amp Application Circuits

Example: Light Emitting Diode (LED) Modulator

- The light output from an LED: Linearly proportional to the current (I_{OUT}) through the diode
- $I_{OUT} = V_{IN}/R_2$
- **The light level is proportional to input signal (V_{OUT}).**



The signal can then be send through a fiber optic cable and detected on the other end.

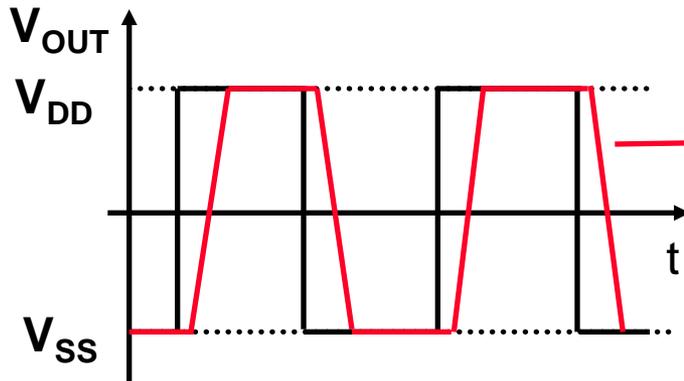
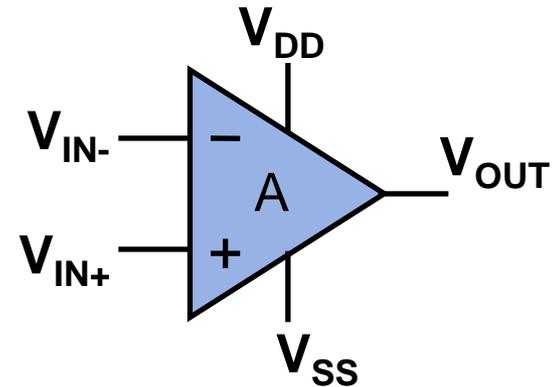


Op Amp Application Circuits

Comparator

- A standard op amp can be used as a comparator in open loop mode.

- $V_{OUT} = V_{DD}$ when $V_{IN+} > V_{IN-}$
- $V_{OUT} = V_{SS}$ when $V_{IN+} < V_{IN-}$



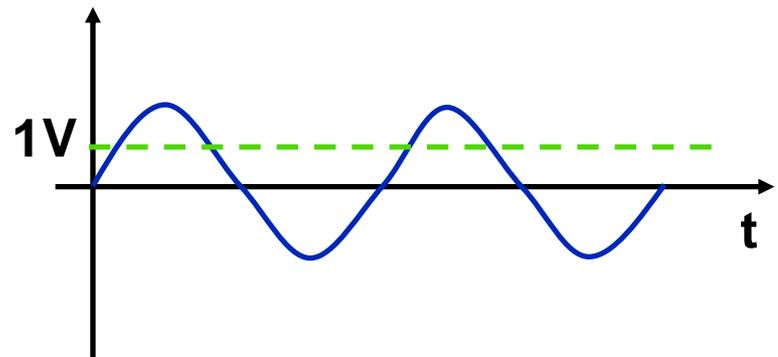
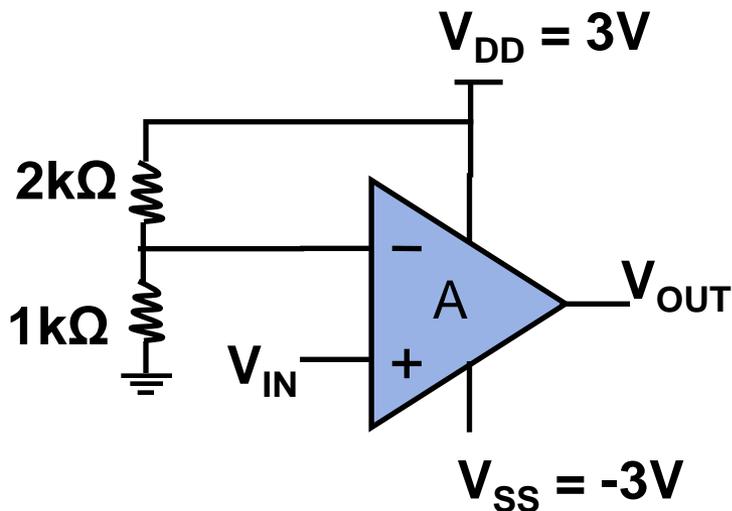
The switching time between V_{SS} and V_{DD} is limited by op amp slew rate. (Propagation Delay)

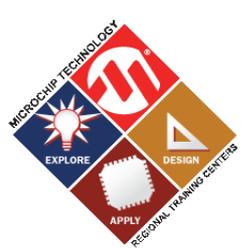


Op Amp Application Circuits

Exercise #25

- Level detector: another name for a comparator used to compare an input voltage to a fixed dc reference voltage.
 - For $V_{IN} = 2V$ and $0.5V$, what is V_{OUT} respectively?
 - If V_{IN} is a sine wave, what is the wave form of V_{OUT} ?

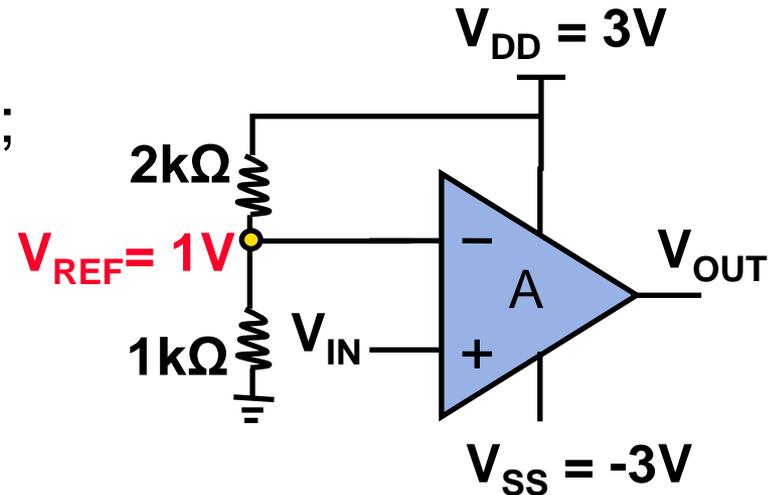




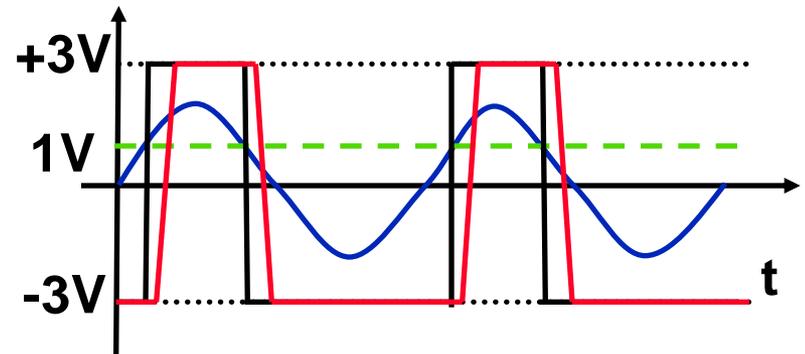
Op Amp Application Circuits

Solution #25

- $V_{ref} = [3V / (2k\Omega + 1k\Omega)] * 1k\Omega = 1V;$
 $V_{IN} = 2V > V_{ref} = 1V, V_{OUT} = 3V;$
 $V_{IN} = 0.5V < V_{ref} = 1V, V_{OUT} = -3V$
- V_{IN} is a sine wave, V_{OUT} ?



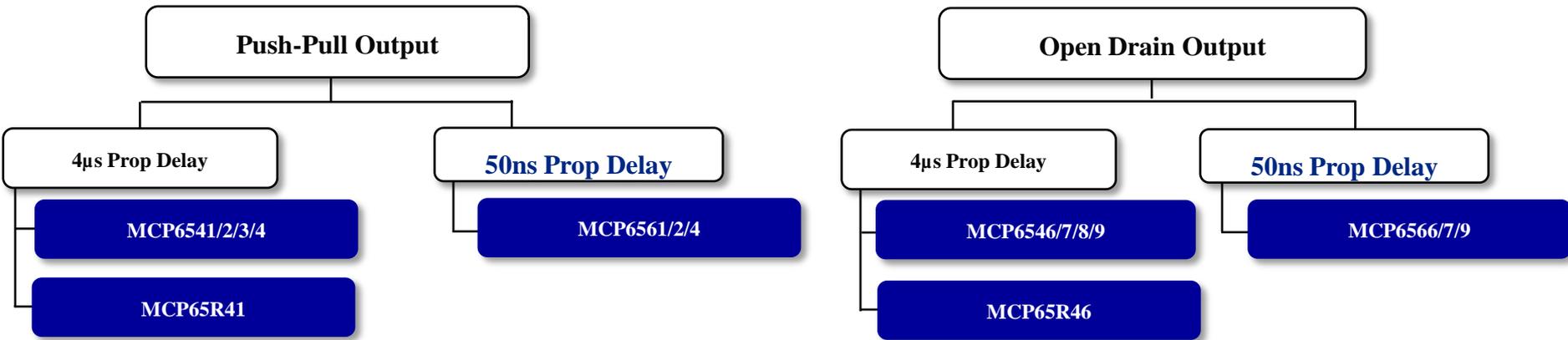
- I. Slew rate limits switching time.
 - II. Open loop gain BW limits the sine wave frequency.
- Recall:** Open loop gain BW drops very fast with frequency.



- Application: Pulse-width modulator.** That is, the DC reference voltage controls, or modulates the pulse width of the output voltage.



Comparators



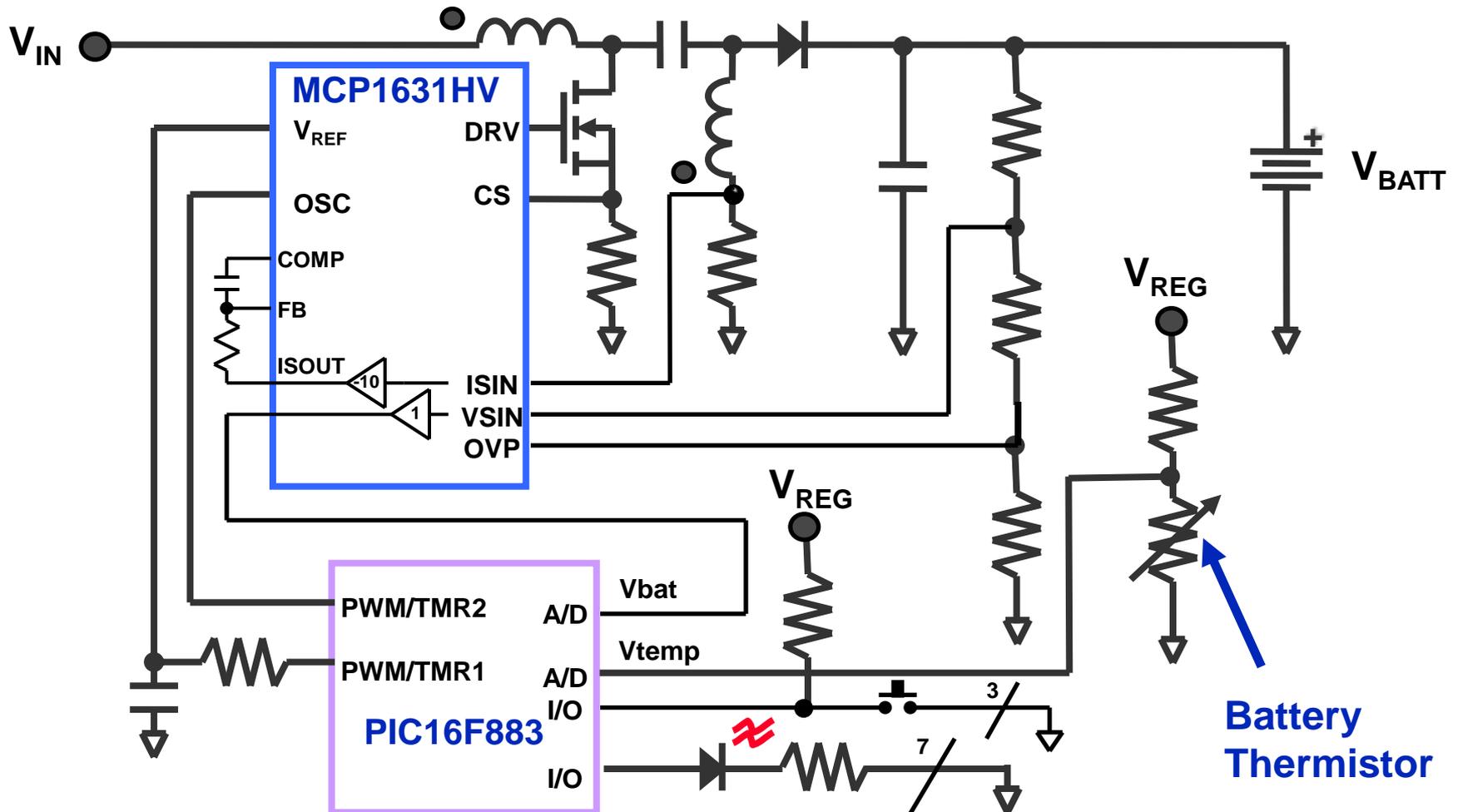
<< BACK

General Purpose
Demo & Eval Boards



Multi-Chemistry Design

Charger Block Diagram



Battery Thermistor



Op Amp Application Circuits

Electronic Filter

- Electronic filters perform signal processing functions
 - **Remove unwanted signal components and/or enhance wanted ones.**

- Classification by technology
 - **Passive filter**
 - **Active filter**



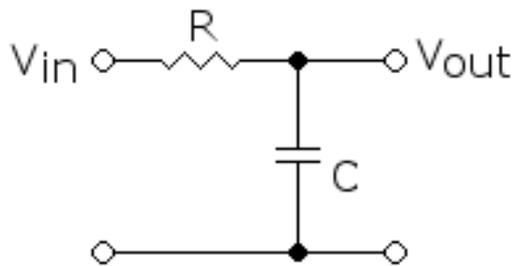
Op Amp Application Circuits

Passive Filter

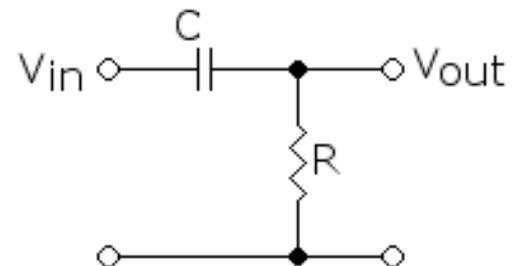
- A passive filter is an electronic filter made entirely from passive components.

A passive component does not require a source of energy to perform its intended function, such as resistors, capacitors, and inductors.

- These filters exist in so-called RC, RL, LC and RLC varieties.



A passive low-pass filter



A passive high-pass filter

Op Amp Application Circuits

— Example



Television signal splitter consisting of a high-pass and a low-pass filter.

Some Drawbacks of Passive Filter:

- Very sensitive to the component value tolerances.
- For low frequencies, the values of R and C can be quite large, leading to physically large components.
- Cannot add gain to the filter itself.
- Potentially have a high output impedance.



Op Amp Application Circuits

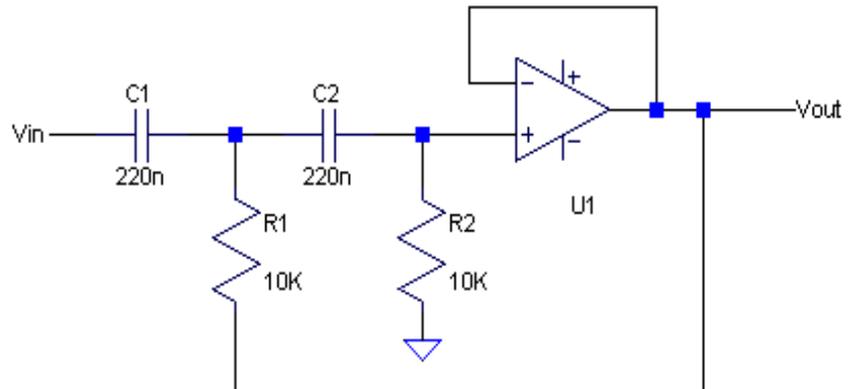
Active Filter

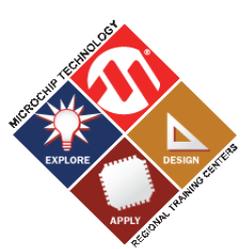
- Active filter is implemented using a combination of passive and active components.

An active component is one that require a source of energy to perform its intended function and can be used to provide gain in an electronic circuit, such as op amps.

- Example:

High-pass active filter





Op Amp Application Circuits

Principal reasons for the use of active filters

The op amps powering the active filter can be used to:

I. Shape the filter's response

- Add gain to the filter.
- Shape the filter how steeply it moves from its passband to stopband. (To do this passively, one must use inductors, which are often quite physically large and tend to pick up surrounding noise.)

II. Buffer the filter from the electronic components it drives.

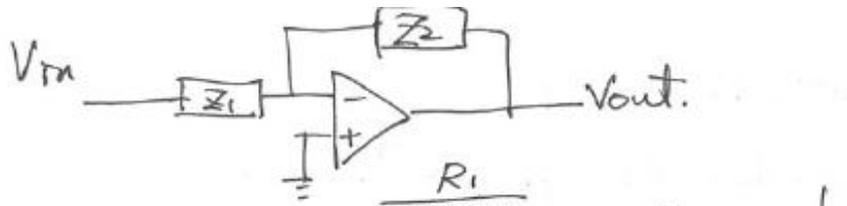
- This is often necessary so that they do not affect the filter's actions.



Op Amp Application Circuits

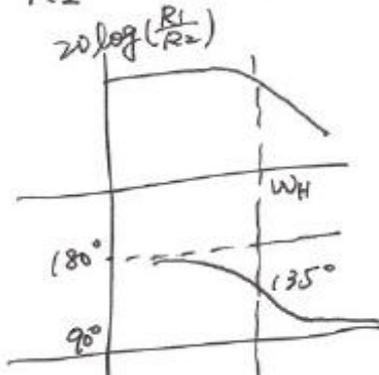
Low Pass Active Filter

- It passes low frequencies well, but attenuates frequencies higher than the cut-off frequency f_c .



$$\frac{V_o}{V_i} = -\frac{Z_2}{Z_1} = -\frac{R_1}{R_2} \cdot \frac{1}{1+sRC}$$

$$= -\frac{R_1}{R_2} \cdot \frac{1}{1+j\frac{\omega}{\omega_0}}$$



$$\frac{1}{R'} = \frac{1}{R_1} + \frac{1}{sC}$$

$$\Rightarrow R' = \frac{R_1}{1+sRC}$$

$$T = RC$$

$$\omega = \frac{1}{RC}$$

$$\Rightarrow f = \frac{1}{2\pi RC}$$

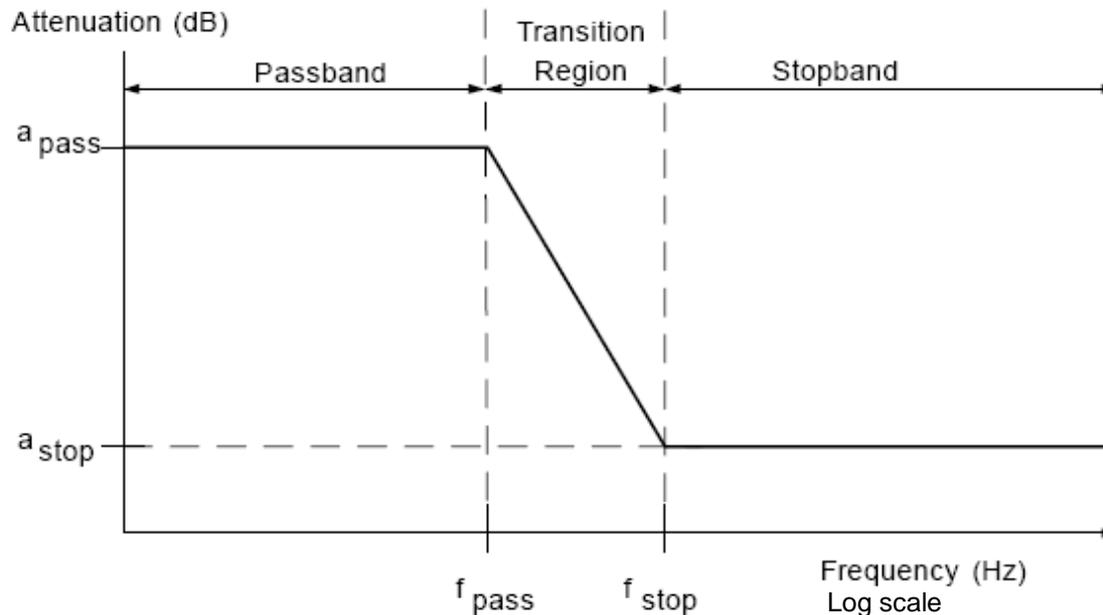
$$: V_o/V_i, f_c = 1/(2\pi R_1 C)$$

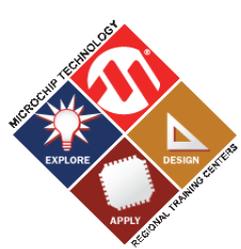
- **Unit: f in hertz (Hz), R in ohms (Ω), C in farads (F)**



Op Amp Application Circuits

- $f \gg f_p$, $G \approx 0$; $f \ll f_p$, $G \approx -R_1/R_2$.
- $f_p = f_{\text{pass}} = f_c = 1/(2\pi R_1 C)$
- f_{stop} must be greater than f_{pass} .





Op Amp Application Circuits

High Pass Active Filter

- It passes high frequencies well, but attenuates frequencies lower than the cut-off frequency f_c .

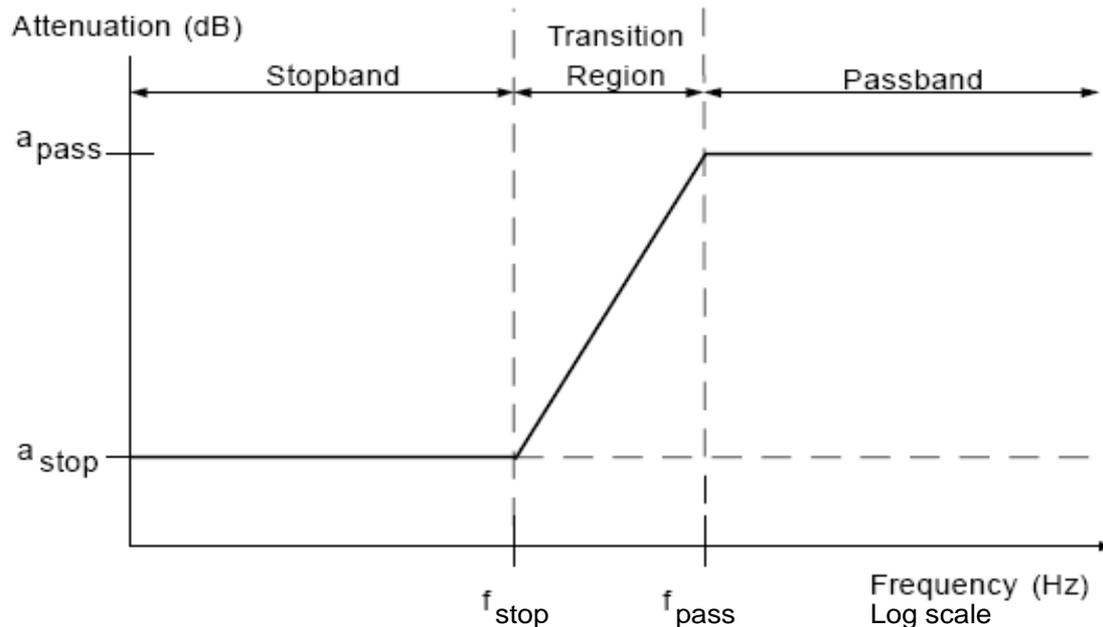
$$\begin{aligned} \frac{V_o(s)}{V_i(s)} &= \frac{-Z_2(s)}{Z_1(s)} = -\frac{R_2}{R_1 + \frac{1}{sC_1}} = -\frac{R_2 s C_1}{1 + s R_1 C_1} \\ &= -\frac{R_2}{R_1} \left[\frac{R_1 s C_1}{1 + s R_1 C_1} \right] \\ T(j\omega) &= \frac{V_o(j\omega)}{V_i(j\omega)} = A_{\infty} \left[\frac{j\omega R_1 C_1}{1 + j\omega R_1 C_1} \right] = A_{\infty} \left[\frac{j\omega/\omega_L}{1 + j\omega/\omega_L} \right] \\ &\qquad\qquad\qquad \omega_L = 1/R_1 C_1 \end{aligned}$$

- Closed loop gain $G = V_o/V_i$, $f_c = 1/(2\pi R_2 C)$
 - **Unit: f in hertz (Hz), R in ohms (Ω), C in farads (F)**



Op Amp Application Circuits

- $f \ll f_p, G \approx 0; f \gg f_p, G \approx -R_1/R_2$
- $f_p = f_{pass} = f_c = 1/(2\pi R_2 C)$
- f_{pass} must be greater than f_{stop} .





Op Amp Application Circuits

Band Pass Active Filter

- It 需注意运算放大器之带宽特性.

an

Pole & Zero

- P
- F

$$Z_1 = Z_2 + R_2 = \frac{1}{j\omega C_2} + R_2$$

$$Z_2 = Z_{C_1} \parallel R_1 = \frac{1}{j\omega C_1} \parallel R_1$$

$$\frac{V_o}{V_i} = -\frac{Z_2}{Z_1} = -\frac{Z_1 \parallel R_1}{Z_2 + R_2}$$

$$= \frac{R_1}{\frac{1}{j\omega C_1 R_1} + 1} = \frac{j\omega C_2 R_1}{(1 + j\omega C_1 R_1)(1 + j\omega C_2 R_2)}$$

- Where $f_{c1} = 1/(2\pi R_1 C_1)$, $f_{c2} = 1/(2\pi R_2 C_2)$.

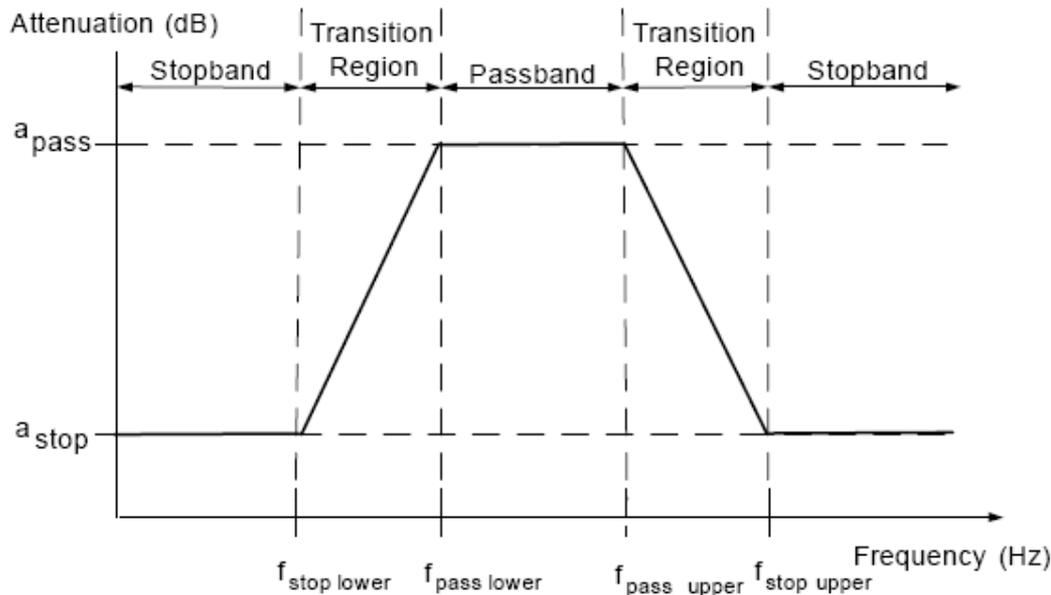
r low pass

with a gain of



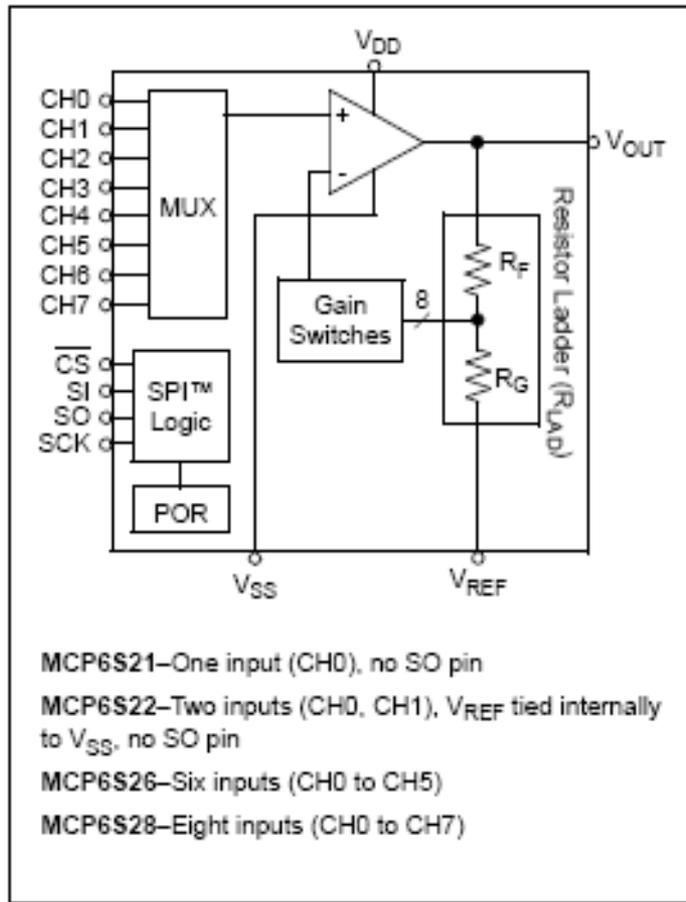
Op Amp Application Circuits

- Attenuate $f \ll f_{PL}$, $f \gg f_{PU}$; Pass $f_{PL} \leq f \leq f_{PU}$, $G = -R_1/R_2$
 - $f_{PL} = f_{\text{pass-lower}} = f_{c2} = 1/(2\pi R_2 C_2)$
 - $f_{PU} = f_{\text{pass-upper}} = f_{c1} = 1/(2\pi R_1 C_1)$
- $f_{\text{stop-lower}} < f_{\text{pass-lower}} < f_{\text{pass-upper}} < f_{\text{stop-upper}}$



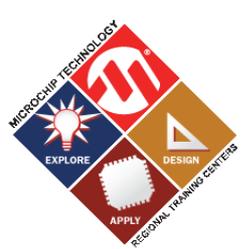


Programmable Gain Amplifier MCP6S2X



Features

- Multiplexed Inputs: 1, 2, 6 or 8 channels
- 8 Gain Selections:
 - +1, +2, +4, +5, +8, +10, +16 or +32 V/V
- Serial Peripheral Interface (SPI™)
- Rail-to-Rail Input and Output
- Low Gain Error: $\pm 1\%$ (max)
- Low Offset: $\pm 275 \mu V$ (max)
- High Bandwidth: 2 to 12 MHz (typ)
- Low Noise: 10 nV/Hz @ 10 kHz (typ)
- Low Supply Current: 1.0 mA (typ)
- Single Supply: 2.5V to 5.5V

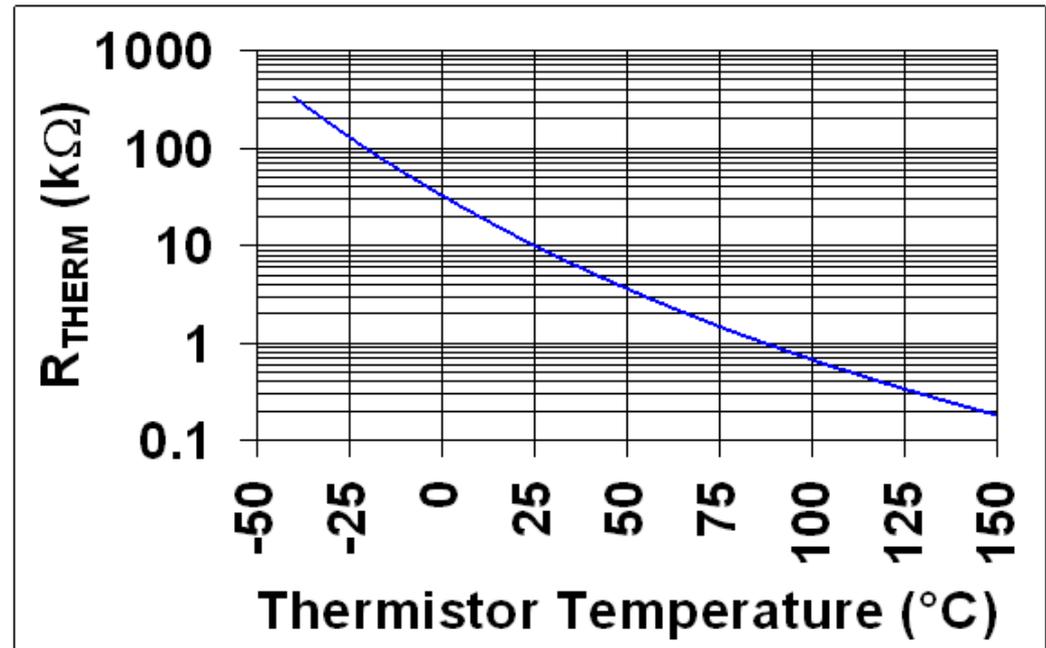


Resistive Sensors – Thermistor

Resistance vs. Temperature

T_{THERM} (C)	T_{THERM} (F)	R_{THERM} (k)
-40	-40	332.1
0	32	32.56
25	77	10.00
70	158	1.753
125	257	0.3387
150	302	0.1826

BCcomponents P/N: 2381 640 55103





Resistive Sensors – Thermistor

- **Resistance to Voltage Conversion**

- **Requires current excitation**

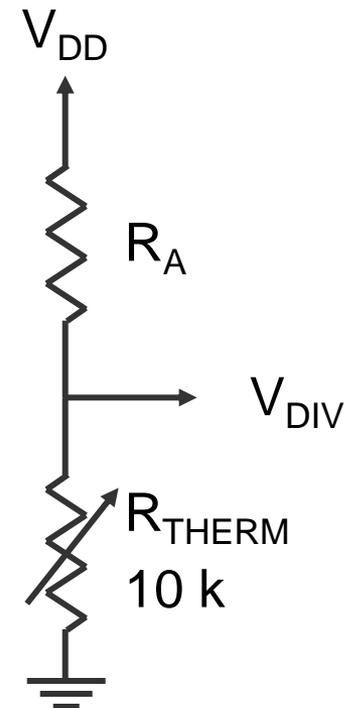
- Voltage Reference and Resistor
- Current Reference

- **R_{THERM} vs. temperature**

- Is very non-linear
- Is approximately exponential

- **Voltage divider**

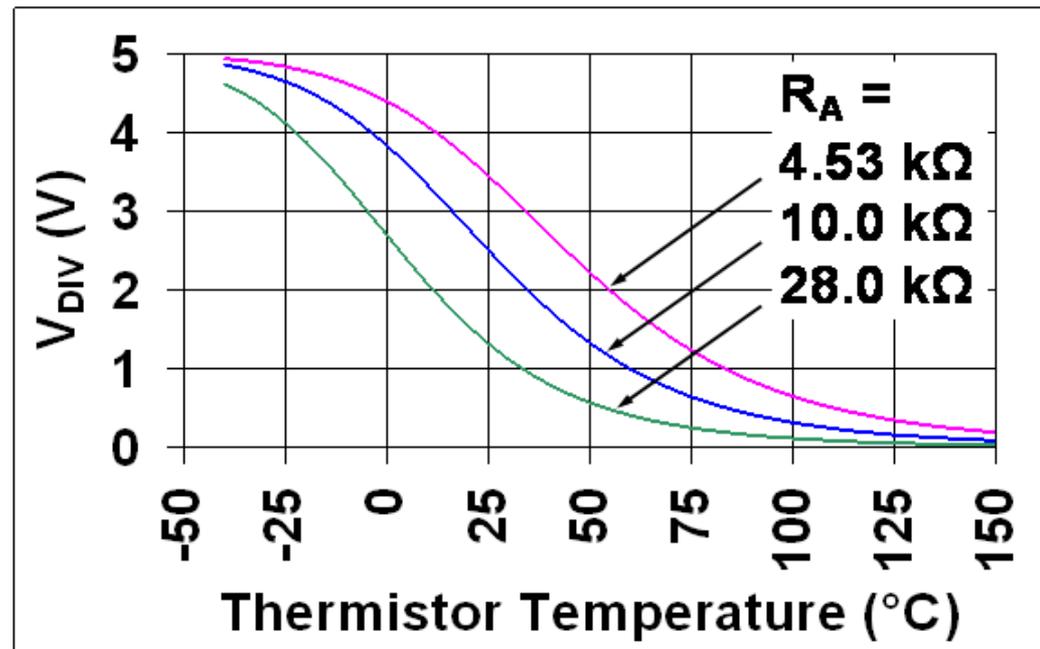
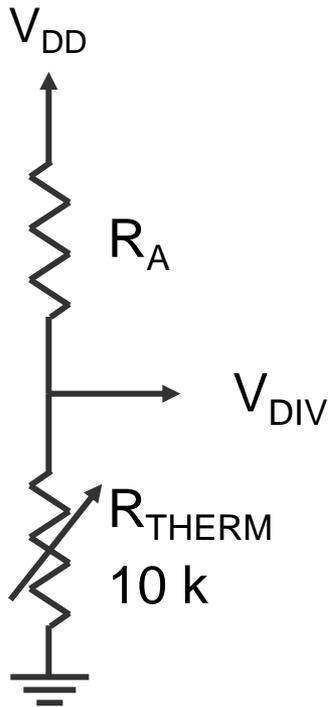
- Ratiometric ($V_{DD} = \text{ADC's } V_{REF}$)





Resistive Sensors – Thermistor Divider Output Voltage

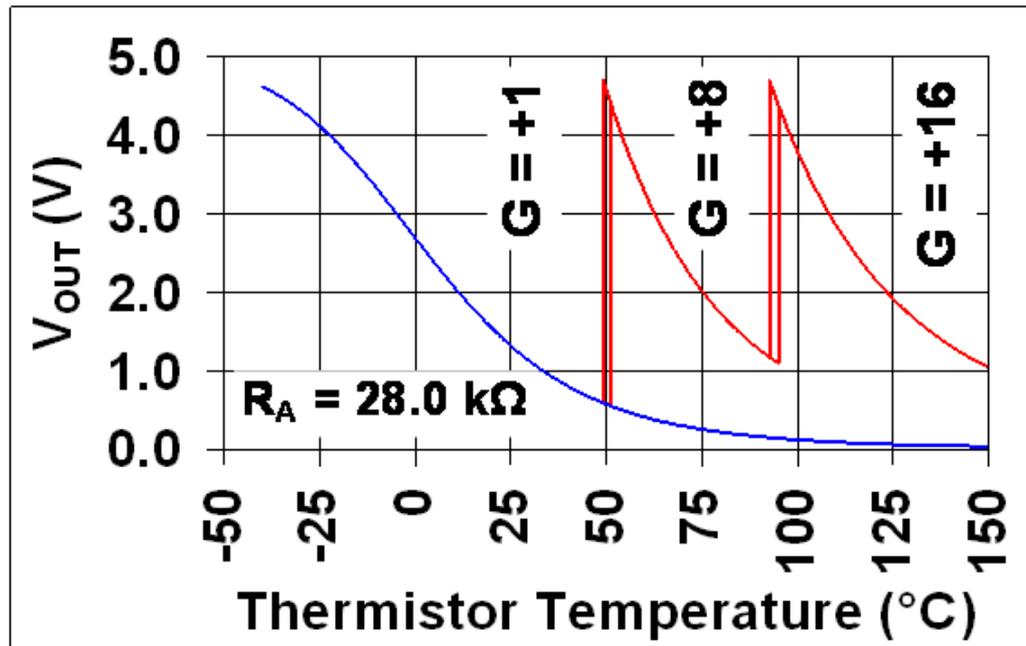
- Increasing R_A :
 - Lowers “Linear” Temperature Range
 - Reduces Self-Heating





Resistive Sensors – Thermistor With PGA and Filter

- PGA Gain = 1 only
 - Limited Temperature Range
 - Poor linearity
 - Poor sensitivity
 - Easier Design
- PGA Gain = 1, 8, 16
 - Full Temperature Range
 - Good Linearity
 - Good Sensitivity
 - Much Better Accuracy





Digital Potential Meter MCP41XXX

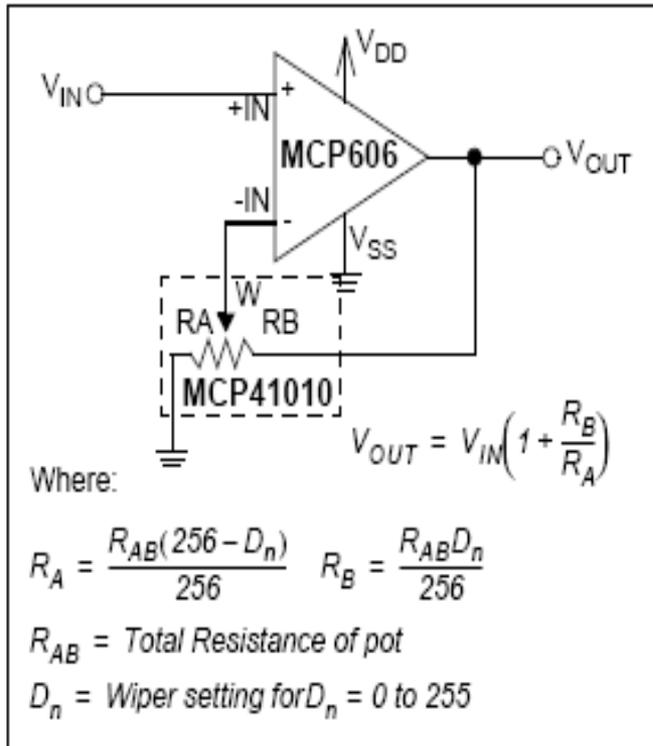


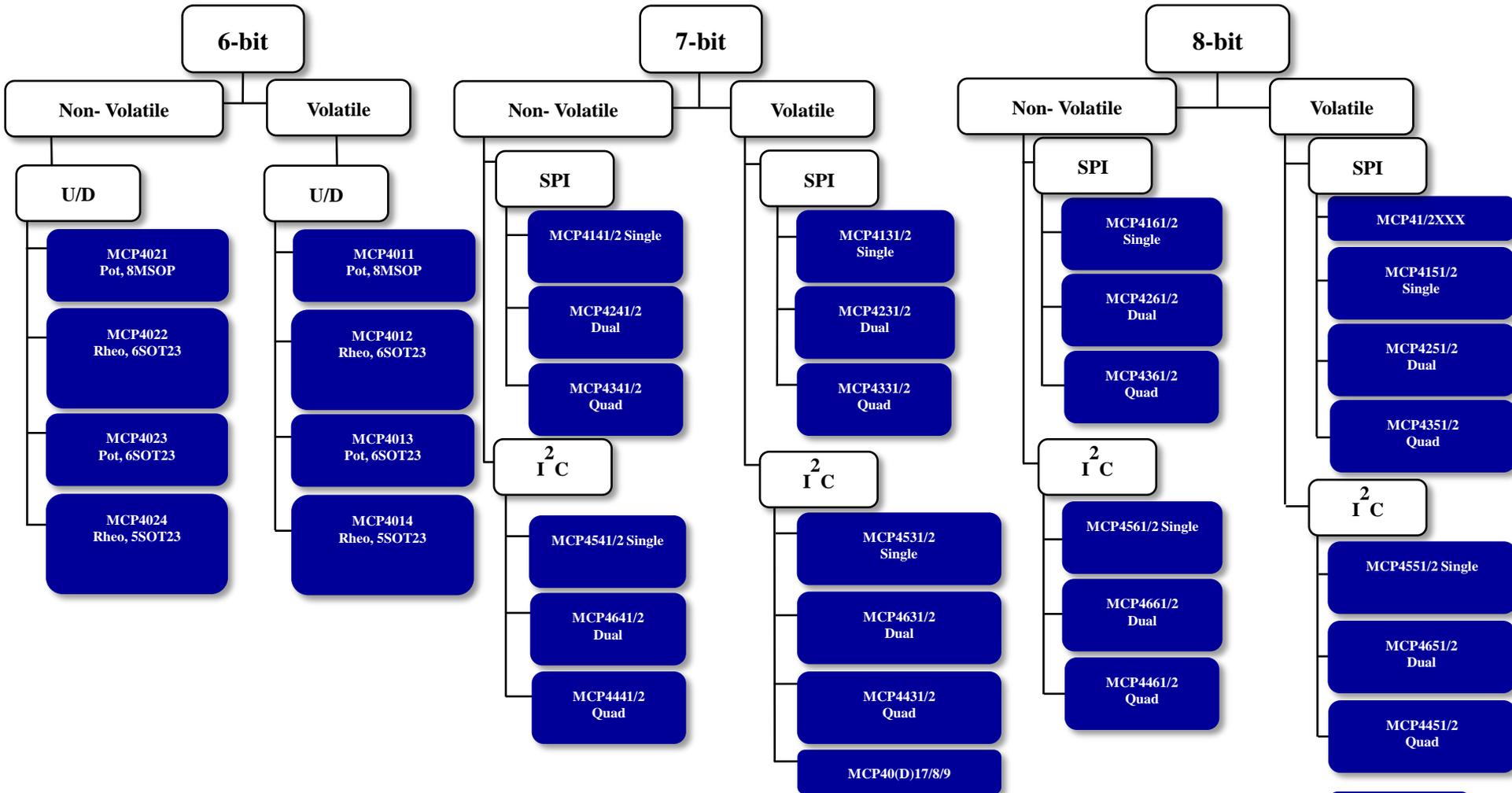
FIGURE 4-5: Single-supply, programmable, non-inverting gain amplifier.

Features

- 256 taps for each potentiometer
- Potentiometer values for 10 kΩ, 50 kΩ and 100 kΩ
- Single and dual versions
- SPI™ serial interface (mode 0,0 and 1,1)
- ±1 LSB max INL & DNL
- Low power CMOS technology
- 1 μA maximum supply current in static operation
- Multiple devices can be daisy-chained together (MCP42XXX only)
- Shutdown feature open circuits of all resistors for maximum power savings
- Hardware shutdown pin available on MCP42XXX only
- Single supply operation (2.7V - 5.5V)
- Industrial temperature range: -40°C to +85°C
- Extended temperature range: -40°C to +125°C



Digital Potentiometers



Mixed Signal
Demo & Eval Boards

<< BACK



New Release Information

● Documentation links

– Product Datasheets

- [MCP651](#), “50 MHz, 6 mA Op Amps with mCal”
- [MCP621](#), “20 MHz, 2.5 mA Op Amps with mCal”

– Application Notes

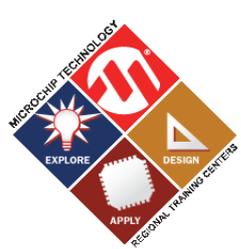
- [AN1177](#), “Op Amp Precision Design: DC Errors”
- [AN1258](#), “Op Amp Precision Design: PCB Layout Techniques”
- AN1353, “Op Amp Rectifiers, Peak Detectors and Clamps”



Op Amp Application Circuits

Other Applications

- Audio and video pre-amplifiers and buffers
- Voltage and current regulators
- Analog-to-digital converter driver
- Digital-to-analog converter buffer
- Oscillators and waveform generators
- Analog computer(Integrator, Differentiator, etc..)



Application Notes

- **AN1151 - PIC18F2520 MCP3909 3-Phase Energy Meter Reference Design**
- **AN1291 - Low Cost Shunt Power Meter using MCP3909 and PIC18F25K20**
- **AN994 - IEC Compliant Active-Energy Meter Design Using the MCP3905A/6A**
- **AN1327A - Avoiding MOSFET Driver Overstress**
- **AN1256 - Microchip's Power MOSFET Driver Simulation Models**
- **AN763 - Latch-Up Protection for MOSFET Drivers**
- **AN786 - Considerations for Driving Power MOSFETs in High-Current, Switch Mode Regulators**
- **AN799 - Matching MOSFET Drivers to MOSFETs**
- **AN1258 - Op Amp Precision Design: PCB Layout Techniques**
- **AN1297 - Microchip's Op Amp SPICE Macro Models**
- **AN1306 - Thermocouple Circuit Using MCP6V01 and PIC18F2550**
- **AN1316 - Using Digital Potentiometers for Programmable Amplifier Gain**
- **AN679 - Temperature Sensing Technologies**

More.... → Please visit www.microchip.com/analog



Summary

We Have Met Our Objectives

- Learned the basic op amp concepts and terminology.
- Understood the typical DC and AC specifications found in our op amp datasheet.
- Worked on the op amp application circuits.
- Learned Microchip Analog and Interface Products Offerings (Treelink for Analog and Interface Product Selection and Reference Demo Boards)

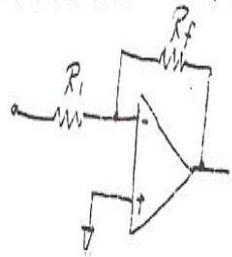
Quiz Answer

(B) 1. 理想運算放大器之定義不包含

- A) 輸入阻抗 = ∞ B) 輸出阻抗 = ∞ C) 開環增益 = ∞ D) 頻率響應 = ∞

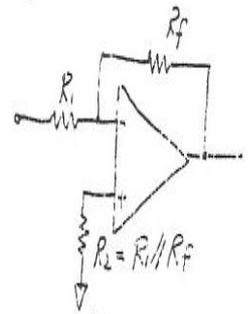
(C) 2. 右側電路之輸入阻抗為

- A) ∞ B) 0 C) R_1 D) R_1^2



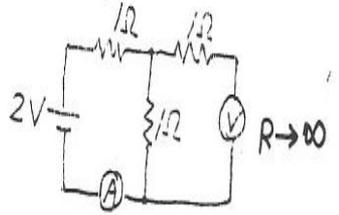
(C) 3. 右側電路之 R_2 作用為何

- A) 增加輸出阻抗 B) 減少消耗電流
C) 平衡 I_{bias} 所造成的 V_{os} D) 增加頻寬



(C) 4. 右圖之電流錶讀值為

- A) 2A B) 2/1.5A C) 1A D) 0A



(A) 5. 上題之電壓錶讀值為

- A) 1V B) 2V C) 1/1.5V D) 0V

$R \rightarrow 0$

(A) 6. 若一 OP-AMP 之 GBWP 為 10MHz, 若在小信號放大時, 增益為 10 倍則頻寬為

- A) 1 MHz B) 10 MHz C) 100 KHz D) 需考慮扭轉率 (Slew Rate)

(D) 7. 若一 OP-AMP 接單電源且使用 2 個電阻, 則以下何者為真

- A) 反相或非反相輸入端可為負電壓 B) 可以構成反相放大器 C) 可構成 Audio 信號放大 D) 若 $V_{in} > 0$, 可以構成非反相放大器

(C) 8. 若一 OP-AMP 之 $V_{os} = 2mV$, 作小信號放大 Gain = 100 倍, 當 $V_{in} = 0$, 則 $V_o =$

- A) 2 mV B) 100mV C) 200mV D) 0mV

(B) 9. 對於 OP 作為隨耦級, 以下敘述何者為非

- A) 增加輸入阻抗 B) 增加輸出阻抗 C) 增加輸出驅動能力 D) 電壓增益 = 1

(E) 10. 以 CMOS 構成的 OP-AMP 有些特點, 以下何者為非

- A) 低 Supply current B) 低 I_{bias} C) 容易做到 rail-to-rail Input/Output
D) 低雜訊 E) 高速放大

(Bandwidth Limitation)



References

- [1] MCP601/2/3/4, MCP6021/2/3/4, MCP6041/2/3/4 Datasheets
- [2] **Applications Note An722 “Operational Amplifier DC Specifications and Applications”**, Baker, Bonnie C, Microchip Technology Inc., 2000
- [3] **Applications Note An723 “Operational Amplifier AC Specifications and Applications”**, Baker, Bonnie C, Microchip Technology Inc., 2000
- [4] “Analog Integrated Circuit Design”, Wiley 1997 by Martin, Johns.
- [5] “Design of Analog CMOS Integrated Circuits” International Edition 2001 by Razavi, Behzad.
- [6] **“Microelectronic Circuits” Fourth Edition 1998 by Sedra, Adel S. and Smith, Kenneth C.**
- [7] Paul Horowitz and Winfield Hill, "The Art of Electronics 2nd Ed. " Cambridge University Press, Cambridge, 1989
- [8] Black, H., Stabilized Feedback Amplifiers, Bell System Technical Journal 13, 1/35
- [9] Graeme, J.G., Feedback Models Reduce Op Amp Circuits to Voltage Dividers, EDN, June 20, 1991



Thank You
for attending the class!

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